

**Preliminary  
Stormwater Management Report**

**Life at the Woodland  
Township of Otonabee-South  
Monaghan  
County of Peterborough**

**Residential Subdivision Development**

**D.M. Wills Project No. 19-10874**



**D.M. Wills Associates Limited**

Partners in Engineering, Planning and  
Environmental Services  
Peterborough  
Bancroft

**February 2022**

**Prepared for:  
Life at the Woodland Inc.**

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## 1.0 Purpose

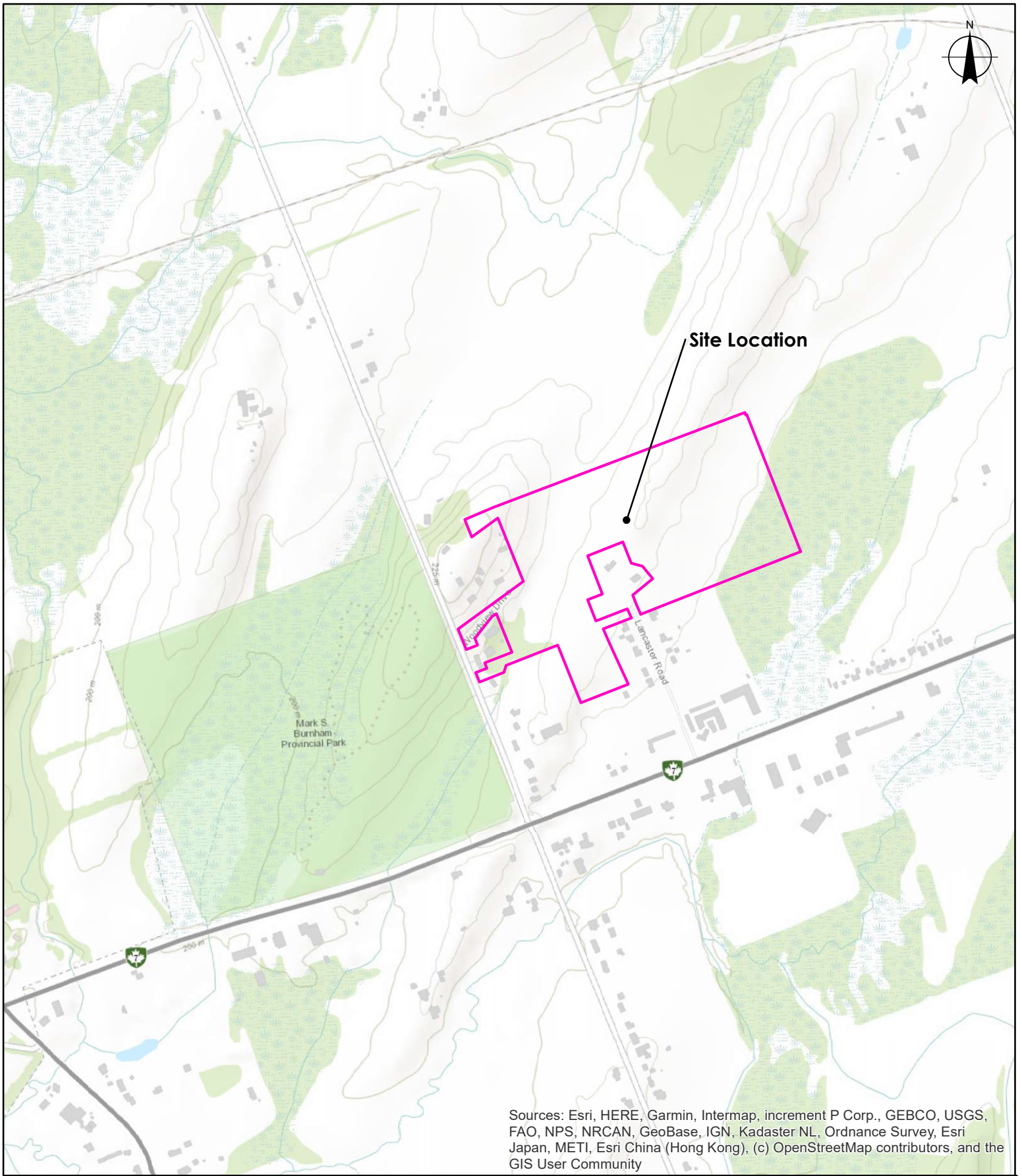
D.M. Wills Associates Limited (Wills) has been retained by Mr. Rubal Kundra of Life at the Woodland Inc. to prepare a Preliminary Stormwater Management Plan and Report for the proposed residential subdivision located on Part of Lot 27, Concession 10, Township of Otonabee-South Monaghan in the County of Peterborough.

The purpose of this report is to evaluate the impact of the proposed development on the stormwater runoff and to develop a preliminary plan for stormwater management that will permit the development to proceed with no adverse impacts to the receiving drainage systems. This report has been prepared specifically for the County of Peterborough (County) and the Otonabee Region Conservation Authority (ORCA) to address stormwater management for the development and to satisfy the statutory requirements.

## 2.0 Site Description

The subject property is located in the township of Otonabee-South Monaghan with access provided from Burnham Line, situated approximately 6 kilometres east of Peterborough. The subject site is legally described as a Part of Lot 27, Concession 10 in the Township of Otonabee-South Monaghan in the County of Peterborough and is approximately 17.67 ha in area. The property is bounded by agricultural land use to the north, Burnham Line and wooded area to the west, wetland and wooded area to the east and residential lots accessed by Lancaster Road to the south. An unevaluated wetland feature is located in the western portion of the property, which drains to two separate outlets. The location of the site is shown on **Figure 1**.

The proposed residential subdivision consists of twenty-seven (27) lots adjacent to the wetland buffer. The portion of the site within the wetland buffer is to remain in an undisturbed natural state. The development of the site will require the removal of vegetated areas and grasslands. A cul-de-sac roadway off Burnham Line will provide access for the proposed lots.



Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community

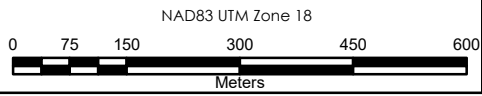
**Figure 01  
Location Plan**



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**Legend**  
— Property Limits

Drawn by: RC	Scale (Horz.)  1:10,000
Checked by: CPB	
Engineer: RC/CPB	Map Date Dec 2021
Project No. 10874	Map File No. 10874-DP01



According to the Soil Survey Complex of Ontario, the subject site is primarily composed of two types of surficial soils. The wetland portion of the site is composed of Foxboro Silt Loam with the remainder of the site composed of Otonabee Loam. According to the SCS method of classifying soils, these types of surficial soils correspond to Hydrologic Soils Groups C and B respectively.

A topographic survey of the subject property was completed by JBF Surveyors Ltd. (Project #7369) with the latest drawing version dated January 13, 2020, to determine existing elevations and the location of drainage features on the site. This information was used to determine drainage patterns and preliminary catchment area characteristics. A digital elevation model of the wetland was obtained from the South Central Ontario Orthophotography (SCOOP) under Land Information Ontario (LIO) database. The horizontal datum for the SCOOP is projected in UTM Zone 17 of the NAD83 Canadian Spatial Reference System and the vertical datum is sourced CGVD28. The SCOOP DEM raster has a resolution of 20 cm, however it was resampled into a raster cell of size 2 m. This data was produced to meet ASPRS Positional Accuracy Standards for Digital Geospatial Data (2014) with +/- 46.0cm actual VVA accuracy at the 95<sup>th</sup> percentile.

### 3.0 Methodology

The present hierarchy of watershed planning in Ontario can be described by the following in descending order: Watershed Plans, Sub-watershed Plans and individual Stormwater Management Plans. There is no Master Plan directing the stormwater management strategy for this watershed. As such, the proposed development was prepared as an individual Preliminary Stormwater Management Plan.

#### 3.1 Site Specific Stormwater Design Criteria

A pre-consultation meeting was held to discuss the requirements of the Draft Plan Approval process. The following design criteria have been established from the pre-consultation meeting and with follow-up correspondence from the County and ORCA.

- To provide stormwater quality controls, to achieve “Enhanced” Level 1 protection as defined in the Stormwater Management Planning and Design Manual (March 2003).
- To provide stormwater quantity controls, to reduce the post development peak flow rates to the existing condition peak flow rates at each outlet location, for the 2 to 100-year design storms.
- To respect the recommended statutory setback requirements provided by the regulatory agency for the unevaluated wetland located within the property.
- To incorporate Low Impact Development (LID) features as part of the proposed stormwater management strategy.

### 3.2 Catchment Area Characterization

For the purpose of the preliminary SWM plan, the site will be analyzed as six (6) catchment areas based on the site topography under existing conditions. The existing catchment areas are shown on **Figure 2**. The internal wetland area will remain undisturbed and has not been included in the analysis.

- Catchment area **EX-100** consists of 2.02 ha of land and includes the northwestern portion of the subject site and neighboring lots. This catchment consists of the current gravel access to the site from Burnham Line, wooded areas and rural residential lots. Runoff from this catchment currently flows overland to the wetland, discharging to **OUT-1 WEST**.
- Catchment area **EX-101** consists of 1.42 ha of land and includes the southwest portion of the site. This catchment is comprised of woodlots and grassed areas. Runoff from this catchment will flow overland northerly to the wetland, discharging to **OUT-1 EAST**.
- Catchment area **EX-200** consists of 1.53 ha of land and includes the northern portion of the site. This catchment is comprised of wooded areas and neighboring residential rear yards. Runoff from this catchment will flow overland towards the wetland, discharging to **OUT-2 WEST**.
- Catchment area **EX-201** consists of 2.44 ha of land and includes the north central portion of the site. This catchment consists of wood lots and grassed areas. Runoff from this catchment will drain northerly towards the wetland, discharging to **OUT-2 EAST**.
- Catchment **EX-300** consists of 8.72 ha of land located in the eastern portion of the site. This catchment is comprised of extensive grassed range type areas with a band of wooded areas and wetland area. The runoff generated within this catchment drains southeasterly to an unidentified wetland located southeast of the site (**OUT-3**).
- Catchment **EX-400** consists of 1.24 ha of land located in the south central portion of the subject property west of Lancaster Road. This catchment is comprised of grassed range with some wood pockets. The runoff generated within this catchment drains southerly overland towards the private properties on Lancaster Road (**OUT-4**).

