

Water Supply Summary Report - Kawartha Downs & Speedway, Fraserville, Ontario

October 14, 2021

Prepared for:

Romspen Investment Corporation

Cambium Reference: 12579-001

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Table of Contents

| 1.0 | Introduction | 1 |
|---------|--|----|
| 1.1 | Site Description | 1 |
| 2.0 | Surrounding Area Hydrogeology and Water Supply | 3 |
| 2.1 | Water Well Records | 3 |
| 2.1.1 | Tested Water Wells | 4 |
| 2.1.1.1 | Well 1: 5119296 | 4 |
| 2.1.1.2 | 2 Well 2: 5119297 | 4 |
| 2.1.2 | Minimum Yield Rate | 5 |
| 2.2 | Wetlands | 5 |
| 2.3 | Vulnerable and Regulated Areas | 6 |
| 2.4 | Hydrogeological Conditions | 6 |
| 3.0 | Pumping Test Results | 8 |
| 3.1 | Well 1 | 8 |
| 3.2 | Well 2 | 9 |
| 3.3 | Extrapolated Drawdown | 10 |
| 4.0 | Conclusions and Recommendations | 11 |
| 4.1 | Respectfully submitted, | 13 |
| 5.0 | References | 14 |
| 6.0 | Standard Limitations | 15 |



| ı | List | of | Tal | h | es |
|---|------|-----|-----|--------------|----|
| ı | LIJL | OI. | IG | \mathbf{v} | |

| Table 1: | Water Well Record Information | 4 |
|--------------|--|----|
| Table 2: | Aquifer Test Pro TM Results | 10 |
| Table 3: Res | ults of Drawdown Extrapolation | 10 |

List of Appended Figures

| Figure 1 | Site Plan |
|----------|--|
| igure 2 | MECP Well Records within 500 m of Site |
| Figure 3 | Water Level Fluctuations – Well 1 |
| igure 4 | Water Level Fluctuations – Well 2 |
| igure 5 | Extrapolated Drawdown |

List of Appendices

Appendix A Land Information and Proposed Development Plan

Appendix B MECP Water Well Records for Test Wells

Appendix C AquiferTest ProTM Results



1.0 Introduction

Cambium Inc. (Cambium) was retained by Romspen Investment Corporation (Client) to conduct a water supply assessment for the Kawartha Downs and Speedway, located at 1382 County Road 28, in the community of Fraserville, in the County of Peterborough, Ontario (Site).

The present land-use for the middle and southern section of the Site is as a commercial raceway; the northern section of the site is presently rural residential with some agricultural uses (Figure 1). Cambium understands that the Client is exploring a subdivision development for the subject property.

The water supply assessment was completed in support of a proposed re-development and includes a general review of available surrounding hydrogeological and water supply information and an evaluation of the results of pumping tests conducted on two (2) on-site wells. As part of the scope of work, Cambium was also retained to complete a Geotechnical Investigation (Cambium, 2021a), a Phase I and Phase II Environmental Site Assessment (ESA) (Cambium, 2021b; Cambium, 2021c; Cambium, 2021d), a Preliminary Natural Features Assessment & Ecological Constraints (Cambium, 2021e), a Wastewater Packaged Treatment Plant Concept (Cambium, 2021f), and an Environmental Impact Study (EIS) (Cambium, 2021g); each of these reports will be presented under a different cover.

1.1 Site Description

The Site is 267 acres (108 ha) and is L-shaped. The southern portion of the Site is developed with a commercial building, paved parking, paved driveways, and a 3/8-mile paved oval racetrack; it is zoned Commercial District 4 (C4) as per plate 'D-4' per the Township of Cavan-Monaghan Zoning By-Law 2015-58 Schedule. The northern portion of the Site is currently vacant field; it is zoned Agricultural (A) as per 'Map D-4' per the Township of Cavan-Monaghan Zoning By-Law 2015-58 Schedule. The Site is bordered by natural core, rural residential, and agricultural to the west, hamlet residential and agricultural to the south, County Road 28 to the



east, and Moore Drive to the North. Refer to **Error! Reference source not found.** for Zoning By-Law and land information.



2.0 Surrounding Area Hydrogeology and Water Supply

2.1 Water Well Records

The Ministry of Environment Conservation and Parks (MECP) Water Well Information System (WWIS) was accessed to review water well records in the area of the Site. There were 48 water well records located within approximately 500 m of the borders of the Site (see Figure 2). The following water well records were identified:

- Forty-four (44) water well records for drilled wells
- One (1) water well record for a monitoring well
- One (1) record outlined no information
- Two (2) records outlined well abandonments

The soil profile generally consisted of >1 m of topsoil, underlain by overburden. Overburden generally consisted of interlayered beds of brown clay with clasts and sand and sand with silt and gravel sediments. 24 well records reported bedrock (limestone and shale) contact between 8.23 to 14.48 metres below ground surface (mbgs).

Water bearing sediments were identified within overburden at various depths. Water bearing strata were also identified at the overburden bedrock contact and within bedrock (within 0 to 26.51 m, average 4.88 m of bedrock contact).

The static water level of overburden wells ranged from 1.22 to 9.14 mbgs, average of 4.70 mbgs. The recommended flow rate reported from the overburden supply wells ranged from 3 gallon per minute (gpm, assumed to be US gallons per minute) to 30 gpm, averaging 11 gpm. These flow rates equate to ranges between 11 L/min and 114 L/min, averaging 41 L/min.

The static water level of bedrock wells ranged from 0.61 to 7.01 mbgs, average of 3.42 mbgs. The recommended flow rate reported from the bedrock supply wells ranged from 4 gpm to 25 gpm, averaging 11 gpm. These flow rates equate to ranges between 15 L/min and 95 L/min, averaging 41 L/min. Further information summarized from the water well records are listed below in Table 1.



Table 1: Water Well Record Information

| | | Total Depth (mbgs) | Depth Water Encountered (m) | Depth Installed into Bedrock (m) | Static Water Level (mbgs) | Recommended Pumping Rate (gpm) |
|--------------|------|-----------------------|-----------------------------------|--|------------------------------|--------------------------------------|
| Overburden | Min | 9.14 | 7.01 | - | 1.22 | 3.00 |
| Wells | Max | 17.37 | 17.37 | - | 9.14 | 30.00 |
| Count:22 | Avg. | 11.53 | 11.25 | - | 4.70 | 10.82 |
| Bedrock | Min | 10.67 | 8.23 | 0.30 | 0.61 | 4.00 |
| Wells Count: | Max | 41.15 | 39.62 | 28.04 | 7.01 | 25.00 |
| 22 | Avg. | 20.12 | 14.87 | 10.13 | 3.42 | 10.91 |

2.1.1 Tested Water Wells

The following MECP wells records correlate to the wells that were used for the pump testings for the scope of work for this assessment. The MECP well records can be found in Appendix B.

2.1.1.1 Well 1: 5119296

Well 1 (MECP Tag # 5119296) was installed on November 20, 2002, approximately 400 m southeast of the existing residential dwelling at 1627 Moore Drive, Fraserville, Ontario. Well 1 was installed to a depth of 22.86 mbgs, with an open bedrock hole extending from 14.48 mbgs to 22.86 mbgs. During installation, sediments were described as sandy clay transitioning into sandy clay with gravel and some boulders. A water-bearing gravel layer was encountered at the overburden – bedrock contact at 14.48 mbgs. Limestone bedrock continued until well termination at 22.86 mbgs. Static water level on the day on the well installation was 3.35 mbgs. The well driller's recommended pumping rate was 38 L/min. The location of Well 1 is provided on Figure 1.

2.1.1.2 Well 2: 5119297

Well 2 (MECP Tag # 5119297) was installed on November 18, 2002, approximately 350 m east of the existing residential dwelling at 1627 Moore Drive, Fraserville, Ontario. Well 2 was installed to a depth of 23.16 mbgs, with an open bedrock hole extending from 11.58 mbgs to 23.16 mbgs. During installation, sediments were described as silty sand overlying sandy clay



with gravel. A water-bearing gravel layer was encountered at the overburden – bedrock contact at 11.58 mbgs. Limestone bedrock continued until well termination at 23.16 mbgs. Static water level on the day on the well installation was 3.05 mbgs. The well driller's recommended pumping rate was 45 L/min. The location of Well 2 is provided on Figure 1.