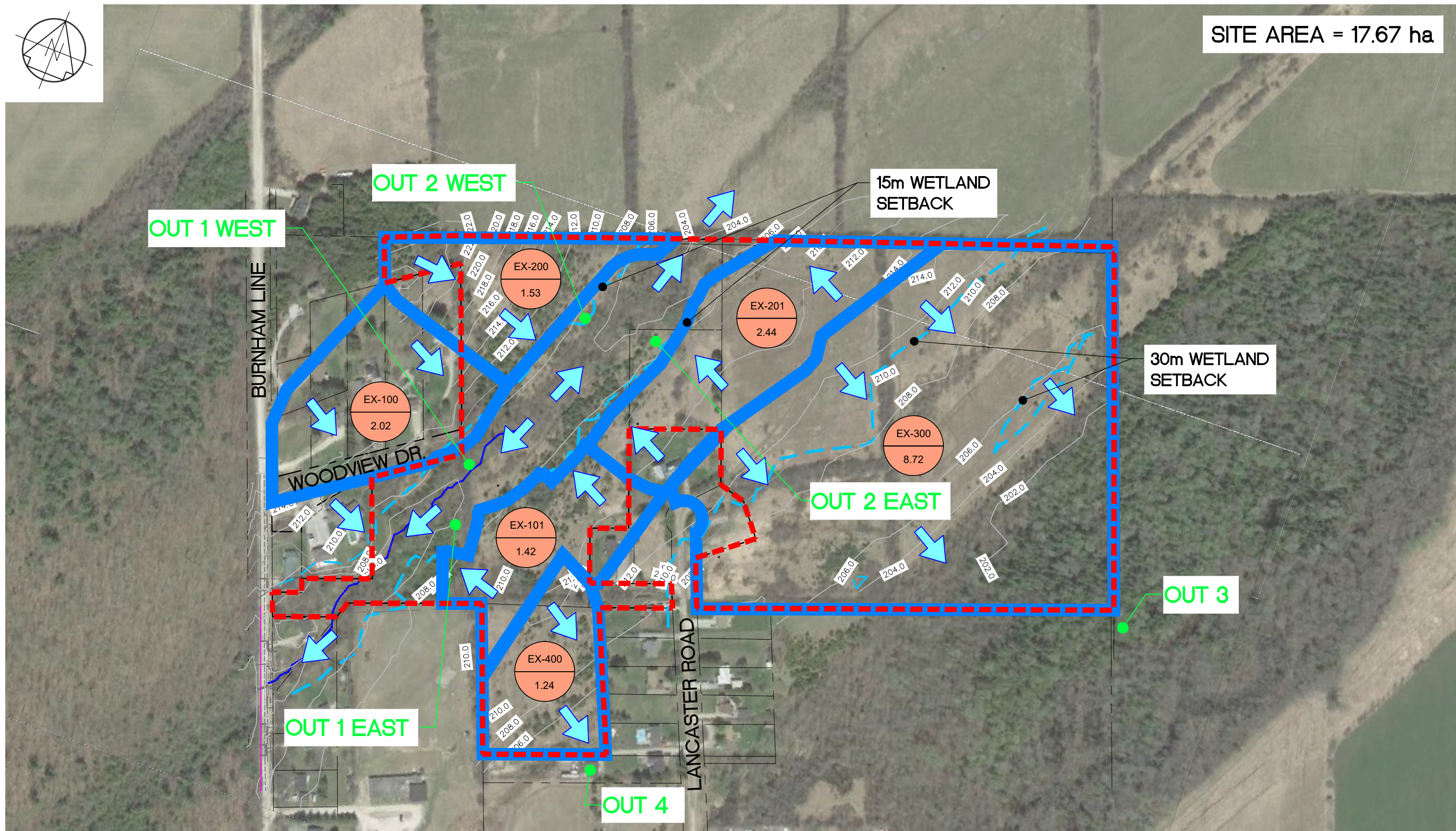
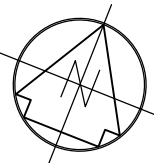
Under the proposed condition, the catchment areas subject to land use change were delineated into eight (8) sub-catchment areas as shown on **Figure 3**.

- Catchment area **PR-100** consists of 2.66 ha of land and includes the northwest neighboring lots and proposed access road from Burnham Line. Runoff from this catchment will flow overland towards a proposed SWM facility for treatment and will then outlet to the wetland, discharging to **OUT-1 WEST**.
- Catchment area **PR-101** consists of 0.59 ha of land comprised of the rear lot yards located west of the proposed cul-de-sac. Runoff from this catchment will

drain uncontrolled towards the wetland as in the existing condition, discharging to **OUT-1 EAST**.

- Catchment area **PR-102** consists of 1.48 ha of land and includes the southern portion of the developed site comprised of the proposed roadway and cul-de-sac, and a portion of the proposed residential lots. Runoff from this catchment will flow overland to a proposed SWM facility for treatment and will then outlet to the wetland, discharging to **OUT-1 EAST**.
- Catchment area **PR-200** consists of 0.75 ha of land and includes the northern portion of the subject site. This catchment is comprised of proposed lots and a portion of the proposed roadway. Runoff from this catchment will drain towards a proposed SWM facility and will outlet to the wetland, discharging to **OUT-2 WEST**.
- Catchment area **PR-201** consists of 1.28 ha of land and includes a portion of the proposed roadway and residential lots. Runoff from this catchment will drain towards a proposed SWM facility and will outlet to the wetland, discharging to **OUT-2 EAST**.
- Catchment area **PR-202** consists of 1.40 ha of land and includes the northeastern portion of the site, consisting of the proposed roadway and lots. Runoff from this catchment will flow overland towards the wetland, discharging to **OUT-2 EAST**.
- Catchment **PR-300** consists of 8.50 ha of land includes the eastern portion of the site. This catchment is comprised of proposed lots and the existing wetland to the east. Runoff generated from this catchment will drain overland easterly to the existing wetland area (**OUT 3**) as in the existing condition.
- Catchment **PR-400** consists of 0.58 ha of land and includes the southern tip of the property, consisting of the rear yards of the proposed lots. Runoff from this catchment will drain overland, south easterly towards Lancaster Road as in the existing condition (**OUT 4**).

SITE AREA = 17.67 ha



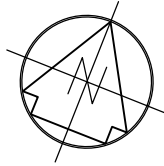
	CATCHMENT ID		WETLAND SETBACK		OUTLET LOCATION
	CATCHMENT AREA (ha)		SUBJECT PROPERTY LINE		OVERLAND FLOW DIRECTION
	CATCHMENT BOUNDARY				

Sketch No.  
**FIGURE 2**  
 LIFE AT THE WOODLAND  
 EXISTING DRAINAGE  
 AREA PLAN



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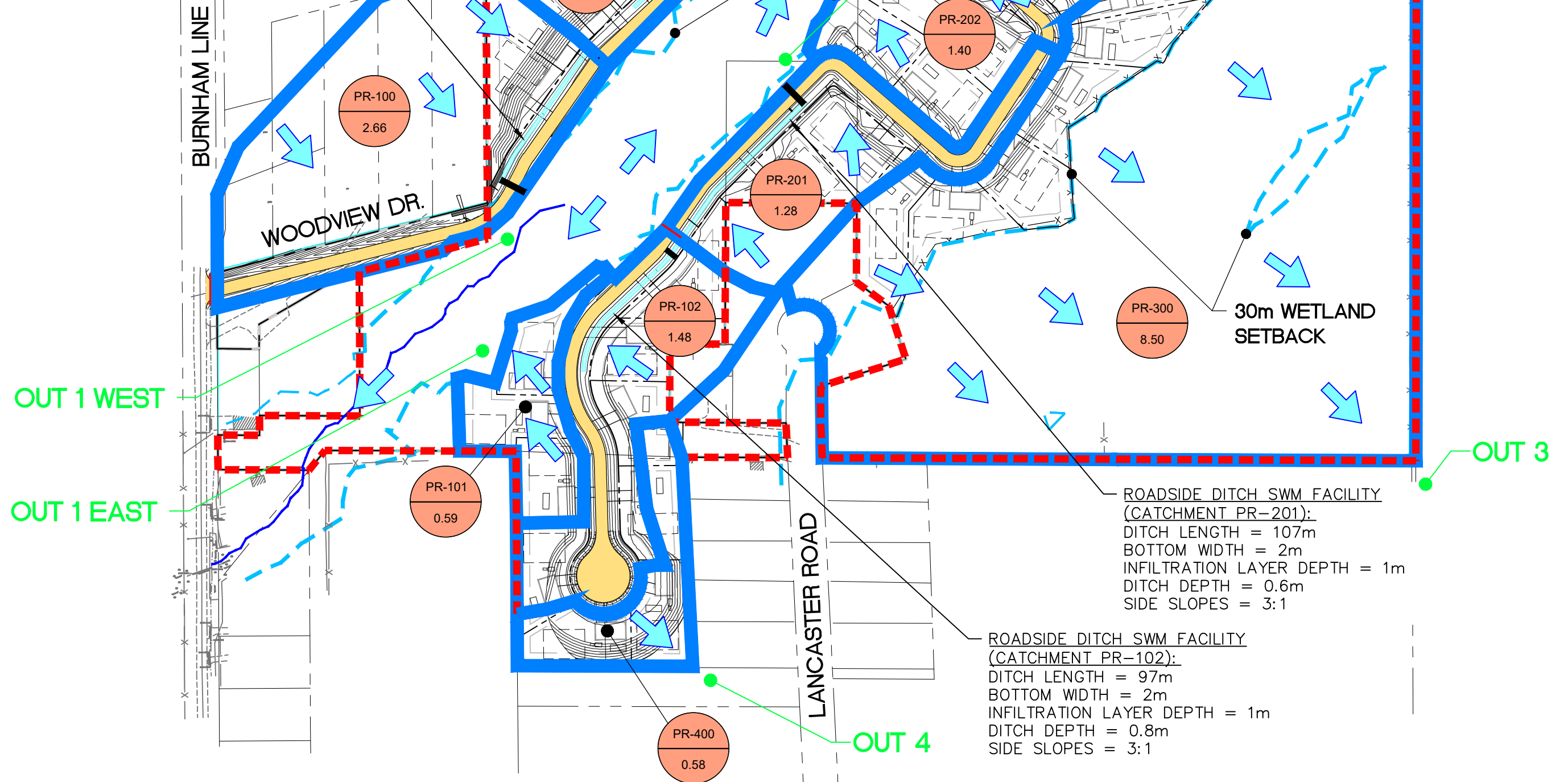
Drawn By	RC	Scale	1: 3000
Designed By	RC	Plot Date	FEB 2022
Checked By	CPB	Project No.	19-10874
Engineer	RC/CPB	Drawing File No.	SWM FIGURE 2



ROADSIDE DITCH SWM FACILITY  
(CATCHMENT PR-100):  
DITCH LENGTH = 90m  
BOTTOM WIDTH = 2m  
INFILTRATION LAYER DEPTH = 1m  
DITCH DEPTH = 0.6m  
SIDE SLOPES = 3:1

ROADSIDE DITCH SWM FACILITY  
(CATCHMENT PR-200):  
DITCH LENGTH=50m  
BOTTOM WIDTH=2m  
SIDE SLOPES=3:1  
INFILTRATION LAYER DEPTH = 0.5m

SITE AREA = 17.67 ha



PR-100 CATCHMENT ID  
0.22 CATCHMENT AREA (ha)  
CATCHMENT BOUNDARY

WETLAND SETBACK  
SUBJECT PROPERTY LINE

OUT OUTLET LOCATION  
OVERLAND FLOW DIRECTION

Sketch No.  
FIGURE 3  
LIFE AT THE WOODLAND  
PROPOSED DRAINAGE  
AREA PLAN



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Drawn By RC  
Designed By RC  
Checked By CPB  
Engineer CPB

Scale 1:2500  
Plot Date FEB 2022  
Project No. 19-10874  
Drawing File No. SWM FIGURE 3

The hydrologic parameters used for each catchment area, in both existing and proposed conditions, are summarized **Table 1** and documented in **Appendix A**.

**Table 1 – Existing and Proposed Hydrologic Parameters**

Standhyd <sup>1</sup>						
Catchment ID	Area (ha)	Impervious %	CN* <sup>2</sup>	Ia <sup>3</sup>	Pervious Slope (%)	Impervious Slope (%)
PR-102	1.48	23	60.7	5.3	5.0	2.0
PR-201	1.28	24.6	62.5	5.8	6.6	1.0

Nashyd <sup>1</sup>					
Catchment ID	Area (ha)	Impervious %	CN* <sup>2</sup>	Ia <sup>3</sup>	Tp <sup>4</sup> (hrs)
EX-100	2.02	1.9	61.5	5.3	0.17
EX-101	1.42	2.4	63.1	9.1	0.22
EX-200	1.53	0.0	61.7	8.7	0.17
EX-201	2.44	0.7	68.8	8.0	0.17
EX-300	8.72	0	64.6	8.8	0.39
EX-400	1.24	0	67.5	8.2	0.26
PR-100	2.66	9.7	64.8	4.8	0.17
PR-101	0.59	10.0	65.0	4.7	0.17
PR-200	0.75	16.1	68.1	7.4	0.17
PR-202	1.40	14.8	67.1	4.6	0.17
PR-300	8.50	1.6	64.4	8.4	0.39
PR-400	0.58	12.1	66.1	4.6	0.26

- Notes:
1. Command Line refers to the unit hydrograph used in the VO3 hydrologic model for the respective catchment area.
  2. CN\* refers to the modified CN number adjusted to Antecedent Moisture Conditions II. Excludes Impervious Area for Standhyd.
  3. Ia refers to Initial Abstraction. Excludes Impervious Area for Standhyd.
  4. Tp refers to Time of Peak.

Hydrologic parameters such as soil infiltration properties, land use and runoff response were determined based on aerial photography, site reconnaissance and literature review. Topographic mapping and AutoCAD Civil 3D 2019 software were used to establish sub-catchment areas, land use and slopes. Rainfall data for the site is taken from the City of Peterborough Engineering Design Standards (April 2019) and is included in **Appendix A**.

## 4.0 Stormwater Management

### 4.1 Low Impact Development Design

As the practice of stormwater management has evolved, increasing emphasis has been placed on utilizing a treatment train approach to manage runoff as close to the source as possible. This design philosophy is often referred to as Low Impact Development (LID), where the ultimate goal is to maintain and mimic the natural hydrologic conditions. LID designs accomplish this by reducing the runoff volume generated by a site and implementing features that infiltrate, filter, evaporate, harvest and detain runoff, while also preventing pollution. ORCA encourages the use of LID features as part of the water quality design for a site and, therefore, opportunities to utilize these features have been investigated.

For infiltration based LID features, a minimum separation of 1.0 m is required from the bottom of feature to the higher of the seasonally high groundwater or bedrock elevation. As such, a geotechnical study with in-situ infiltration testing will ultimately be required to confirm the availability of minimum separation and observed infiltration rates.

LID features must also include an underdrain for infiltration rates less than 15 mm/hr. Sandy loam soils typically have infiltration rates from 30 to 50 mm/hr. and therefore underdrains are not anticipated to be required. This assumption can be confirmed once the in-situ infiltration rates have been established during detailed design.

A variety of LID features were considered for the development and evaluated based on site constraints, capital cost, maintenance considerations and water quality benefits. The preferred design selected are stone filled infiltration trenches with detention storage provided above the infiltration portion where required. These features will be incorporated as part of the roadside ditch system. The SWM facilities have been designed to achieve the necessary quality control targets.

### 4.2 Stormwater Quality Control

The proposed subdivision may cause additional pollutants to be conveyed off site. As such, the selection and sizing of the water quality measures are based on the procedures set out in the Stormwater Management Planning and Design Manual (MOE, March 2003) for Enhanced (Level 1) protection. As such, the goal of SWM is to preserve the natural hydrologic cycle. In addition, SWM measures should be assessed in the following order:

- Stormwater lot level controls
- Stormwater conveyance controls
- End-of-pipe SWM facilities

Stormwater lot level controls represent measures that are implemented on an individual lot basis such as soak-a-way pits, flatter grading and reduction of the impervious footprint.

Stormwater conveyance controls represent the conveyance systems used to transport stormwater runoff from the lots to the receiving waters such as pervious pipes, catchbasin treatment and grassed swales.

End-of-pipe SWM facilities represent the common urban SWM measures used to service numerous lots or whole subdivisions including wet ponds, wetlands, dry ponds, infiltration based facilities, Oil-Grit separators and filter systems.

#### 4.2.1 Quality Control Summary

A SWM assessment was completed to evaluate the most appropriate measures to provide stormwater quality treatment for the proposed development. The following table summarizes the feasibility of each option for the proposed development.

**Table 2 – Quality Control Feature Options Summary**

Facility Description	Comments and Feasibility
<b>Lot Level Controls</b> <ul style="list-style-type: none"> <li>• Soak-Away Pits</li> </ul>	<ul style="list-style-type: none"> <li>• Not a feasible option as a standalone <b>water quality</b> control for roadway runoff.</li> </ul>
<b>Conveyance Controls</b> <ul style="list-style-type: none"> <li>• Pervious pipes</li> <li>• Catchbasin treatment</li> <li>• Grass Swales</li> </ul>	<ul style="list-style-type: none"> <li>• Feasible option for <b>water quality</b> control.</li> <li>• Grassed swales can be considered as a viable option in combination with infiltration features to provide the necessary <b>water quantity control</b>.</li> </ul>
<b>End-of-Pipe Controls</b> <ul style="list-style-type: none"> <li>• Wetlands</li> <li>• Wet Ponds</li> <li>• Dry Ponds</li> <li>• Infiltration Basins</li> <li>• Infiltration Trenches</li> <li>• Filter Strips</li> <li>• Sand Filters</li> <li>• Oil-Grit separators (OGS)</li> </ul>	<ul style="list-style-type: none"> <li>• Not a feasible option due to site constraints and multiple outlets.</li> <li>• Wetlands are not feasible with available site area and configuration.</li> <li>• The increase in impervious area is not sufficient to consider a wet or dry pond facility as a viable option.</li> <li>• An OGS is not considered a viable option due to the outlet grade and configuration.</li> <li>• Infiltration basin/trench can be considered as viable options in combination with a conveyance feature to provide <b>water quality</b> control.</li> <li>• Filter systems are typically cumbersome, expensive and require extensive maintenance at regular intervals.</li> </ul>

A review of the above-mentioned BMPs indicates that a hybrid feature incorporating conveyance and infiltration is an appropriate method for achieving the necessary quality control required.

Based on Table 3.2 of the Stormwater Management Planning and Design Manual, the proposed SWM facilities were designed to provide the necessary “Enhanced” level of protection for the proposed development. **Table 3** provides a summary of the proposed SWM features and demonstrates how water quality protection can be achieved for the selected sub-catchments.

**Table 3 – Proposed Water Quality Treatment Summary**

Description	Quality Control Feasibility
<p><b>Catchment – PR-100</b></p> <ul style="list-style-type: none"> <li>Stone filled infiltration trench located within roadside ditch system.</li> </ul>	<ul style="list-style-type: none"> <li>To achieve Level 1 (enhanced) protection, a storage volume of 66.5 m<sup>3</sup> is required based on Table 3.2 of the SWM Manual (2.66 ha x 25 m<sup>3</sup>/ha)</li> <li>Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.</li> </ul>
<p><b>Catchment – PR-102</b></p> <ul style="list-style-type: none"> <li>Stone filled infiltration trench located within roadside ditch system.</li> </ul>	<ul style="list-style-type: none"> <li>To achieve Level 1 (enhanced) protection, a storage volume of 37 m<sup>3</sup> is required based on Table 3.2 of the SWM Manual (1.48 ha x 25 m<sup>3</sup>/ha)</li> <li>Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.</li> </ul>
<p><b>Catchment – PR-200</b></p> <ul style="list-style-type: none"> <li>Stone filled infiltration trench located within roadside ditch system.</li> </ul>	<ul style="list-style-type: none"> <li>To achieve Level 1 (enhanced) protection, a storage volume of 19 m<sup>3</sup> is required based on Table 3.2 of the SWM Manual (0.75 ha x 25 m<sup>3</sup>/ha)</li> <li>Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.</li> </ul>
<p><b>Catchment – PR-201</b></p> <ul style="list-style-type: none"> <li>Stone filled infiltration trench located within roadside ditch system.</li> </ul>	<ul style="list-style-type: none"> <li>To achieve Level 1 (enhanced) protection, a storage volume of 32 m<sup>3</sup> is required based on Table 3.2 of the SWM Manual (1.28 ha x 25 m<sup>3</sup>/ha)</li> <li>Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.</li> </ul>

### 4.3 Stormwater Quantity Control

#### 4.3.1 Peak Flow Calculations

Peak flows were estimated using Visual Otthymo version 3.0 (VO3) hydrologic modelling software

for each of the 2, 5, 10, 25, 50 and 100-year storm events. These calculations consider the 6-hour SCS storm duration as prescribed by the City of Peterborough Engineering Design Standards (April 2019). The schematic layout of the VO3 model and the simulation results are presented in **Appendix B**.