2.1.2 Minimum Yield Rate

As per Guideline D-5-5 (Ministry of the Environment, 1996) the minimum yield rate per person is 450 litres per day (0.3125 L/min). As per the most up-to-date proposed site plan at the preparation of this report (Appendix A), there will be 588 single-family dwellings built. At an average of 2.5 residents per dwelling, the minimum yield from one supply well for the proposed development would average approximately 460 L/min continually. Guideline D-5-5 also dictates that peak demand occurs for a period of 120 minutes per day and the peak demand rate is a minimum of 3.75 L/min per person. This yield of a minimum rate for the proposed development to approximately 5,500 L/min.

As per the MECP WWIS, the average yields of the overburden supply wells and bedrock supply wells were both approximately 41 L/min. This yield rate is insufficient for a communal/municipal supply that would be required for the proposed development.

2.2 Wetlands

A provincially significant wetland (PSW) is located within the boundaries of the Site. The PSW was identified as Cavan Creek Wetland. Existing Ministry of Natural Resources and Forestry (MNRF) PSW mapping shows two pieces of the PSW on the property, one extending eastward into the property from the western property boundary, in the central portion of the Site and the other extending southward onto the property from the northwest corner. Mapped unevaluated wetlands are approximate; as such, they require field verification in order to determine their presence and confirm their boundaries. In addition, areas of unevaluated wetlands are mapped surrounding the PSW's perimeter on the Site and adjacent lands. Mapped unevaluated wetlands are approximate; as such, they require field verification to determine their presence and confirm their boundaries (Cambium, 2021e).



The central portion of the Cavan Creek Wetland drains westwards off the Site. The northern portion of the Cavan Creek Wetland drains northwards off the Site. Other wetland areas in the northeastern portion of the Site drain eastwards off-site. All drainage from the Site converges with Cavan Creek before outletting to the Otonabee River.

2.3 Vulnerable and Regulated Areas

As per the Ministry of the Environment, Conservation and Parks (Ministry) Source Water Protection Information Atlas (SPIA) the Site is within the following areas:

- Highly Vulnerable Aquifer
- Significant Groundwater Recharge Area
- Intake Protection Zone 3

The SPIA mapping is attached in Appendix A.

There are several setback areas associated with the wetlands present on-site that should be considered as part of development on the property. Further studies to delineate on-site wetland boundaries and associated setback will be required (Cambium, 2021e).

2.4 Hydrogeological Conditions

Available information indicates that there are fine- to medium-grained sediments located at surface on the Site. Overburden sediments generally were water bearing indicating a shallow aquifer in the area averaging 4.70 mbgs. 22 drilled well records encountered bedrock on average 10.9 mbgs; each of these records recorded water found at or below the overburden bedrock contact, indicating an additional deeper bedrock aquifer averaging 14.9 mbgs.

Groundwater flow within the shallow overburden sediments on-site was assumed to follow the overlying topography of the Site, and groundwater to the north and west of the topographic high was assumed to flow northward off-site into the PSW (Cavan Creek Wetland). Groundwater to the south and east of the topographic high flows to the east toward the Otonabee River (Error! Reference source not found.; Error! Reference source not



found.). The on-site unevaluated wetland is assumed to be sourced both from surface runoff and shallow groundwater discharge.



3.0 Pumping Test Results

This section presents the results of the pumping tests for two (2) on-site wells.

3.1 Well 1

The static water level of Well 1 was 2.77 mtop (which corresponds to a depth of 2.15 mbgs) just prior to the pumping test. The pumping test commenced at 10:20 am on August 16, 2021 at a rate of 30 L/min. Within 10 minutes after the commencement of the pumping test, the water level of Well 1 lowered to 6.88 mtop. After the initial 10 minute interval the water level of Well 1 lowered consistently until 12:20 pm to a level of 8.27 mtop. At 12:20 pm, the pumping rate was increased to 45 L/min. Within 10 minutes of the new pumping rate, the water level lowered to 9.85 mtop; water levels then lowered consistently until 2:20 pm to a level of 10.88 mtop. Finally, the pumping rate was adjusted to 60 L/min at 2:20 pm. Again, after the initial 10 minute interval the water level was lowered to 13.92 mtop. Water levels consistently lowered after this until the end of the pumping test at 3:32 pm with a recorded water level of 14.88 mtop. The depth of drawdown achieved at Well 1 upon completion of the pumping test was 10.41 m. The pumping rate was maintained at an average rate of 30 L/min throughout the first two hours of the test, which equated to approximately 3,600 L of water and an initial interval Specific Capacity of 5.45 L/min/m and a theoretical yield of 113.3 L/min. The next two hours of the test maintained a pumping rate of 45 L/min which corresponds to 5,400 L of water and an interval Specific Capacity of 25.00 L/min/m. The final two hours of the test maintained a pumping rate of 60 L/min which corresponds to 7,200 L of water and an interval Specific Capacity of 18.99 L/min/m; the total amount of water withdrawn is approximately 16,200 L.

Upon completion of the pumping test the water level of Well 1 was allowed to recover. By 3:58 pm on August 16, 2021 the water level in Well 1 recovered to 4.47 mtop (or 86% recovery to pre-test static conditions). The water level responses of Well 1 during the pumping test are provided on a time/drawdown plot in Figure 3.

The drawdown data recorded from Well 1 were imported into AquiferTest Pro[™] and processed to determined transmissivity and hydraulic conductivity. The transmissivity was calculated to



be 4.89 m²/day; the hydraulic conductivity was 6.75×10^{-6} m/s. The results of the aquifer test analyses are outlined below in Table 2. The AquiferTest ProTM results are included in Appendix C.

The stepped – drawdown test indicates a sustainable yield of between 45 and 60 L/min.

3.2 Well 2

The static water level of Well 2 was 2.66 mtop (which corresponds to a depth of 1.67 mbgs) just prior to the pumping test. The pumping test commenced at 10:58 am on August 17, 2021 at a rate of 65 L/min. The water level within Well 2 dropped quickly upon initiation of the pumping test, and had reached 21.63 mtop within 6 minutes. Due to the rate that the water level was dropping at and the pump being installed at 23.3 mtop, the pumping test was ended at the 6 minute mark. Throughout the duration of the pumping test, the pumping rate was maintained at an average rate of 65 L/min.

Upon completion of the pumping test the water level of Well 2 was allowed to recover. By 12:45 pm on August 16, 2021 the water level in Well 2 recovered to 4.12 mtop (or 92% recovery to pre-test static conditions). The water level responses of Well 2 during the pumping test are provided on a time/drawdown plot in Figure 4.

The drawdown data recorded from Well 2 were imported into AquiferTest Pro^{TM} and processed to determined transmissivity and hydraulic conductivity. The transmissivity was calculated to be 0.18 m²/day; the hydraulic conductivity was 1.79 x 10^{-7} m/s. The results of the aquifer test analyses are outlined below in Table 2. The AquiferTest Pro^{TM} results are included in Appendix C.

The sustainable yield of Well #2 is less than 65L/min.



Table 2: Aquifer Test Pro™ Results

| Well | Transmissivity (m²/day) | Hydraulic Conductivity (m/s) |
|--------|-------------------------|------------------------------|
| Well 1 | 4.89 | 6.75 x 10 ⁻⁶ |
| Well 2 | 0.18 | 1.79 x 10 ⁻⁷ |

3.3 Extrapolated Drawdown

The lowering water levels trend recorded near the end of the pumping test for Well 1 (when a stable lowering was recorded) was extrapolated to 1 year and 20 years on a logarithmic time scale. Because it has to be assumed that the pumping rate would remain stable; only the extrapolated drawdown for the pumping rate of 30 L/min was viable as it was the pumping rate that started at static water level (Figure 5). Well 2 could not be analysed in this way as it never reached a stable lowering trend. This kind of assessment is valuable in estimating long-term impacts related to water withdrawal at a well. The results of the drawdown extrapolation for Well 1 are in Table 3:

Table 3: Results of Drawdown Extrapolation

| Well 1 | Time Frame | Extrapolated Drawdown (m) | Available Drawdown (m) |
|-----------|-------------------|---------------------------|------------------------|
| | Beginning of Test | - | 20.79 |
| 20 I /min | End of Test | 5.50 | 15.29 |
| 30 L/min | 1 Year | 11.80 | 8.99 |
| | 20 Years | 13.00 | 7.79 |

Note: Extrapolated drawdown indicates the expected drawdown from the static water level of each respective well

The results of the extrapolated drawdown analysis indicate that if water withdrawal at the Well 1 is continued for 1 and 20 Years at 30 L/min, the depths of drawdown were estimated to be 11.80 m and 13.00 m, respectively. The corresponding depths of available drawdown for the 1 and 20 Year periods were estimated to be 8.99 m and 7.79 m, respectively.



4.0 Conclusions and Recommendations

Cambium completed a pumping test on two (2) previously installed wells on-Site. Both of these wells are drilled into similar stratigraphy which characterizes the area: overburden extended until approximately 12.5 mbgs and consisting of sandy clay with some gravel, and bedrock extending until well termination and composed of limestone. Both wells draw from the aquifer that exists at or within several metres of the overburden – bedrock contact.

Water withdrawal occurred for a continuous 6 hour period for the pumping test at Well 1; the pumping test at Well 2 was cut short at 6 minutes due to insufficient water supply. The rate at Well 1 was initially 30 L/min for the first 2 hours, stepped up to 45 L/min for the middle 2 hours, and finally increased to 60 L/min for the final 2 hours. The pumping rate at Well 2 was initiated at 65 L/min. In total, 16,200 L and 390 L of water was withdrawn from the Well 1 and Well 2, respectively. The Specific Capacity of Well 1 during the 30 L/min pumping rate was 5.50 L/min/m with a theoretical yield of 113.3 L/min, during the 45 L/min pumping rate the Specific Capacity was 3.16 L/min. The Specific Capacity of Well 2 with a 65 L/min pumping rate was calculated to be 3.43 L/min/m with a theoretical yield of 73.72 L/min.

Upon completion of the pumping test for Well 1, approximately 16,200 L was pumped from the well and a maximum drawdown of 5.50 m was recorded (leaving approximately 15.29 m of available drawdown in the well). With a sustained pumping rate of 30 L/min, the depths of drawdown were extrapolated to be 11.80 m after 1 year of pumping and 13.00 m after 20 years of pumping. The corresponding depths of available drawdown for the 1 and 20 year periods were estimated to be 8.99 m and 7.79 m, respectively. This is a sufficient supply for a single residential dwelling use, however a pumping rate of 30 L/min is not sufficient for communal or municipal use. Because the pumping rates of 45 L/min and 60 L/min for Well 1 did not start at static water level, an accurate extrapolated drawdown could not be established. However, based off of the pumping test for Well 2 at 65 L/min which is installed in the same stratigraphy and is assumed to draw from the same aquifer, the higher pumping rate of 60 L/min (and most likely 45 L/min) would not be sustainable for any significant period of time and therefore would



not be sufficient. Furthermore, the proposed development would require a higher pumping rate than 65 L/min to sustain the amount of single-family dwellings proposed (see Section 2.1.2); therefore, neither well would be sufficient for the proposed development as neither can sustain a pumping rate of 65 L/min, and a pumping rate of 65 L/min would still be insufficient for the proposed development requirements of municipal/communal use.

In summary, the pumping test data collected from the two (2) on-Site wells are consistent with the MECP well records for water supply wells in the area: that there is insufficient water supply in the area for communal or municipal purposes. However, should private on-site servicing be considered in future, there is adequate supply for single family homes.

Given the objective of the study was to determine if an adequate communal supply was available on-site, water quality testing was not performed as there was no indication from the onsite wells that an adequate yield was available.

Cambium recommends that the proponent investigate off-site municipal supply well potential, The Township of Cavan Monaghan recently undertook a study to investigate the possibility of providing a Municipal Supply to the Fraserville Settlement Area and secured a property at 1256 Syer Line where a water well was installed in overburden sediments that was pumped continuously for 72 hours and provided a potential yield of ~9000L/min based on the pumping rate and extrapolation of Specific Capacity.



4.1 Respectfully submitted,

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5.0 References

- Cambium. (2021a). Geotechnical Investigation Report 1683 Moore Drive and 1490 County Road 28, Fraserville, Ontario. Cambium Inc.
- Cambium. (2021b). Phase I Environmental Site Assessment 1382 County Road 28, Fraserville, Ontario.
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- Cambium. (2021g). Environmental Impact Study 1490 County Road 28 and 1683 Moore

 Drive, Fraserville, Cavan-Monaghan, County of Peterborough, Ontario.
- Ministry of the Environment. (1996). *Procedure D-5-5, Technical Guideline for Private Wells:*Water Supply Assessment.



6.0 Standard Limitations

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A site assessment is created using data and information collected during the investigation of a site and based on conditions encountered at the time and particular locations at which fieldwork is conducted. The information, sample results and data collected represent the conditions only at the specific times at which and at those specific locations from which the information, samples and data were obtained and the information, sample results and data may vary at other locations and times. To the extent that Cambium's work or report considers any locations or times other than those from which information, sample results and data was specifically received, the work or report is based on a reasonable extrapolation from such information, sample results and data but the actual conditions encountered may vary from those extrapolations.

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Reliance

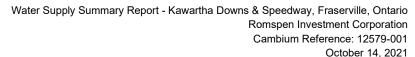
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WATER SUPPLY ASSESSMENT

ROMSPEN INVESTMENT CORPORATION Kawartha Downs and Speedway Fraserville, Ontario

LEGEND

Pump Test Well



Borehole



Monitoring Well

120 m Adjacent Lands

30m Wetland Setback

Watercourse, Intermittent

Contour 5m Interval (Major)

Contour 5m Interval (Minor)

Provincially Significant Wetland

Wetland Community



Site (approximate)

Notes:

- Base mapping features are © Queen's Printer of Ontario, 2019 (this does not constitute an endorsement by the Ministry of Natural Resources and Forestry or the Ontario Government).

- Distances on this plan are in metres and can be converted to feet by dividing by 0.3048.

- Cambium Inc. makes every effort to ensure this map is free from errors but cannot be held responsible for any damages due to error or omissions. This map should not be used for navigation or legal purposes. It is intended for general reference use only.



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SITE PLAN

Project No.: October 2021 12579-001 Rev.: Scale: Projection: NAD 1983 UTM Zone 17N 1:10,000 Checked by: Created by: Figure: MAT MB

WATER SUPPLY ASSESSMENT

ROMSPEN INVESTMENT CORPORATION Kawartha Downs and Speedway Fraserville, Ontario

LEGEND

Water Well Record



500 m Buffer



Notes:

- Base mapping features are @ Queen's Printer of Ontario, 2019 (this does not constitute an endorsement by the Ministry of Natural Resources and Forestry or the Ontario Government).

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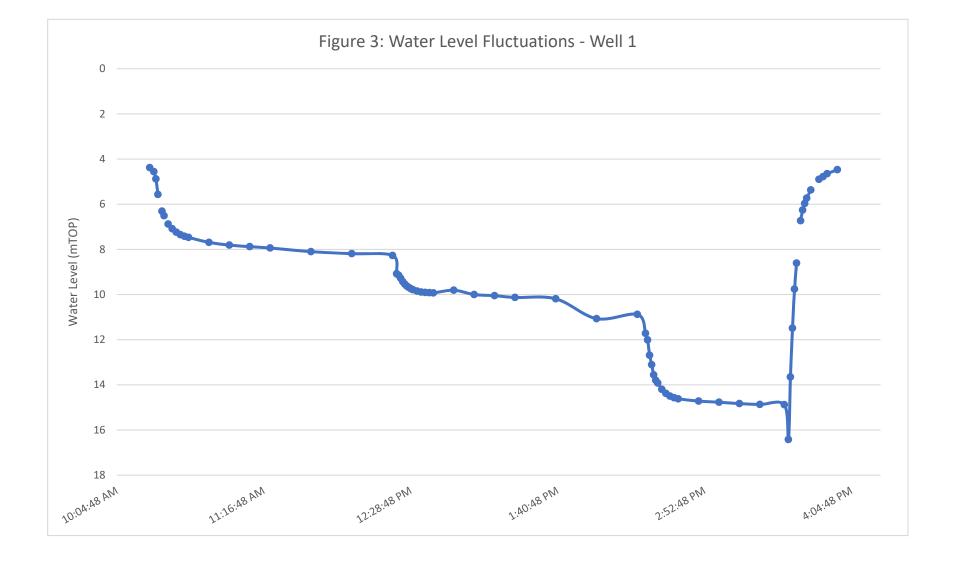