**Table 4 – Existing and Uncontrolled Peak Flow Rates – OUT 1 and OUT 2**

Return Period	Peak Flow Rates (m <sup>3</sup> /s)							
	OUT 1 WEST		OUT 1 EAST		OUT 2 WEST		OUT 2 EAST	
	EX <sup>1</sup>	UNC <sup>2</sup>	EX <sup>1</sup>	UNC <sup>2</sup>	EX <sup>1</sup>	UNC <sup>2</sup>	EX <sup>1</sup>	UNC <sup>2</sup>
2-Year	0.042	<b>0.063</b>	0.020	<b>0.081</b>	0.025	0.017	0.056	<b>0.092</b>
5-Year	0.078	<b>0.117</b>	0.042	<b>0.133</b>	0.052	0.034	0.110	<b>0.149</b>
<u>10-Year</u>	0.107	<b>0.159</b>	0.060	<b>0.171</b>	0.073	0.046	0.151	<b>0.196</b>
<u>25-Year</u>	0.147	<b>0.216</b>	0.086	<b>0.238</b>	0.103	0.064	0.210	<b>0.257</b>
<u>50-Year</u>	0.180	<b>0.264</b>	0.107	<b>0.283</b>	0.128	0.078	0.257	<b>0.320</b>
<u>100-Year</u>	0.215	<b>0.313</b>	0.129	<b>0.330</b>	0.154	0.093	0.306	<b>0.374</b>

- Notes: 1. EX refers to the existing development condition. (NHYD = 1, 2, 3, 4)  
2. UNC refers to the proposed conditions without SWM controls. (NYHD = 6, 9, 13, 12)

As shown in **Table 4**, the proposed uncontrolled flows to **OUT 1 WEST**, **OUT 1 EAST** and **OUT 2 EAST** exceed the existing condition levels without the use of SWM controls, and therefore stormwater quantity controls will be required for these outlet locations. The proposed uncontrolled flows to **OUT 2 WEST** are reduced due to a reduction in drainage area discharging to that location in the proposed condition. As a result, stormwater quantity controls will not be required for **OUT 2 WEST**. The outlet locations are shown on **Figure 2** and **Figure 3**.

**Table 5 – Existing and Uncontrolled Peak Flow Rates – OUT 3 and OUT 4**

Return Period	Peak Flow Rates (m <sup>3</sup> /s)			
	OUT 3		OUT 4	
	EX <sup>1</sup>	UNC <sup>2</sup>		
2-Year	0.089	0.089	0.020	0.011
5-Year	0.184	0.182	0.040	0.021
10-Year	0.261	0.256	0.056	0.028
25-Year	0.369	0.361	0.078	0.038
50-Year	0.458	0.448	0.096	0.047
100-Year	0.553	0.541	0.115	0.055

- Notes: 1. EX refers to the existing development condition. (NHYD = 5, 55)  
2. UNC refers to the proposed condition without SWM controls. (NYHD = 14, 56)

In the post development condition for Outlet 3 (**OUT 3**), a portion of the overall developed site, including six (6) residential homes and backyards, will be directed to

the outlet. In the post development condition for Outlet 4 (**OUT 4**), a portion of the rear yards at the southern tip of the property will be directed to the outlet. A review of the hydrologic parameters and modelling indicates a reduction in drainage area to both **OUT 3** and **OUT 4**, offsetting the increase in impervious area. As a result and as outlined in **Table 5**, there is no increase in peak flow rates discharging to **OUT 3** and **OUT 4**, and therefore no stormwater quantity controls will be required for either outlet.

#### 4.3.2 Quantity Control Summary

In accordance with the design criteria established in **Section 3.1**, quantity controls are required to ensure that post-development flow rates do not exceed existing conditions, for each outlet, up to the 100-year storm. The VO3 model is used to estimate the required storage volume to provide the necessary quantity control without overtopping. A preliminary design of the combination stone filled infiltration trenches / detention ditches have been completed to confirm that sufficient stage storage can be provided. The flow regulation can be achieved by means of an outlet control structure for each facility.

#### 4.4 Stormwater Management Facilities

SWM facilities will be required for the development to achieve the necessary quality and quantity control targets. As discussed in **Table 3**, stone filled infiltration trenches will provide the necessary water quality control for each outlet location. As necessary, an open detention portion will be provided above the infiltration trench as part of the roadside ditch system, and will be controlled by a dedicated outlet structure within each facility.

##### 4.4.1 Design Overview

The preliminary selection of the SWM facilities was designed based on the required volume targets, outlet configuration and site topography. A review of **Table 6** provides a summary of each SWM facility for each outlet location.

**Table 6 – Proposed Stormwater Management Facility Summary**

Catchment	Outlet ID	Design Summary
PR-100	OUT-1 WEST	<ul style="list-style-type: none"> <li>• 1.0 m deep stone filled infiltration trench, 2.0 m in width and 90 m in length</li> <li>• Required storage volume of stone filled trench for quality control is 66.5 m<sup>3</sup>, with 72 m<sup>3</sup> provided.</li> <li>• Total storage volume required for quantity control is 261 m<sup>3</sup>, with 278 m<sup>3</sup> provided at 0.6 m depth.</li> <li>• One stage outlet control is assumed in the preliminary calculations, multi-stage will be considered during detailed design to maximize outlet efficiency and reduce facility size.</li> </ul>
PR-102	OUT-1 EAST	<ul style="list-style-type: none"> <li>• 1.0m deep stone filled infiltration trench, 2.0 m in width and 97 m in length</li> <li>• Required storage volume of stone filled trench for quality control is 37 m<sup>3</sup>, with 74 m<sup>3</sup> provided.</li> <li>• Total storage volume required for quantity control is 433 m<sup>3</sup>, with 435 m<sup>3</sup> provided at 0.8m depth.</li> <li>• One stage outlet control is assumed in the preliminary calculations, multi-stage will be considered during detailed design to maximize outlet efficiency and reduce facility size.</li> </ul>
PR-200	OUT-2 WEST	<ul style="list-style-type: none"> <li>• 0.5 m deep stone filled infiltration trench, 2.0 m in with and 50 m in length.</li> <li>• Required storage volume of stone filled trench for quality control is 19 m<sup>3</sup>, with 21 m<sup>3</sup> provided.</li> <li>• Stormwater quantity control not required for PR-200.</li> </ul>
PR-201	OUT-2 EAST	<ul style="list-style-type: none"> <li>• 1.0 m deep stone filled infiltration trench, 2.0 m in width and 107 m in length</li> <li>• Required storage volume of stone filled trench for quality control is 32 m<sup>3</sup>, with 52 m<sup>3</sup> provided.</li> <li>• Total storage volume required for quantity control is 200 m<sup>3</sup>, with 301 m<sup>3</sup> provided at 0.6 m depth.</li> <li>• One stage outlet control is assumed in the preliminary calculations, multi-stage will be considered during detailed design to maximize outlet efficiency and reduce facility size.</li> </ul>

A review of **Table 6** indicates that sufficient storage volumes can be provided within the SWM facilities to meet the LID, water quality and water quantity control requirements. A geotechnical study of the site is recommended during the detailed design phase to

determine actual infiltration rates and groundwater levels to confirm the final dimensions of the proposed facility and to include a shallow infiltration bottom to the proposed facilities.

#### 4.4.2 Proposed Release Rates

The proposed peak flow rates for from the preliminary SWM facilities with respect to design storm events are shown in **Table** below.

**Table 7 – Existing and Proposed Peak Flow Summary**

Return Period	Peak Flow Rates (m <sup>3</sup> /s)							
	OUT 1 WEST		OUT 1 EAST		OUT 2 WEST		OUT 2 EAST	
	EX <sup>1</sup>	PR <sup>2</sup>	EX <sup>1</sup>	PR <sup>2</sup>	EX <sup>1</sup>	PR <sup>2</sup>	EX <sup>1</sup>	PR <sup>2</sup>
2-Year	0.042	0.020	0.020	0.020	0.025	0.017	0.056	0.056
5-Year	0.078	0.068	0.042	0.038	0.052	0.034	0.110	0.110
10-Year	0.107	0.104	0.060	0.049	0.073	0.046	0.151	0.149
25-Year	0.147	0.140	0.086	0.065	0.103	0.064	0.210	0.194
50-Year	0.180	0.165	0.107	0.077	0.128	0.078	0.257	0.232
100-Year	0.215	0.186	0.129	0.089	0.154	0.093	0.306	0.268

- Notes: 1. EX refers to the existing development condition. (NH<sub>YD</sub> = 1, 2, 3, 4)  
 2. PR refers to the proposed conditions with controlled flows from the proposed control facility. (NY<sub>HD</sub> = 16, 20, 13, 24)

A review of **Table 7** indicates the proposed SWM facilities will provide the required quantity controls such that the proposed development will not increase peak flow rates at each outlet location. Stage-Storage-Discharge calculations are provide for each facility in **Appendix D**. It is noted that these facilities have been conservatively designed using a single outlet control. During detailed design, the outlet configuration and infiltration storage depth for each facility will be optimized to reduce the storage volume requirements.

## 5.0 Conclusion

As the proposed residential subdivision will alter existing drainage patterns, a preliminary stormwater management report has been prepared to address the requirements of the County of Peterborough and ORCA.

Low Impact Development considerations and stormwater quality controls such as stone filled infiltration trenches within the roadway corridor can be provided to achieve “Enhanced” Level 1 protection as defined in the Stormwater Management Planning and Design Manual (March 2003).