P.O. Box 325, 52 Hunter Street East Peterborough, Ontario, K9H 1G5 Tel: (705) 742.7900 Fax: (705) 742.7907

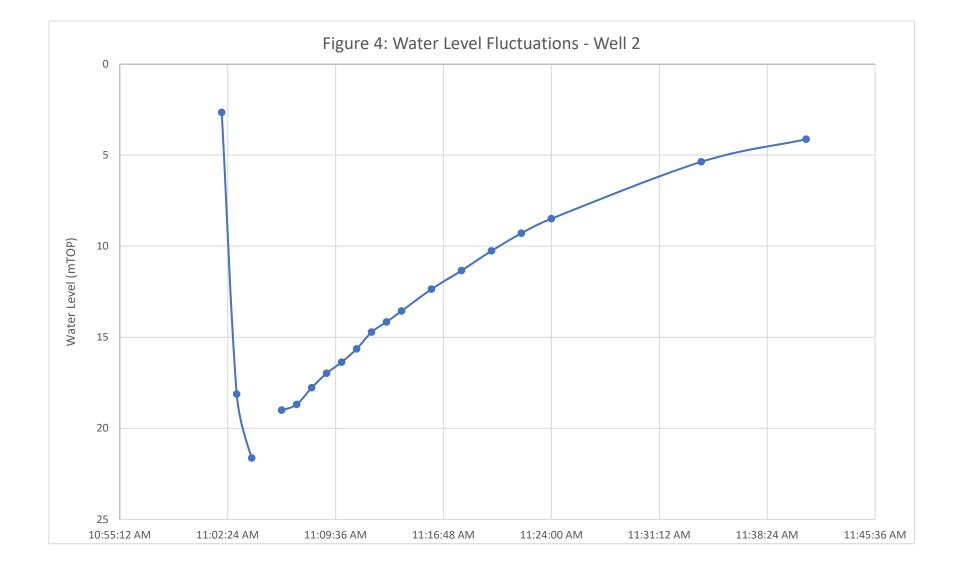
WATER WELL RECORDS LOCATED WITHIN 500 m OF SITE

Project No.: October 2021 Rev.: 12579-001 Scale: Projection: NAD 1983 UTM Zone 17N 1:14,000 Created by: Checked by: MAT MB

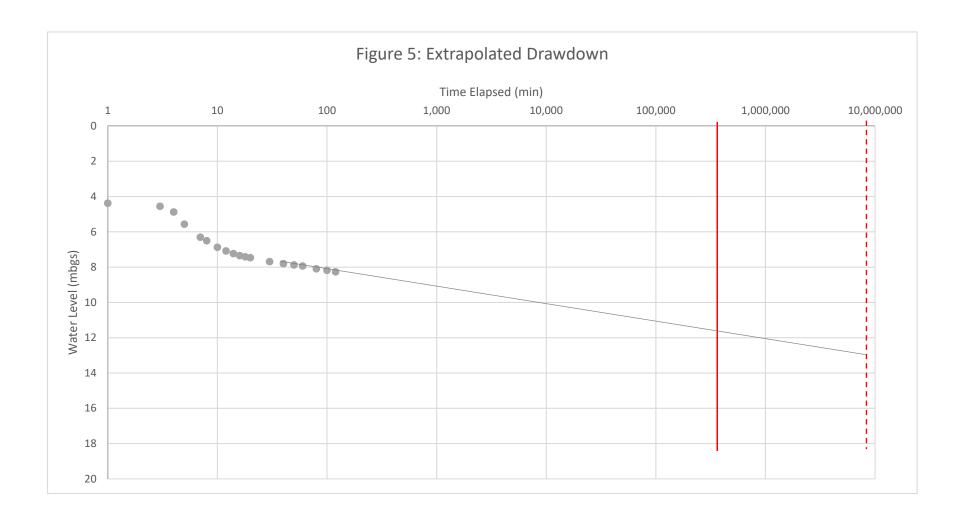


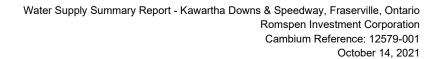








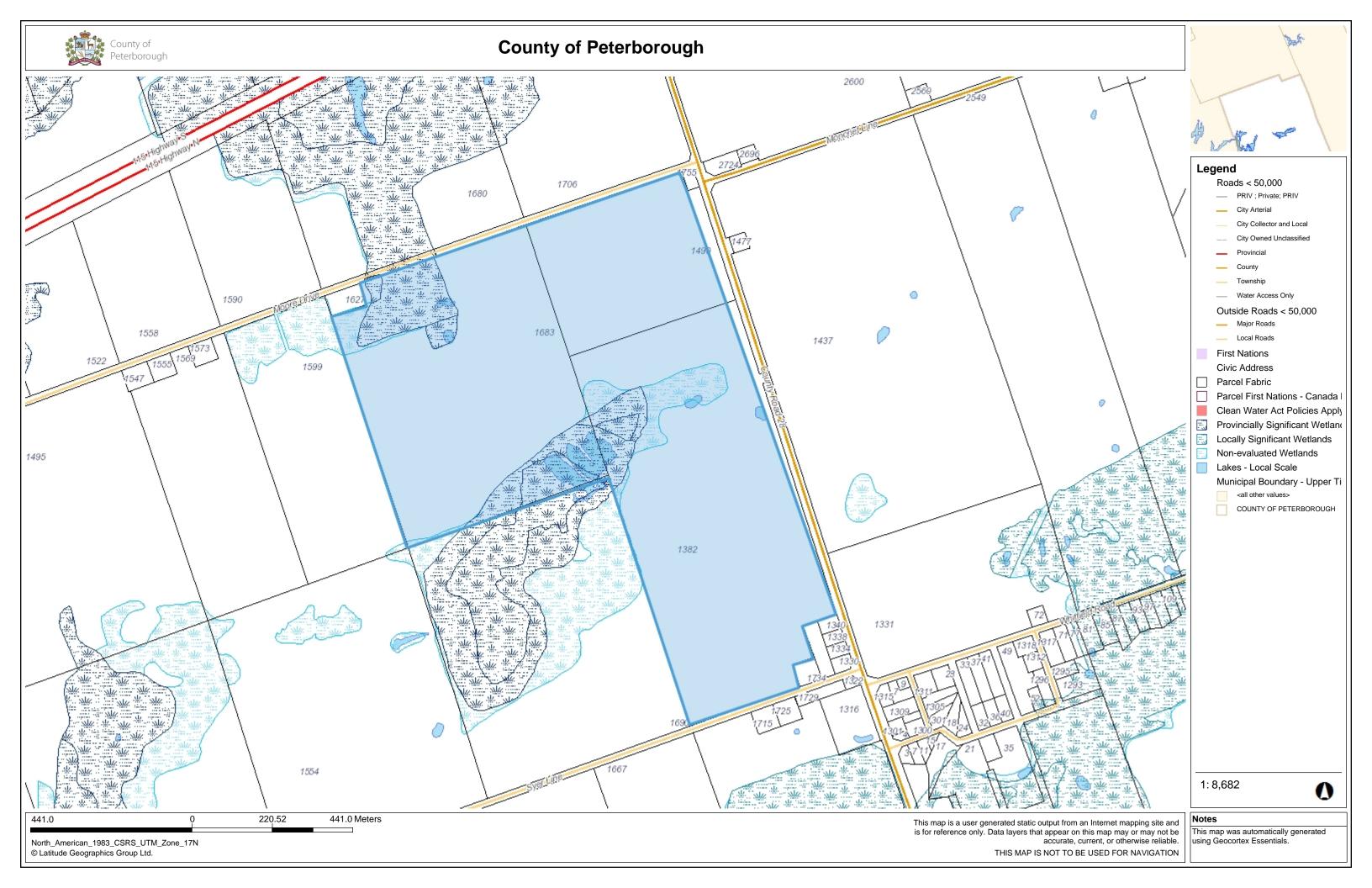






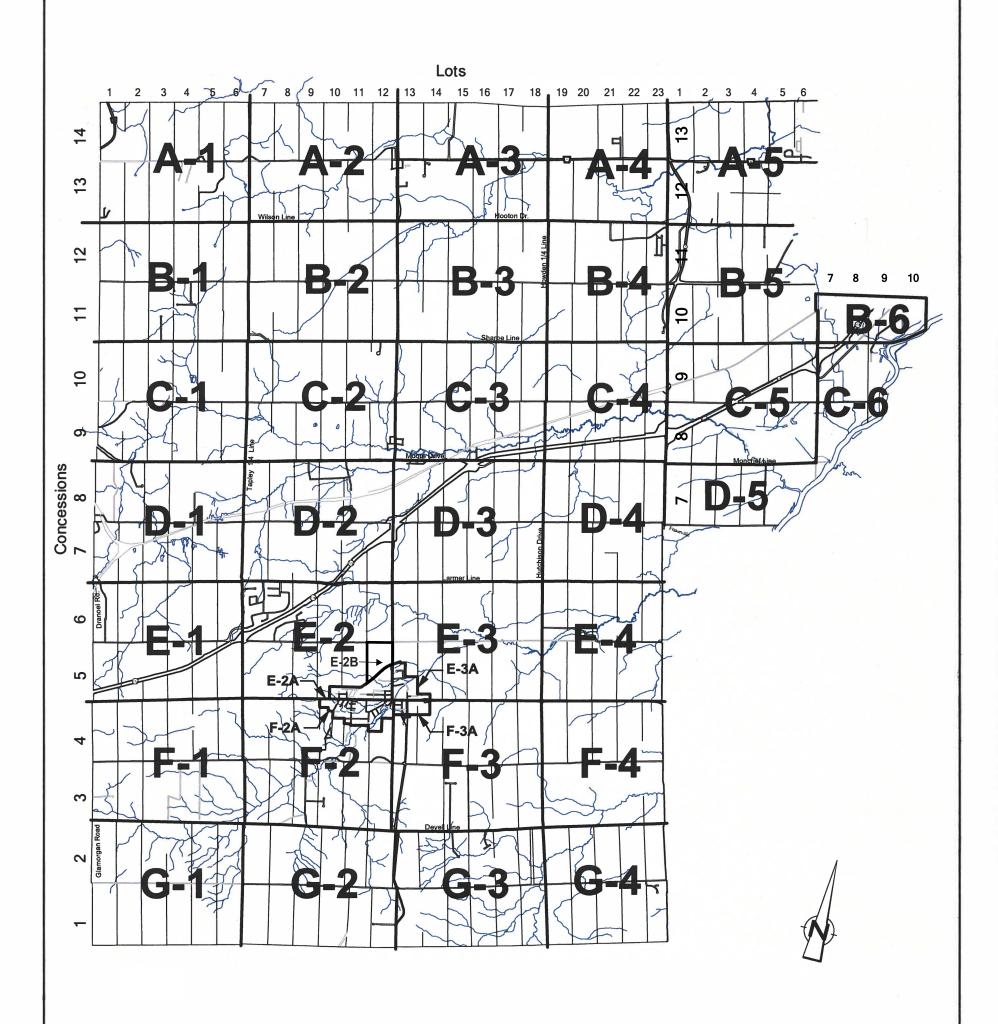
Appendix A

Land Information and Proposed Development Plan



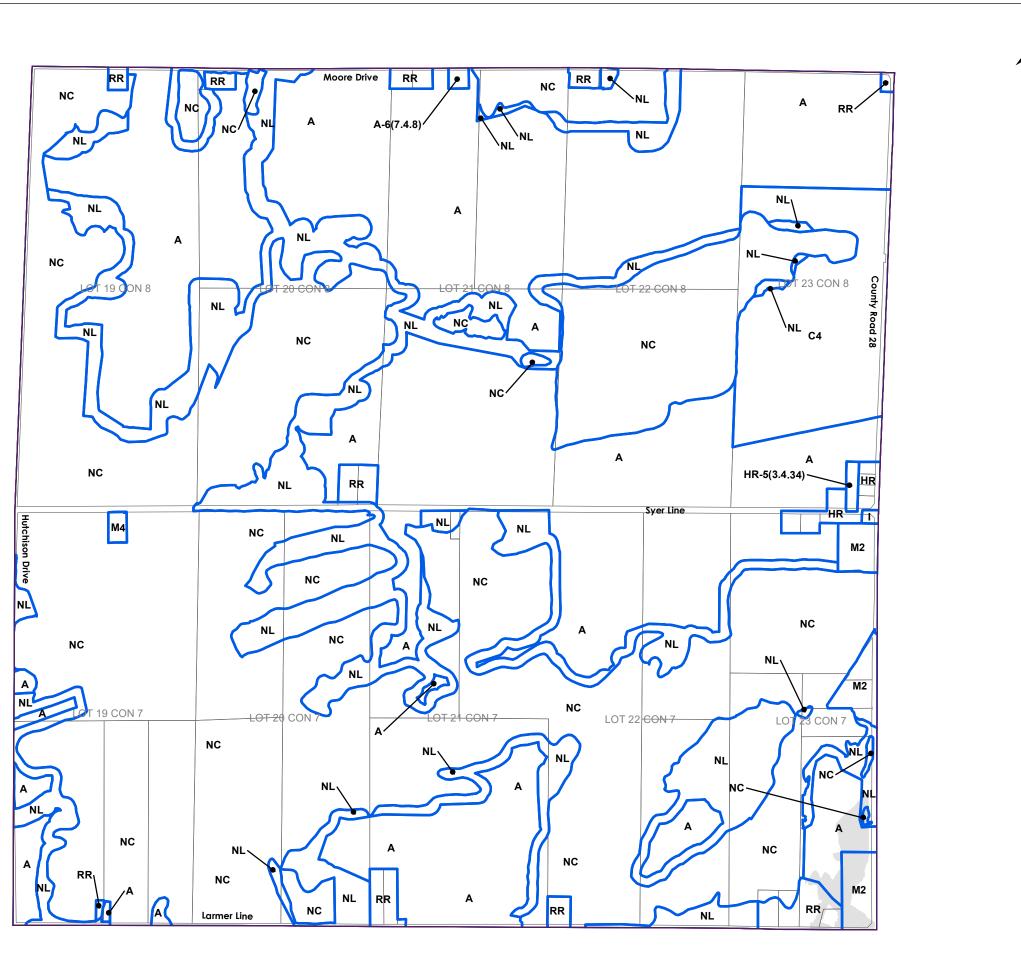
INDEX MAP Schedule A Zoning By-Law

Township of Cavan Monaghan By-Law No. 2018-58, as amended











.egena

Land Parcels

Zoning

Floodplain Overlay

Zone Description

A - Agricultural

C4 - Entertainment Commercial

HR - Hamlet Residential

I - Institutional

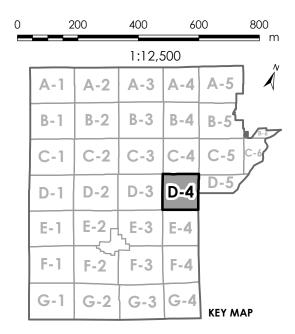
M2 - Rural Employment

M4 - Disposal Industrial

NC - Natural Core

NL - Natural Linkage

RR - Rural Residential

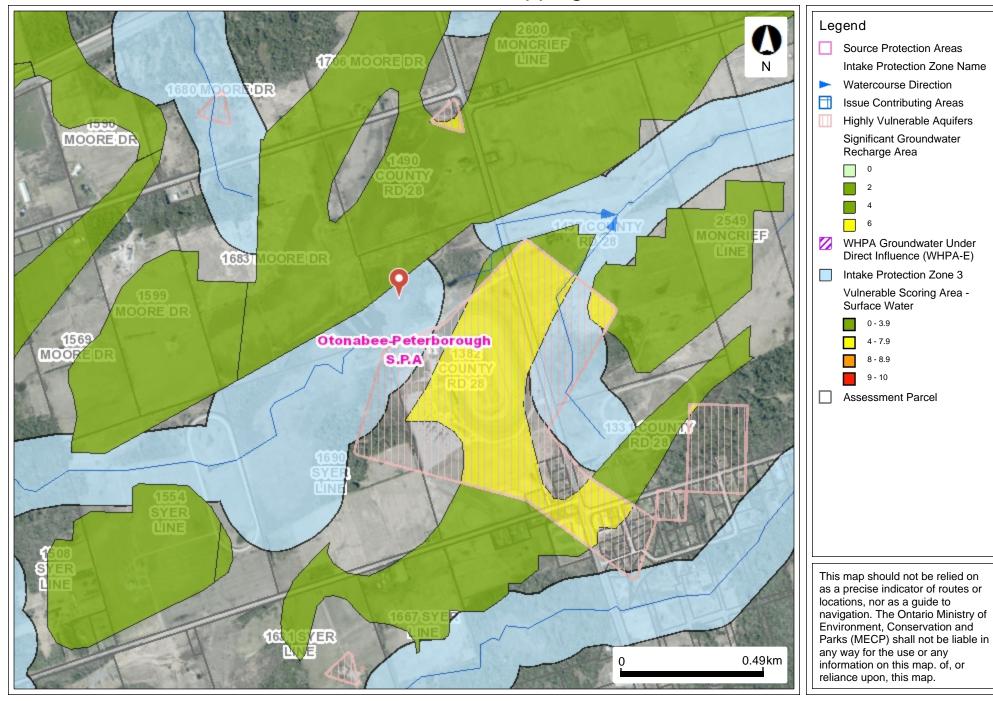


Schedule A Zoning By-law

Township of Cavan Monaghan Zoning By-law No. 2018-58

Map D-4

SPIA Mapping





Map Created: 3/23/2021

Map Center: 44.20943 N, -78.39505 W

Kawartha Downs

Map created: 3/5/2021

Notes: Enter map notes

Legend Woodland Provincial Park Natural Heritage System Provincially Significant Wetland Evaluated Non - Provincially Significant Unevaluated Wetland Area of Natural Heritage & Scientific Interest (ANSI)

Provincially Significant Life Science ANSI Provincially Significant Earth Science ANSI

Boundary - - Greenhelt External Connections Land Use Designations

Protected Countryside Greenbelt Towns and Villages

Urban River Valley Greenbelt Specialty Crop Area Niagara Escarpment Plan (NEP)

Boundary Parks and Open Space System Land Use Designations