Water quantity controls can be provided by the stone filled infiltration ditches within the roadway corridor with outlet control structures providing detention control to existing condition levels.

If you require any further information, or have any questions, please do not hesitate to contact the undersigned.

Respectfully submitted,



Chris Proctor-Bennett, P.Eng.  
Group Leader, Stormwater Management



A handwritten signature in black ink, appearing to read "Mark Wilson".

Mark Wilson, A.Sc.T.  
Water Resources Designer

MW/CPB/jl

### Statement of Limitations

This report has been prepared by D.M. Wills Associates Limited on behalf of Mr. Rubal Kundra of Life at the Woodland Inc. to address the requirements of the County of Peterborough and ORCA.

The conclusions and recommendations in this report are based on available background documentation and discussions with applicable agencies at the time of preparation.

The report is intended to determine the feasibility of the proposed development with respect to Stormwater Management of the Site. The design information provided in this report is preliminary in nature and should not be used for site plan application or construction purposes.

Any use that a third party makes of this report other than a Preliminary Stormwater Management Report for the proposed development is the responsibility of such third parties. D.M. Wills Associates Limited accepts no responsibility for damages, if any, suffered by a third party as a result of decisions made or action taken based on using this report for purposes other than a Preliminary Stormwater Management Report for the proposed Life at the Woodland residential subdivision.

# Appendix A

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Rainfall Data and Hydrology



## B.1 Storm Sewer System

City of Peterborough Standard Drawings and Specifications shall be adhered to at all times. Where the City has no standard or specification, the City of Peterborough recognizes the July 1984 release of the Ministry of Environment Guidelines for the Design of Storm Sewer Systems as the guidelines by-which all storm sewer work shall conform to. Otherwise, OPSS or OPSD shall apply.

### B.1.1 Definition and Use

Storm systems may consist of one or any combination of pipes, ditches, culverts, open channels and storm water management facilities that convey storm water.

Storm sewers shall be designed to collect storm water discharge from pervious and impervious areas both on private and public lands. Storm drainage connected to buildings on private property requires a building permit before installation.

### B.1.2 Location and Alignment

All works to be constructed within a City road allowance are to be located in accordance with the appropriate City of Peterborough Drawing from standards USD100.01 thru USD100.13. The City must approve locating works in non-standard locations.

Storm sewers connected to buildings on private property are regulated by Part 7 of the OBC. Where there are no specific regulations in the OBC, details from this document shall apply.

Connections to existing storm sewer systems shall be made at manholes. Where no manhole is present a new manhole is required on the City's main. Connections between storm sewer pipes on private property, where not at a manhole or catchbasin, shall be made with manufactured "Tees" and only with approval from the City engineering department and only if sewer is not defined as a *building sewer* 200mm or greater. Control manholes for private sewers shall be placed on the front property line or just inside the property if placement on the property line is not possible.

### B.1.3 Drainage / Sub Drainage Area Plans

Drainage/sub-drainage area limits for sewer designs are to be in accordance with approved grading plans to the proposed maintenance holes (or catchbasins if applicable) located on the R.O.W.

Note: All areas and runoff coefficients are to be shown for each drainage/sub-drainage areas.

#### B.1.4 External Watershed Limits and Drainage Areas

When design abuts undeveloped areas, identify the external watershed limit to be designed for, typically following contour lines. Developed external areas should encompass the entire sewershed.

Note: All areas, runoff coefficients and time of concentrations are to be shown for all drainage areas within external watershed limits.

#### B.1.5 Design Chart

Storm sewer design calculations are to be completed on an appropriate Storm Sewer Design chart.

#### B.1.6 Design Requirements and Location

The City of Peterborough rainfall data based upon 2002 AES Peterborough Airport IDF shall be used for the development of rainfall intensities for storm sewer design. Alternatively, IDF curve parameters A, B, and C provided in Table B.1.7.1 may be used.

Storm sewers shall be designed as a separate sewer system. Effluent from sanitary sewers or any potentially contaminated drainage from industrial, agricultural or commercial operations shall not be discharged into storm sewers. Contaminated drainage means, the introduction of any foreign, undesirable physical, chemical or biological substance into the environment, which results or is likely to result in deleterious effects.

Storm sewers shall be designed as deep storm sewers with approximately 3.0m of cover where private gravity service connections are required. An acceptable alternative to the deep sewer system is the provision of a separate foundation drainage system (generally with smaller pipes) with gravity service connections as well as a traditional storm sewer system with shallow pipes. Where physical constraints do not allow for either above noted system, a shallow system may be approved with pipe typically 1.25m deep.

The alignment of the storm varies depending on the type of road and whether or not deep storm sewers are to be implemented. Typically, deep storm sewers are offset 1.5m on one side of the centreline with the sanitary sewer offset 1.5m from the other side of the centreline. Shallow storm sewers, particularly those less than 450mm in diameter, are typically located 0.31 metres within the curb face. Storm sewers are generally to the north or west of the centerline.

MOE Guidelines require 0.5m vertical or 2.5m horizontal clearances between sewers and watermains. In some circumstances it may be prudent for the PUC/City jointly to decide by what means/best practice one main crosses the other in addition to MOE

design guidelines. Watermain bends may be required at sewer/watermain pipe crossings while sometimes it may be more appropriate to change the grade of a sewer, depending on the circumstances.

The capacity of the minor storm sewer systems shall typically be designed to carry the peak flow resulting from a one (1) in five (5) year rainfall event. Where gravity foundation service connections exist, the five year design flow must not exceed 80% of the just full pipe capacity.

Where gravity service connections exist or are proposed, a 100 year hydraulic grade line analysis must be undertaken, to determine peak 100 year water levels within a potentially surcharged storm sewer system. A minimum freeboard of 0.50m must be provided between the computed 100 year hydraulic grade line and the minimum basement floor level in conjunction with the use of backflow preventers. Where the change in grade has the potential for hydraulic jumps, additional freeboard shall be provided. The implementation of flow regulating ICDs may be permitted by the City Engineer to reduce 100 year storm sewer flows on a case by case basis only at low points in the road, however in all instances, the 5 year flow must pass through the ICD unencumbered with minimal backwater head and no surface ponding. Pipe sizes should be increased elsewhere to accommodate the 100 year flow with appropriate hydraulic grade line elevations.

The major system design shall be based on a one in 100 year rainfall event and should include assessment of road sags and boulevard overflows into stormwater management ponds and watercourses. The maximum ponding depth shall not exceed 300mm as measure to the centerline of the road.

#### B.1.7 Peak Flow Calculation and Storm Sewer Design

The design area shall include all areas, which reasonably or naturally drain to the system. To calculate the peak rate of runoff from an area, the Rational Method shall be used as follows:

$$Q = K \cdot A \cdot i \cdot C$$

Where:

'Q' - is peak flow (l/s)

'K' - is 2.78

'A' - is the area (hectares)

'i' - is the rainfall intensity (mm/hour) calculated as follows:

$$i = \frac{A}{(Tc + B)^C}$$

or as directly derived from 2002 Peterborough Airport IDF curves

Where: A, B and C are per Table B.1.7.1.

Table B.1.7.1

	A	B	C
2 Year	662	7.5	0.79
5 Year	1098	10.1	0.83
10 Year	1560	13	0.86
25 Year	2010	14	0.88
50 Year	2200	14.6	0.87
100 Year	2507	14.8	0.88

Please note that the above A, B, C values shall be used for storm sewer design only, or other calculations design storms of less than 3 hours duration. Stormwater Management Reports should use rainfall directly from the 2006 Peterborough Airport IDF curves.

The time of concentration (Tc) should be calculated rather than relying upon arbitrary minimum and maximum times. Where this is not practical, a ten (10) minute time of concentration (Tc) shall be used except when the zoning requires the use of a runoff coefficient of 0.75 or higher in which case five (5) minute time of concentration (Tc) shall be used.

‘C’ - is the co-efficient of run-off

The runoff co-efficient or “C” for storm drainage unless otherwise specified or adequately proven through calculation, shall be per Table B.1.7.2 for the 5 year design.

Table B.1.7.2

Parks – over 4.0 ha	0.20
Parks – 4.0 ha and under	0.25
Single family residential-15m lots	0.55
Single family residential-12m lots	0.65
Single family residential-9m lots	0.75
Semi-detached	0.80
Townhouses	0.85
Apartments	0.90
Schools and Churches / Industrial	Varies
Commercial	0.90
Heavily Developed Areas	0.90
Asphalt, Concrete, Roofed Areas	0.95

25 to 100 year runoff co-efficients shall be increased to account for soil saturation. Increase co-efficients for the 25, 50, and 100 year storms by 10%, 20%, and 25% respectively up to a maximum value of 0.95.

#### B.1.7.1 Flow Velocities and Minimum Slope

Storm sewer flow velocities shall not be less than 0.8 m/s when flowing full or 0.6m/s at design depth. Minimum longitudinal slope shall be 0.5%. The preferred maximum velocity is 3.0 m/s with an absolute maximum acceptable velocity of 6.0 m/s.

#### B.1.7.2 Pipe Cover

The minimum depth of cover to pipe crown shall be 1.2 m. Excessive cover should be avoided except under special circumstances.

Minimum pipe cover for deep sewers shall be based upon providing gravity connections including hydraulic grade line freeboard for storm services.

For concrete pipe, the maximum allowable cover permitted on concrete pipe to be constructed is to be based on OPSD 807.010, 807.030, 807.040 and 807.050. Where the pipe required exceeds the OPSD charts, a pipe design sealed by a Professional Engineer must be submitted to the City for approval.

For flexible pipe, the maximum allowable cover permitted shall be as per OPSD or manufacturers specifications.

#### B.1.7.3 Gravity Pipe Design

The minimum pipe diameter for storm sewers shall be 250 mm. Minimum pipe diameter for catchbasins leads shall be 250mm with the exception of double catchbasins which shall be 300mm.

The obvert of the inlet pipe at all maintenance holes shall be higher than or equal to the obvert of the outlet pipe. Appropriate invert elevation drops to account for the velocity head, transition and bend losses within manholes should be provided.

An outlet pipe from a manhole is not permitted to be smaller than the incoming pipe even if the outlet pipe has adequate capacity due to greater slope. Allowances may be granted by the City Engineer in special circumstances to allow a smaller outlet pipes on privately owned property in the event other regulatory agencies (e.g. MTO) require this for stormwater retention.