Escarpment Protection Area

Escarpment Rural Area Mineral Resource Extraction Escarpment Recreation Area

Urban Area Minor Urban Centre

Oak Ridges Moraine Conservation Plan (ORM) Boundary

Land Use Designations Natural Core Area Natural Linkage Area

Countryside Area

Palgrave Estates Residential Community

Settlement Area

1.3 0.66

This map should not be relied on as a precise indicator of routes or locations, nor as a guide to navigation. The Ontario Ministry of Natural Resources and Forestry(OMNRF) shall not be liable in any way for the use of, or reliance upon, this map or any information on this map.

© Copyright for Ontario Parcel data is held by Queen's Printer for Ontario and its licensors [2020] and may not be reproduced without permission. THIS IS NOT A PLAN OF SURVEY.

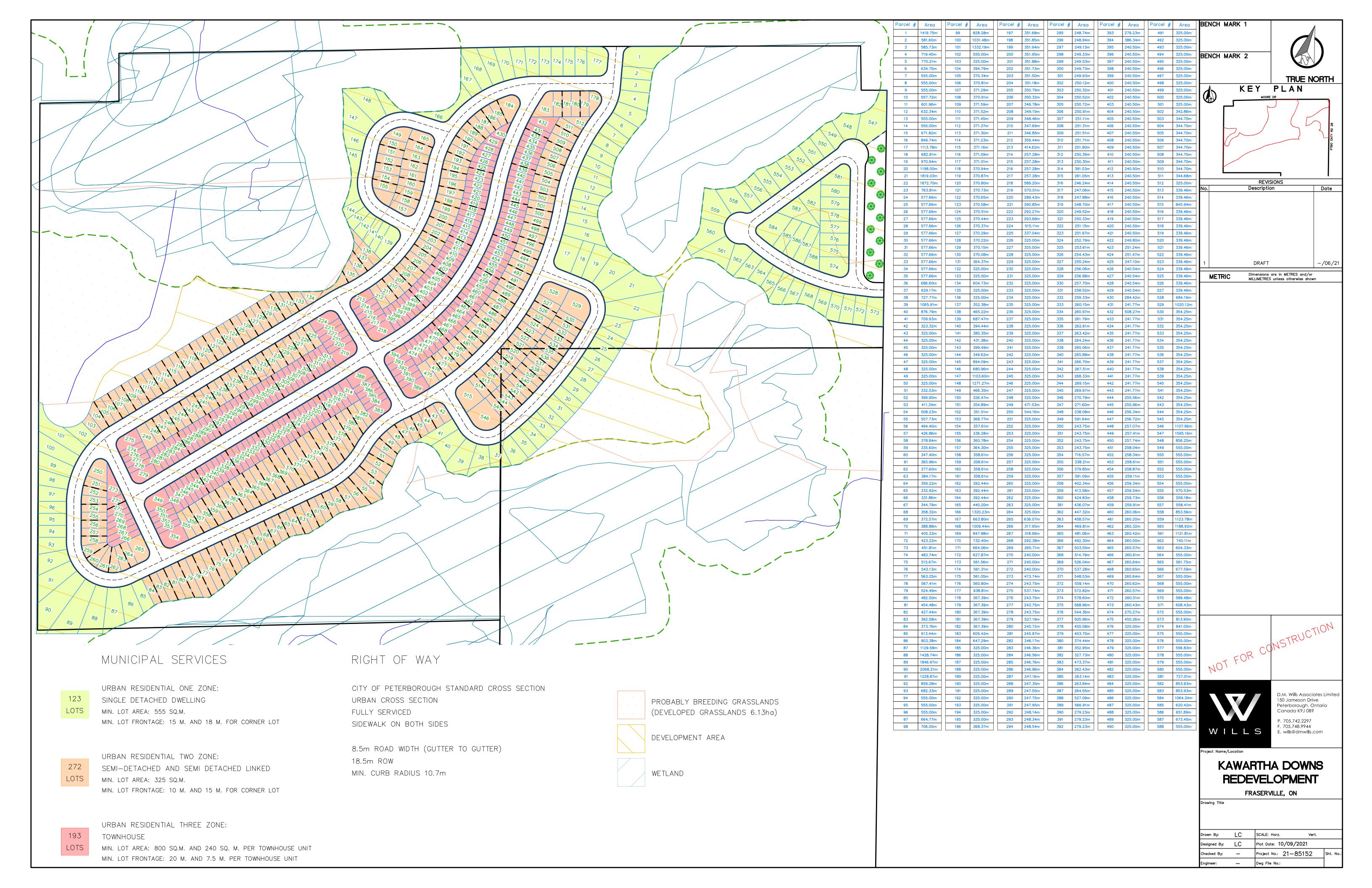
1.3 Kilometers

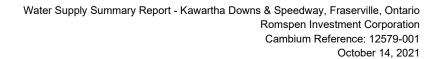
Fraserville

This map may not display all features listed in the legend because the feature layer was not turned on at the time the map was made; the features do not exist in the geographic range; or features have not been mapped. Absence of a feature in the map does not mean they do not exist in this area.

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| | | | | | Ap | pen | dix | В |
|------|-------|------|------|-------|------|-----|-----|----|
| МЕСР | Water | Well | Reco | ds fo | r Te | est | Wel | ls |

The Ontario Water Resources Act WATER WELL RECORD

Print only in spaces provided. Mark correct box with a checkmark, where applicable.