The Manning equation shall be used to calculate the required hydraulic capacity of a gravity sewer as follows:

6 Hour SCS Type II Intensity Hyetographs  
 2006 Peterborough Airport Weather Station  
 (mm/hr)

Time (min.)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
0	0	0	0	0	0	0
15	1.6	2.1	2.5	2.9	3.3	3.6
30	1.6	2.1	2.5	2.9	3.3	3.6
45	2.3	3.2	3.7	4.4	4.9	5.4
60	2.3	3.2	3.7	4.4	4.9	5.4
75	2.3	3.2	3.7	4.4	4.9	5.4
90	2.3	3.2	3.7	4.4	4.9	5.4
105	3.9	5.2	6.2	7.3	8.1	9.0
120	3.9	5.2	6.2	7.3	8.1	9.0
135	4.6	6.3	7.4	8.8	9.8	10.8
150	4.6	6.3	7.4	8.8	9.8	10.8
165	23.2	31.4	36.9	43.7	48.9	53.9
180	60.4	81.78	95.9	113.7	127.0	140.2
195	8.5	11.5	13.5	16.0	17.9	19.8
210	8.5	11.5	13.5	16.0	17.9	19.8
225	3.9	5.2	6.2	7.3	8.1	9.0
240	3.9	5.2	6.2	7.3	8.1	9.0
255	3.1	4.2	4.9	5.8	6.5	7.2
270	3.1	4.2	4.9	5.8	6.5	7.2
285	2.3	3.2	3.7	4.4	4.9	5.4
300	2.3	3.2	3.7	4.4	4.9	5.4
315	1.6	2.1	2.5	2.9	3.3	3.6
330	1.6	2.1	2.5	2.9	3.3	3.6
345	1.6	2.1	2.5	2.9	3.3	3.6
360	1.6	2.1	2.5	2.9	3.3	3.6

## Hydrologic Parameters for EX-100

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** MW / CPB  
**Date:** 22-Feb-22

Land Use				Rainfall Data	
	<u>Internal</u>	<u>External</u>		<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Agriculture	0.00	0.00	ha	<b>Drainage Area</b> 2.02 ha <b>Impervious Area</b> 0.04 ha <b>Percent Impervious</b> 1.9% Connected Impervious 1.9%	
Range	0.00	0.00	ha		
Grass	0.35	1.47	ha		
Woods	0.10	0.06	ha		
Wetland	0.00	0.00	ha		
Gravel	0.00	0.00	ha		
Impervious	0.00	0.04	ha		
<b>SUM</b>	<b>0.45</b>	<b>1.57</b>			
<b>Hydrologic Soil Group<sup>1</sup></b>	<b>B</b>	<b>B</b>			
<b>Soil Type</b>	<b>0</b>	<b>0</b>			
<b>C</b>	0.21	0.21			
<b>CN (Nashyd)</b>	60.3	61.8			
				<b>Pervious</b> <b>Impervious</b>	
				<b>Length</b>	125    5    m
				<b>US Elev</b>	226.5    207.5    m
				<b>DS Elev</b>	207.5    207.4    m
				<b>Slope</b>	15.2    2.0    %
				Steep	Flat

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	<b>B</b>	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.21	
	<b>B</b>	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.21	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	<b>B</b>	74	65	61	58	50	85	98	60.3	60.3
	<b>B</b>	74	65	61	58	50	85	98	61.8	60.9
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	5.3	5.4

Time of Concentration <sup>6</sup>			
<b>Pervious Length</b>	125	m	
<b>Slope</b>	15.2	%	
<b>Airport</b>	13.2	min.	
<b>Bransby - Williams</b>	3.9	min.	Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	<b>15.0</b>	min.	
<b>Time to Peak</b>	10.1	min.	
	<b>0.17</b>	hr.	

Composite Parameters		
<b>Drainage Area</b>	2.02 ha	
<b>Runoff Coefficient</b>	0.21	
<b>SCS Curve No.</b>	61.5	60.8
<b>Modified Curve No.<sup>4</sup>, CN*</b>	<b>61.5</b>	60.7
<b>Initial Abstraction.</b>	<b>5.3</b>	5.4

**Notes:**

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

**Hydrologic Parameters for EX-101**

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** MW / CPB  
**Date:** 22-Feb-22

Land Use				Rainfall Data	
Agriculture	0.00	0.00	ha	<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Range	0.21	0.07	ha		
Grass	0.08	0.00	ha	<b>Drainage Area</b> 1.42 ha <b>Impervious Area</b> 0.03 ha <b>Percent Impervious</b> 2.4% Connected Impervious 0.2%	
Woods	0.96	0.07	ha		
Wetland	0.00	0.00	ha		
Gravel	0.00	0.00	ha		
Impervious	0.03	0.00	ha	<b>Pervious</b> <b>Length</b> 110 m <b>US Elev</b> 212.2 m <b>DS Elev</b> 207.5 m <b>Slope</b> 4.3 % Rolling	
<b>SUM</b>	<b>1.27</b>	<b>0.14</b>			
<b>Hydrologic Soil Group<sup>1</sup></b>	B	B			
<b>Soil Type</b>	0	0			
<b>C</b>	0.15	0.17			
<b>CN (Nashyd)</b>	60.4	61.5			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.15	
	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.17	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	60.4	59.4
	B	74	65	61	58	50	85	98	61.5	61.5
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	9.1	9.3

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	110	m
<b>Average Slope</b>	4.3	%
<b>Airport</b>	20.1	min.
<b>Bransby - Williams</b>	4.5	min.
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	13.5	min.
	0.22	hr.

Flat: 0-2% Slopes  
Rolling: 2-6% Slopes  
Hilly: >6% Slopes

Composite Parameters		
<b>Drainage Area</b>	1.42 ha	
<b>Runoff Coefficient</b>	0.15	
<b>SCS Curve No.</b>	60.5	59.6
<b>Modified Curve No.<sup>4</sup>, CN*</b>	63.1	62.7
<b>Initial Abstraction.</b>	9.1	9.3

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- Connected Impervious is estimated using the Sutherland Equation with a Watershed Selection Criteria of Somewhat Connected

**Hydrologic Parameters for EX-200**

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** MW / CPB  
**Date:** 22-Feb-22

Land Use				Rainfall Data	
	<b>Internal</b>	<b>External</b>		<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Agriculture	0.00	0.00	ha		
Range	0.00	0.00	ha		
Grass	0.27	0.13	ha		
Woods	1.04	0.09	ha		
Wetland	0.00	0.00	ha		
Gravel	0.00	0.00	ha		
Impervious	0.00	0.00	ha		
<b>SUM</b>	<b>1.31</b>	<b>0.22</b>		<b>Drainage Area</b> 1.53 ha <b>Impervious Area</b> 0.00 ha <b>Percent Impervious</b> 0.0% Connected Impervious 0.0%	
<b>Hydrologic Soil Group<sup>1</sup></b>	B	B		<b>Pervious</b> <b>Length</b> 130 m <b>US Elev</b> 225.9 m <b>DS Elev</b> 211.6 m <b>Slope</b> 11.0 % Steep	
<b>Soil Type</b>	0	0			
<b>C</b>	0.27	0.23			
<b>CN (Nashyd)</b>	58.6	59.8			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.27	
	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.23	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	58.6	58.6
	B	74	65	61	58	50	85	98	59.8	59.8
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.7	8.7

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	130	m
<b>Average Slope</b>	11.0	%
<b>Airport</b>	14.1	min.
<b>Bransby - Williams</b>	4.4	min.
		Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	10.1	min.
	0.17	hr.

Composite Parameters		
<b>Drainage Area</b>	1.53	ha
<b>Runoff Coefficient</b>	0.26	
<b>SCS Curve No.</b>	58.8	58.8
<b>Modified Curve No.<sup>4</sup>, CN*</b>	61.7	61.7
<b>Initial Abstraction.</b>	8.7	8.7

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

**Hydrologic Parameters for EX-201**

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** MW / CPB  
**Date:** 22-Feb-22

Land Use				Rainfall Data	
	<b>Internal</b>	<b>External</b>		<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Agriculture	0.00	0.00	ha		
Range	2.16	0.24	ha		
Grass	0.00	0.00	ha		
Woods	0.02	0.00	ha		
Wetland	0.00	0.00	ha		
Gravel	0.00	0.00	ha		
Impervious	0.00	0.02	ha		
<b>SUM</b>	<b>2.18</b>	<b>0.26</b>		<b>Drainage Area</b> 2.44 ha <b>Impervious Area</b> 0.02 ha <b>Percent Impervious</b> 0.7% Connected Impervious 0.7%	
<b>Hydrologic Soil Group<sup>1</sup></b>	B	B		<b>Pervious</b> <b>Length</b> 100 m <b>US Elev</b> 213.2 m <b>DS Elev</b> 206.6 m <b>Slope</b> 6.6 % Hilly	
<b>Soil Type</b>	0	0			
<b>C</b>	0.30	0.34			
<b>CN (Nashyd)</b>	64.9	67.3			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.30	
	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.34	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	64.9	64.9
	B	74	65	61	58	50	85	98	67.3	65.0
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.0	8.0

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	100	m
<b>Average Slope</b>	6.6	%
<b>Airport</b>	13.9	min.
<b>Bransby - Williams</b>	3.6	min.
		Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	10.1	min.
	0.17	hr.

Composite Parameters		
<b>Drainage Area</b>	2.44	ha
<b>Runoff Coefficient</b>	0.30	
<b>SCS Curve No.</b>	65.2	64.9
<b>Modified Curve No.<sup>4</sup>, CN*</b>	68.8	68.5
<b>Initial Abstraction.</b>	8.0	8.0

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

**Hydrologic Parameters for EX-300**

Sheet 1 of 1



Project No: 19-10874  
 Project Name: Life at the Woodland  
 Designed/Checked By: RC/CPB  
 Date: 22-Feb-22

Land Use			Rainfall Data	
	<u>Internal</u>		Gauging Station = Peterborough	
Agriculture	0.00	ha	12 hr, 100 Yr Rainfall =	90.4 mm
Range	5.25	ha		
Grass	0.00	ha		
Woods	3.47	ha		
Wetland	0.00	ha		
Gravel	0.00	ha		
Impervious	0.00	ha		
<b>SUM</b>	<b>8.72</b>			
			<b>Drainage Area</b>	<b>8.72</b> ha
			<b>Impervious Area</b>	<b>0.00</b> ha
			<b>Percent Impervious</b>	<b>0.0%</b>
			Connected Impervious	0.0%
			<b>Pervious</b>	
			<b>Length</b>	330 m
			<b>US Elev</b>	213.5 m
			<b>DS Elev</b>	200.9 m
			<b>Slope</b>	3.8 %
				Rolling
<b>Hydrologic Soil Group<sup>1</sup></b>	<b>B</b>			
<b>Soil Type</b>	<b>0</b>			
<b>C</b>	0.18			
<b>CN (Nashyd)</b>	62.2			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	<b>B</b>	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.18	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	<b>B</b>	74	65	61	58	50	85	98	62.2	62.2
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.8	8.8

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	330	m
<b>Average Slope</b>	3.8	%
<b>Airport</b>	<b>35.2</b>	min.
<b>Bransby - Williams</b>	11.6	min.
		Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	23.6	min.
	<b>0.39</b>	hr.

Composite Parameters		
<b>Drainage Area</b>	8.72	ha
<b>Runoff Coefficient</b>	0.18	
<b>SCS Curve No.</b>	62.2	62.2
<b>Modified Curve No.<sup>4</sup>, CN*</b>	<b>64.6</b>	64.6
<b>Initial Abstraction.</b>	<b>8.8</b>	8.8

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

**Hydrologic Parameters for EX-400**

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use			Rainfall Data	
	<b>Internal</b>		<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Agriculture	0.00	ha	<b>Drainage Area</b>	1.24 ha
Range	1.09	ha	<b>Impervious Area</b>	0.00 ha
Grass	0.00	ha	<b>Percent Impervious</b>	0.0%
Woods	0.15	ha	Connected Impervious	0.0%
Wetland	0.00	ha		
Gravel	0.00	ha		
Impervious	0.00	ha		
<b>SUM</b>	<b>1.24</b>			
<b>Hydrologic Soil Group<sup>1</sup></b>	B		<b>Pervious</b>	
<b>Soil Type</b>	0		<b>Length</b>	165 m
<b>C</b>	0.21		<b>US Elev</b>	211.6 m
<b>CN (Nashyd)</b>	64.2		<b>DS Elev</b>	204.8 m
			<b>Slope</b>	4.1 %
				Rolling

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.21	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	64.2	64.2
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.2	8.2

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	165	m
<b>Average Slope</b>	4.1	%
<b>Airport</b>	23.5	min.
<b>Bransby - Williams</b>	6.9	min.
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	15.7	min.
	0.26	hr.

Composite Parameters		
<b>Drainage Area</b>	1.24	ha
<b>Runoff Coefficient</b>	0.21	
<b>SCS Curve No.</b>	64.2	64.2
<b>Modified Curve No.<sup>4</sup>, CN*</b>	67.5	67.5
<b>Initial Abstraction.</b>	8.2	8.2

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

## Hydrologic Parameters for PR-100

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use				Rainfall Data																									
	<b>Internal</b>	<b>External</b>		<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm																									
Agriculture	0.00	0.00	ha	<b>Drainage Area</b> 2.66 ha <b>Impervious Area</b> 0.26 ha <b>Percent Impervious</b> 9.7% Connected Impervious 9.7%  <table style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th></th> <th style="text-align: center;">Pervious</th> <th style="text-align: center;">Impervious</th> <th></th> </tr> </thead> <tbody> <tr> <td><b>Length</b></td> <td style="text-align: center;">125</td> <td style="text-align: center;">8</td> <td style="text-align: center;">m</td> </tr> <tr> <td><b>US Elev</b></td> <td style="text-align: center;">226.5</td> <td style="text-align: center;">207.5</td> <td style="text-align: center;">m</td> </tr> <tr> <td><b>DS Elev</b></td> <td style="text-align: center;">207.5</td> <td style="text-align: center;">207.3</td> <td style="text-align: center;">m</td> </tr> <tr> <td><b>Slope</b></td> <td style="text-align: center;">15.2</td> <td style="text-align: center;">2.0</td> <td style="text-align: center;">%</td> </tr> <tr> <td></td> <td style="text-align: center;">Steep</td> <td style="text-align: center;">Flat</td> <td></td> </tr> </tbody> </table>			Pervious	Impervious		<b>Length</b>	125	8	m	<b>US Elev</b>	226.5	207.5	m	<b>DS Elev</b>	207.5	207.3	m	<b>Slope</b>	15.2	2.0	%		Steep	Flat	
	Pervious	Impervious																											
<b>Length</b>	125	8	m																										
<b>US Elev</b>	226.5	207.5	m																										
<b>DS Elev</b>	207.5	207.3	m																										
<b>Slope</b>	15.2	2.0	%																										
	Steep	Flat																											
Range	0.00	0.00	ha																										
Grass	0.87	1.47	ha																										
Woods	0.00	0.06	ha																										
Wetland	0.00	0.00	ha																										
Gravel	0.00	0.00	ha																										
Impervious	0.22	0.04	ha																										
<b>SUM</b>	<b>1.09</b>	<b>1.57</b>																											
<b>Hydrologic Soil Group<sup>1</sup></b>	B	B																											
<b>Soil Type</b>	0	0																											
<b>C</b>	0.33	0.21																											
<b>CN (Nashyd)</b>	68.5	61.8																											

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.33	
	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.21	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	68.5	61.0
	B	74	65	61	58	50	85	98	61.8	60.9
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.8	5.1

Time of Concentration <sup>6</sup>			
<b>Pervious Length</b>	125	m	
<b>Slope</b>	15.2	%	
<b>Airport</b>	12.5	min.	
<b>Bransby - Williams</b>	3.7	min.	Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	<b>15.0</b>	min.	
<b>Time to Peak</b>	10.1	min.	
	<b>0.17</b>	hr.	

Composite Parameters		
<b>Drainage Area</b>	2.66 ha	
<b>Runoff Coefficient</b>	0.26	
<b>SCS Curve No.</b>	64.5	60.9
<b>Modified Curve No.<sup>4</sup>, CN*</b>	<b>64.8</b>	60.6
<b>Initial Abstraction.</b>	<b>4.8</b>	5.1

**Notes:**

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

## Hydrologic Parameters for PR-101

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use				Rainfall Data		
	Controlled Lots	Uncontrolled Lots	Roadway	External		
Agriculture	0.00	0.00	ha		Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm	
Range	0.00	0.00	ha			
Grass	0.00	0.53	ha		<b>Drainage Area</b> 0.59 ha <b>Impervious Area</b> 0.06 ha <b>Percent Impervious</b> 10.0% Connected Impervious 10.0%	
Woods	0.00	0.00	ha			
Wetland	0.00	0.00	ha			
Gravel	0.00	0.00	ha			
Impervious	0.00	0.06	ha			
<b>SUM</b>	<b>0.00</b>	<b>0.59</b>				
<b>Hydrologic Soil Group<sup>1</sup></b>	<b>B</b>	<b>B</b>				
<b>Soil Type</b>	<b>0</b>	<b>0</b>				
<b>C</b>		0.21				
<b>CN (Nashyd)</b>		64.7				
				<b>Pervious</b>	<b>Impervious</b>	
				<b>Length</b>	40	5 m
				<b>US Elev</b>	212.2	211.0 m
				<b>DS Elev</b>	210.2	210.9 m
				<b>Slope</b>	5.0	2.0 %
				Rolling	Flat	

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	<b>B</b>	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.21	n.a.
	<b>B</b>	0.32	0.22	0.13	0.11	0.05	0.76	0.90		
<b>SCS Curve No.<sup>3</sup>, CN</b>	<b>B</b>	74	65	61	58	50	85	98	64.7	61.0
	<b>B</b>	74	65	61	58	50	85	98		
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.7	5.0

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	45	m
<b>Average Slope</b>	4.7	%
<b>Airport</b>	11.7	min.
<b>Bransby - Williams</b>	2.0	min.
		Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	<b>15.0</b>	min.
<b>Time to Peak</b>	10.1	min.
	<b>0.17</b>	hr.

Composite Parameters		
<b>Drainage Area</b>	0.59 ha	
<b>Runoff Coefficient</b>	0.21	
<b>SCS Curve No.</b>	64.7	61.0
<b>Modified Curve No.<sup>4</sup>, CN*</b>	<b>65.0</b>	60.5
<b>Initial Abstraction.</b>	<b>4.7</b>	5.0

**Notes:**

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. Connected Impervious does not include areas that discharge to pervious surfaces.

## Hydrologic Parameters for PR-102

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use					Rainfall Data	
	<b>Controlled Lots</b>	<b>Roadway</b>	<b>External</b>		<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Agriculture	0.00	0.00	0.00	ha	<b>Drainage Area</b> 1.48 ha <b>Impervious Area</b> 0.35 ha <b>Percent Impervious</b> 23.3% Connected Impervious 23.3%	
Range	0.00	0.00	0.00	ha		
Grass	0.70	0.29	0.08	ha		
Woods	0.00	0.00	0.07	ha		
Wetland	0.00	0.00	0.00	ha		
Gravel	0.00	0.00	0.00	ha		
Impervious	0.08	0.23	0.03	ha		
<b>SUM</b>	<b>0.78</b>	<b>0.52</b>	<b>0.18</b>			
<b>Hydrologic Soil Group<sup>1</sup></b>	<b>B</b>	<b>B</b>	<b>B</b>			
<b>Soil Type</b>	<b>0</b>	<b>0</b>	<b>0</b>			
<b>C</b>	0.21	0.48	0.26			
<b>CN (Nashyd)</b>	64.7	77.7	66.6			
					<b>Pervious</b>	<b>Impervious</b>
					<b>Length</b>	<b>US Elev</b>
					40	212.2
					5	211.0
					210.2	210.9
					<b>Slope</b>	<b>%</b>
					5.0	2.0
					Rolling	Flat

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient <sup>2</sup> , C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.21	
	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.48	
	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.26	n.a.
SCS Curve No. <sup>3</sup> , CN	B	74	65	61	58	50	85	98	64.7	61.0
	B	74	65	61	58	50	85	98	77.7	61.0
	B	74	65	61	58	50	85	98	66.6	59.6
Initial Abstraction <sup>5</sup> , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.5	5.3

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	45	m
<b>Average Slope</b>	4.7	%
<b>Airport</b>	10.4	min.
<b>Bransby - Williams</b>	1.8	min.
	Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes	
<b>Applicable Minimum<sup>7</sup></b>	<b>15.0</b>	min.
<b>Time to Peak</b>	10.1	min.
	<b>0.17</b>	hr.