5119296 11

| Municipality | Con. | | _ | |
|--------------|------|--------|------|---|
| 151 n.24 | CON | | 0 | Ì |
| | 46 | 22 | 23 2 | 4 |

0506 (07/00) Front Form 9

| County or District | | | nip/Borough/City/ | Town/Villa | ge | | Con bloc | k tract survey | | ot 25-27 23 |
|---|---|---|-------------------------------|--------------------------------|--------------------------|--|---------------------|---------------------|--|-----------------------|
| Peterboro | ougn | Addres | an Twp. | | | K | OL IVO | Date | 20 1 | |
| | | Gene | eral Deli | very, | | ille, O | N . | completed | | month year |
| 21 | υ Τ | 1 1 1 1 1 | Northing | | RC Eleva | ation RC | Basin Code | e ii | 1 1 1 1 | 17 |
| 2 | LOG O | F OVERBURDI | EN AND BEDR | OCK MA | TERIALS (se | ee instructio | ons) | | _ | |
| General colour | Most common material | 1 | ther materials | | | | description | | From | oth - feet To |
| Black | Topsoil | | | | | | | | 0 | 1 |
| Brown | Sandy clay | | | | | | | | 1 | 5 |
| Brown | Sandy clay & grave | 1 | | | | | | | 5 | 12 |
| | Sandy clay & grave | | ders | | | | | | 12 | 19 |
| Gray Gray | Silty sand & grave | | clay, bou | lders | | | | | 19 | 471 |
| Gray | Limestone | | | | | | ····· | | 47 | 청 75 |
| Gray | DIMOCONO | | | | | | | <u> </u> | | |
| | | | | | | | | | <u> </u> | |
| | | | | | _ | .— | | | | |
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| | 1 | 1 | 1 1 1 1 | | 1 1 | 1.11 | . 1 1 . 1 | . 1 . 11 | . 11. | |
| 31 | | <u>. . </u> | <u> </u> | | <u> </u> | ┸┸┙┖┸┷ ┃╻┃┃╻╻ | <u>. . </u> | <u> </u> | _ | |
| 10 | 14 15 21 51 51 | CASING & | OPEN HOLE | L L | <u> </u> | Sizes of | | 31-33 Diameter | 34-38 Le | 75 e |
| Water found at - feet | Kind of water Inside | Material | Wall thickness | | oth - feet To | (Slot No. | | | inches | feet |
| 10-13 1 | ☐ Fresh 3 ☐ Sulphur 14 ☐ inche | | inches | | 13-16 | Material | and type | | Depth at to | op of screen 3 |
| 15.40 | Fresh 3 Sulphur 19 | 3 Concrete 4 Open hole | 100 | +2 ¹ / ₇ | 47 3 | | | | <u> </u> | feet |
| 2 | ☐ Salty 6 ☐ Gas 17-1 | 1 1 3 See | 19 | | 20-23 | | PLUGGIN Annular spa | G & SEALIN ∞ | G RECOF Abando | |
| | ☐ Fresh 3 ☐ Sulphur 24 ☐ Minerals ☐ Salty 6 ☐ Gas 6 | 2 ☐ Galvanize 3 ☐ Concrete 4 ☑ Open hole | İ | 47 1 | 75 | Depth set a | To M | aterial and type (C | ement grout, | , bentonite, etc.) |
| | ☐ Fresh 3 ☐ Sulphur 29 ☐ Selb. 4 ☐ Minerals 24: | 5 🗆 Plastic | 26 | 77.2 | 27-30 | O -13 | | entonite | | |
| 20.22 | □ Freeh 3 □ Sulphur 34 60 | 2 ☐ Gatvanize 3 ☐ Concrete | 1 | | | 18-21 26-29 | 22-25 30-33 80 | г | | *** |
| | ☐ Salty 6 ☐ Gas | 4 Open hole 5 Plastic | • | | | | | | | |
| | Monitor All I tumping the to | 1-14 Duration of pt | umping -16 ours 30 Mins | | | LO | CATION O | F WELL | | |
| Static lovel | Water level 25 Water levels during | IFM HO | 2 Recovery | | In diagrar Indicate r | m below sho | w distance w. | s of well from | road and | lot line. |
| 19-21 | end of pumping 22-24 15 minutes 30 minutes | , - | 60 minutes 35-37 | 11 | 1 | . . | | 1 | HWY 1 | 15 |
| 19-21 11 feet If flowing give | 74 17 15 | 13.5 feet | 12.5 _{feet} |] , | \mathcal{N} | | | | | |
| If flowing give | | Water at end | | | 7 | | | | | |
| Recommended | pump type Recommended | 43-45 Recommend pump rate | ded 46-49 | 1 | | | | | | |
| ☐ Shallow | Deep purify seturity 70 | feet | 10 дрм | } | Mo | ORE DR. | | | | |
| FINAL STATE | | ent supply ⁹ □ Un | finished | 1 | | 一个。 | , . | # 1683 | | |
| 1 ☐ Water su 2 ☐ Observa 3 ☐ Test hol | upply 5 ☐ Abandoned, insufficientation well 6 ☐ Abandoned, poor quale 7 ☐ Abandoned (Other) | | placement well | | | poo | | 100 | - 4WY 28 | 8 |
| 4 ☐ Recharg | ge well 8 Dewatering | | |] [| | | 000 | L | HWY 28 | |
| WATER USE | tic 5 🗆 Commercial | 9 D No | ot use her 7°51 | | | 0 | | $_{\Box}$ | MOR | Ne |
| 2 ☐ Stock 3 ☐ Irrigation | 6 ☐ Municipal n 7 ☐ Public supply | , | her 1837 | | | 150' | | 7 | 2. 7. | - (|
| 4 🗌 Industria | | y | | 1 | | | | 1 | | |
| 1 ☐ Cable to | CONSTRUCTION 57 pol 5 Air percussion | 9 🗆 Dr | | | | | | | | |
| ² ☐ Rotary (³ ☐ Rotary (⁴ 🔀 Rotary (| (conventional) ⁶ ☐ Boring | ¹⁰ □ Di ¹¹ □ O t | | | | | | | 25 | 237 7 |
| - UN Hotary (| (an) - Detung | · | | | | | | | | * * |
| Name of Well Cor | | 1 | tractor's Licence No | | Data source | 58 Contractor | 266 | 59-62 Date re | | 2003 |
| Address | Sons Well Drilling | LLU4 ZO | <u> </u> | <u> [</u> | Date of inspection | , | Inspector | | 190 | LUUJ |
| Box 850, | Fenelon Falls, ON | Well Tee | hnician's Licence No | NISTRY USE | Remarks | | 1 | | _ · · | |
| Bryan Wa | | T-2 | 441 | STR | | | | CC | e no | " |
| Signature of Tech | hnician/Contractor | Submiss | ion date | ΙĮŽ | | | | CD | S.ES. | 5 |

Signature of Technician/Contractor

Ministry of the Environment

The Ontario Water Resources Act WATER WELL RECORD

Print only in spaces provided.

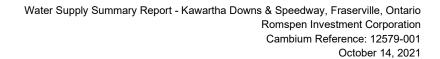
Mark correct box with a checkmark, where applicable.

<u>11</u> 5119297

| Municipality | Con. | 1 108 |
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0506 (07/00) Front Form 9

| County or District Peterboro | ough | | | Township/Bo | orough/City/To | wn/Villa | ge | | Con blo | ock tract survey | , etc. I | ot 25-27 23 |
|---|--|---|-----------------------|---|---------------------|--------------------|--------------------|--|-------------------------|----------------------|------------|-------------------------------------|
| | | | | Address General | l Delive | ery, | Fraserv | | 100 | completed | day | 11 02 ⁶⁻⁵³ month year |
| 21 | | Ŭ M | | | Northing | | RC Eleva | | Basin Co | de ii | | iv |
| 2 | | 10 | OG OF OVE | ERBURDEN A | ND BEDRO | CK MA | ATERIALS (se | ee instructio | ons) | | | |
| General colour | Most comm | non material | | Other r | materials | | | General | description | | From | oth - feet To |
| Black | Topsoil | - | | | | | | | | | 0 | 1 |
| Brown | Silty sa | and | | | | | | | | | 1 | 3 |
| Brown | Silty cl | lay | | | | | | | | | 3 | |
| Gray | Sandy cl | lay & g | ravel | | | | | | | | 8 | 21 |
| Gray | Silty sa | and & g | rave1 | some cla | ay | | wet | | | | 21 | 38 |
| Gray | Limestor | ne | | | | | | | | | 38 | 76 |
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| 31 | البلبليل | | | للسا | <u> </u> | سا ا | 1111 | ـــالـــــــــــــــــــــــــــــــــ | لبلب | | | |
| | 14 15 | 21 | | 32 | <u> </u> | 43 | | 54 Sizes of | onesina | 31-33 Diameter | 34-38 [4 | 75 8 |
| Water found | ER RECORD Kind of water | | Inside | ASING & OPE | Wall thickness | | oth - feet | | | Diameter | inches | feet |
| at - feet | Y Fresh 3 □ Sulp | hur 14 | diam inches | Material 12 | inches | From | To 13-16 | (Slot No. | and type | | Depth at t | op of screen 41-44 |
| 38 And | Salty & Gas | | 2 3 | Galvanized | .188 | +2 1 /2 | 38 | [6] | | | | feet |
| | ☐ Fresh 3 ☐ Sulp ☐ Salty 6 ☐ Gas | erals | 5 🗆 | Plastic | .100 | +4 2 | 20-23 | | | NG & SEALING | G RECOI | |
| | ☐ Fresh ³ ☐ Sulp ☐ Salty 5 ☐ Gas | erals | 2 | Galvanized Concrete | | 38 | 76 | Depth set a | | Material and type (C | | |
| | □ Freeh 3 □ Sulp | ohur 29 | 5 - | Open hole Plastic | | | | 10(1)s | 70 20 ⁷ I | Bentonite | | |
| 20 22 | ☐ Salty 6 ☐ Gas | | 2 | Steel ²⁶ Galvanized Concrete | | | 27-30 | 18-21 | 22-25 | | | |
| 1 1 | ☐ Fresh 4 ☐ Mind ☐ Salty 6 ☐ Gas | erals | 4 [| Open hole Plastic | | | | 26-29 | 30-33 80 | | | |
| _ Pumping test r | method Air Pu | mping rate 12 | 11-14 D | Ouration of pumping | 920 1718 | | - 009 | LOG | CATION | OF WELL | | |
| 71 : □ Pump 2 | Baller 25 | · · · · · · · · · · · · · · · · · · · | u w | | Recovery | | In diagrar | n below show | w distance | es of well from | road and | lot line. |
| | end of pumping | Water levels du minutes 30 26-28 | _ | , | 60 minutes 35-37 | ١, | Indicate n | orth by arrov | w. | HWY# 115 | | |
| 5 10 feet | | 25 feet | 21 feet | 18.5 | 17 feet | | ○ 1 | | | ···· | HWY | 28 |
| If flowing give | 20.41 | mp intake set at | | Vater at end of test | 42 ☐ Cloudy | | 1 | | | | Hw. | |
| Hecommended | pump type Re | commended mp setting | 43-45 | Recommended | 46-49 | | m | luore DR. | | | | |
| ☐ Shallow | Deep Pu | | feet | | GPM | | - | 150] | N | | | |
| FINAL STATU | | 54 | | | | | | 150) | | | Mo | NCTIEF LINE. |
| 1 ☐ Water su 2 ☐ Observa 3 🛪 Test hole 4 ☐ Recharge | upply 5 ∐ ution well 6 □ e 7 □ | Abandoned, ir Abandoned, p Abandoned (C | oor quality | ly ⁹ ☐ Unfinishe ¹⁰ ☐ Replacen | | | | 4 | 20 | | | LINE. |
| Recharge | je well 8 🗀 | Dewatering | · - <u></u> := | | | | | | I | * | | |
| WATER USE | c 5 🗆 | 55-56 Commercial | | 9 ☐ Not use | ald the | | | | | | | |
| 2 ☐ Stock 3 ☐ Irrigation 4 ☐ Industria | 7 🗆 |] Municipal] Public supply] Cooling & air (| conditioning | 10 X 1 Other / | J. J.W. | | | | | | | |
| | CONSTRUCTION | ON 57 | | | | | | | | | | |
| 1 ☐ Cable to | ool ⁵ 💆 | Air percussion Boring | 1 | 9 ☐ Driving 10 ☐ Digging | | | | | | | | |
| 3 Rotary (i | reverse) 7 🗆 | Diamond Jetting | | 11 Other | | | | | | | 25 | 2375 |
| | | | | Well Contractor | e Licence No. | <u> </u> | Data | 58 Contractor | | 59-62 Date re | ceived | 63-68 |
| Name of Well Con G. Hart & | Sons Well | Drill: | ing Ltd | | | | ource | 58 Contractor | 66 | 2 FEE | 3 19 | 2003 |
| Address | Fenelon F | | | | | USE | Date of inspection | | Inspector | | | |
| Name of Well Tec | chnician | | | Well Technician | n's Licence No. | RY L | Remarks | | | | | |
| Bryan Watson Signature of Technician/Contractor | | | T-2441 Submission dat | le l | MIST | Remarks CSS.ES3 | | | | | | |





| | App | endix | C |
|-------------|------|--------|----|
| AquiferTest | Pro™ | Result | ts |



194 Sophia St. Peterborough, ON K9H1E5

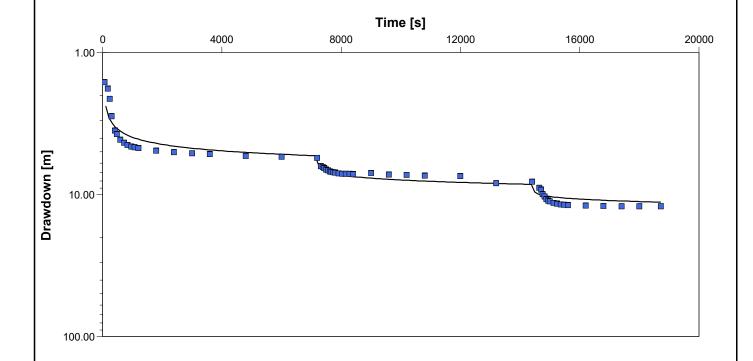
Pumping Test Analysis Report

Project: Water Supply Assessment, Kawartha Downs

Number: 12579-001

Client: Romspen Investment Corporation

| Location: Kawartha Downs, Fraserville, ON | Pumping Test: Pumping Test - Well 1 | Pumping Well: Well 1 | | |
|---|---|--------------------------|--|--|
| Test Conducted by: C. Kinsella | Test Date: 9/16/2021 | | | |
| Analysis Performed by: N. Heikoop | Pumping Test - Well 1 | Analysis Date: 10/6/2021 | | |
| Aquifer Thickness: 8.38 m | Discharge: variable, average rate 11.278 [U.S. gal/min] | | | |



Calculation using Hantush Observation Well Transmissivity Hydraulic Storage Hydr. Leakage factor Radial Conductivity coefficient resistance Distance to PW [m²/s] [m/s] [s] [m] [m] 5.66×10^{-5} 6.75×10^{-6} 8.12×10^{-2} 9.40×10^{3} 5.01×10^{11} 5.32×10^{3} Well 1 0.08



194 Sophia St. Peterborough, ON K9H1E5

Pumping Test Analysis Report

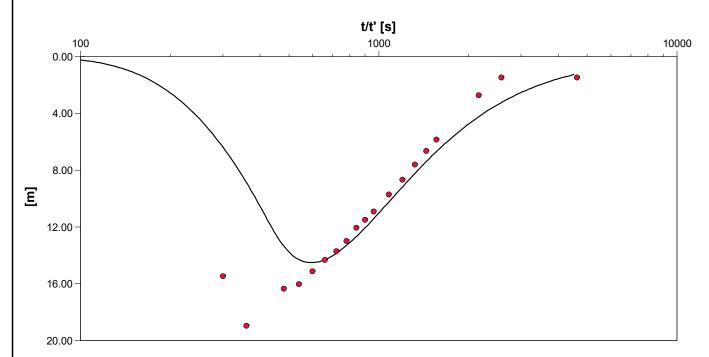
Project: Water Supply Assessment, Kawartha Downs

Number: 12579-001

Client: Romspen Investment Corporation

| Location: Fraserville, ON | Pumping Test: Pumping Test - Well 2 | Pumping Well: Well 2 | | |
|-----------------------------------|--|--------------------------|--|--|
| Test Conducted by: C. Kinsella | | Test Date: 9/17/2021 | | |
| Analysis Performed by: N. Heikoop | Pumping Test - Well 2 | Analysis Date: 10/6/2021 | | |
| Aguifer Thickness: 11.33 m | Discharge: variable, average rate 17.17 [LLS, gal/min] | | | |

Promargo, variable, average rate 17.17 [e.e. gammin]



| Calculation | usina | Theis |
|-------------|-------|--------|
| Calculation | using | 111013 |

| Observation Well Transmissivity | | | Storage coefficient | Р | Radial Distance to |
|---------------------------------|-------------------------|-------------------------|-------------------------|------------------------|--------------------|
| | | Conductivity | | | PW |
| | [m²/s] | [m/s] | | | [m] |
| Well 2 | 2.03 × 10 ⁻⁶ | 1.79 × 10 ⁻⁷ | 5.21 × 10 ⁻¹ | 2.60 × 10 ⁰ | 0.08 |