Composite Parameters		
<b>Drainage Area</b>	1.48 ha	
<b>Runoff Coefficient</b>	0.31	
<b>SCS Curve No.</b>	69.5	60.8
<b>Modified Curve No.<sup>4</sup>, CN*</b>	70.8	<b>60.7</b>
<b>Initial Abstraction.</b>	4.5	<b>5.3</b>

**Notes:**

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

## Hydrologic Parameters for PR-200

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use			Rainfall Data																			
	<u>Internal</u>	<u>External</u>	<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm																			
Agriculture	0.00	ha	<b>Drainage Area</b> 0.75 ha <b>Impervious Area</b> 0.12 ha <b>Percent Impervious</b> 16.1% Connected Impervious 16.1%  <table style="width: 100%; border: none;"> <tr> <td style="text-align: center;"><b>Pervious</b></td> <td style="text-align: center;"><b>Impervious</b></td> <td></td> </tr> <tr> <td><b>Length</b></td> <td>130</td> <td>8 m</td> </tr> <tr> <td><b>US Elev</b></td> <td>225.9</td> <td>210.0 m</td> </tr> <tr> <td><b>DS Elev</b></td> <td>211.6</td> <td>209.8 m</td> </tr> <tr> <td><b>Slope</b></td> <td>11.0</td> <td>2.0 %</td> </tr> <tr> <td></td> <td>Steep</td> <td>Flat</td> </tr> </table>		<b>Pervious</b>	<b>Impervious</b>		<b>Length</b>	130	8 m	<b>US Elev</b>	225.9	210.0 m	<b>DS Elev</b>	211.6	209.8 m	<b>Slope</b>	11.0	2.0 %		Steep	Flat
<b>Pervious</b>	<b>Impervious</b>																					
<b>Length</b>	130	8 m																				
<b>US Elev</b>	225.9	210.0 m																				
<b>DS Elev</b>	211.6	209.8 m																				
<b>Slope</b>	11.0	2.0 %																				
	Steep	Flat																				
Range	0.00	ha																				
Grass	0.20	ha																				
Woods	0.43	ha																				
Wetland	0.00	ha																				
Gravel	0.00	ha																				
Impervious	0.12	ha																				
<b>SUM</b>	<b>0.75</b>																					
<b>Hydrologic Soil Group<sup>1</sup></b>	B																					
<b>Soil Type</b>	0																					
<b>C</b>	0.36																					
<b>CN (Nashyd)</b>	65.2																					

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.36	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	65.2	59.0
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	7.4	8.4

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	138	m
<b>Average Slope</b>	10.5	%
<b>Airport</b>	13.0	min.
<b>Bransby - Williams</b>	5.1	min.
		Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	10.1	min.
	0.17	hr.

Composite Parameters		
<b>Drainage Area</b>	0.75 ha	
<b>Runoff Coefficient</b>	0.36	
<b>SCS Curve No.</b>	65.2	59.0
<b>Modified Curve No.<sup>4</sup>, CN*</b>	68.1	61.7
<b>Initial Abstraction.</b>	7.4	8.4

**Notes:**

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

### Hydrologic Parameters for PR-201

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use					Rainfall Data	
	Controlled Lots	Controlled Roadway	External			
Agriculture	0.00	0.00	0.00	ha	Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm	
Range	0.00	0.00	0.24	ha		
Grass	0.41	0.30	0.00	ha	Drainage Area 1.28 ha Impervious Area 0.31 ha Percent Impervious 24.6% Connected Impervious 24.6%  Pervious Length 100 m US Elev 213.2 m DS Elev 206.6 m Slope 6.6 % Hilly	
Woods	0.00	0.00	0.00	ha		
Wetland	0.00	0.00	0.00	ha		
Gravel	0.00	0.00	0.00	ha		
Impervious	0.05	0.25	0.02	ha		
<b>SUM</b>	<b>0.46</b>	<b>0.55</b>	<b>0.26</b>			
Hydrologic Soil Group <sup>1</sup>	B	B	B			
Soil Type	0	0	0			
<b>C</b>	0.26	0.51	0.34			
<b>CN (Nashyd)</b>	<b>64.7</b>	<b>77.7</b>	<b>67.3</b>			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient <sup>2</sup> , C	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.26	
	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.51	
	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.34	n.a.
SCS Curve No. <sup>3</sup> , CN	B	74	65	61	58	50	85	98	64.7	61.0
	B	74	65	61	58	50	85	98	77.7	61.0
	B	74	65	61	58	50	85	98	67.3	65.0
Initial Abstraction <sup>5</sup> , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.8	5.8

Time of Concentration <sup>6</sup>		
Total Length	100	m
Average Slope	6.6	%
Airport	12.5	min.
Bransby - Williams	3.8	min.
Applicable Minimum <sup>7</sup>	15.0	min.
Time to Peak	10.1	min.
	0.17	hr.

Flat: 0-2% Slopes  
 Rolling: 2-6% Slopes  
 Hilly: >6% Slopes

Composite Parameters		
Drainage Area	1.28 ha	
Runoff Coefficient	0.39	
SCS Curve No.	70.9	62.0
Modified Curve No. <sup>4</sup> , CN*	72.2	62.5
Initial Abstraction.	4.8	5.8

**Notes:**

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

**Hydrologic Parameters for PR-202**

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use				Rainfall Data	
	<b>Uncontrolled Lots</b>	<b>Uncontrolled Roadway</b>		<b>Gauging Station =</b> Peterborough <b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Agriculture	0.00	0.00	ha		
Range	0.00	0.00	ha		
Grass	1.09	0.10	ha		
Woods	0.00	0.00	ha		
Wetland	0.00	0.00	ha		
Gravel	0.00	0.00	ha		
Impervious	0.12	0.09	ha		
<b>SUM</b>	<b>1.21</b>	<b>0.19</b>		<b>Drainage Area</b> 1.40 ha <b>Impervious Area</b> 0.21 ha <b>Percent Impervious</b> 14.8% Connected Impervious 14.8%	
<b>Hydrologic Soil Group<sup>1</sup></b>	B	B		<b>Pervious</b> <b>Length</b> 100 m <b>US Elev</b> 213.2 m <b>DS Elev</b> 206.6 m <b>Slope</b> 6.6 % Hilly	
<b>Soil Type</b>	0	0			
<b>C</b>	0.26	0.51			
<b>CN (Nashyd)</b>	64.7	77.7			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.26	
	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.51	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	64.7	61.0
	B	74	65	61	58	50	85	98	77.7	61.0
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.6	5.0

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	100	m
<b>Average Slope</b>	6.6	%
<b>Airport</b>	14.1	min.
<b>Bransby - Williams</b>	3.8	min.
		Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	10.1	min.
	0.17	hr.

Composite Parameters		
<b>Drainage Area</b>	1.40	ha
<b>Runoff Coefficient</b>	0.29	
<b>SCS Curve No.</b>	66.5	61.0
<b>Modified Curve No.<sup>4</sup>, CN*</b>	67.1	60.5
<b>Initial Abstraction.</b>	4.6	5.0

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

**Hydrologic Parameters for PR-300**

Sheet 1 of 1



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** RC/CPB  
**Date:** 22-Feb-22

Land Use			Rainfall Data	
	<b>Internal</b>		<b>Gauging Station =</b> Peterborough	
Agriculture	0.00	ha	<b>12 hr, 100 Yr Rainfall =</b> 90.4 mm	
Range	3.90	ha		
Grass	0.99	ha		
Woods	3.47	ha		
Wetland	0.00	ha		
Gravel	0.00	ha		
Impervious	0.14	ha		
<b>SUM</b>	<b>8.50</b>			
<b>Hydrologic Soil Group<sup>1</sup></b>	B		<b>Drainage Area</b>	8.50 ha
<b>Soil Type</b>	0		<b>Impervious Area</b>	0.14 ha
<b>C</b>	0.18		<b>Percent Impervious</b>	1.6%
<b>CN (Nashyd)</b>	62.2		Connected Impervious	1.6%
			<b>Pervious</b>	
			<b>Length</b>	330 m
			<b>US Elev</b>	213.5 m
			<b>DS Elev</b>	200.9 m
			<b>Slope</b>	3.8 %
				Rolling

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.18	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	62.2	61.6
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.4	8.5

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	330	m
<b>Average Slope</b>	3.8	%
<b>Airport</b>	35.2	min.
<b>Bransby - Williams</b>	11.6	min.
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	23.6	min.
	0.39	hr.

Composite Parameters		
<b>Drainage Area</b>	8.50	ha
<b>Runoff Coefficient</b>	0.18	
<b>SCS Curve No.</b>	62.2	61.6
<b>Modified Curve No.<sup>4</sup>, CN*</b>	64.4	63.7
<b>Initial Abstraction.</b>	8.4	8.5

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

**Hydrologic Parameters for PR-400**

Sheet 1 of 1



Project No: 19-10874  
 Project Name: Life at the Woodland  
 Designed/Checked By: RC/CPB  
 Date: 22-Feb-22

Land Use			Rainfall Data	
	<u>Internal</u>		Gauging Station = Peterborough	
Agriculture	0.00	ha	12 hr, 100 Yr Rainfall = 90.4 mm	
Range	0.00	ha		
Grass	0.51	ha		
Woods	0.00	ha		
Wetland	0.00	ha		
Gravel	0.00	ha		
Impervious	0.07	ha		
<b>SUM</b>	<b>0.58</b>			
<b>Drainage Area</b>	<b>0.58</b>	ha		
<b>Impervious Area</b>	<b>0.07</b>	ha		
<b>Percent Impervious</b>	<b>12.1%</b>			
Connected Impervious	12.1%			
			<b>Pervious</b>	
<b>Length</b>	165	m		
<b>US Elev</b>	211.6	m		
<b>DS Elev</b>	204.8	m		
<b>Slope</b>	4.1	%		
			Rolling	
<b>Hydrologic Soil Group<sup>1</sup></b>	B			
<b>Soil Type</b>	0			
<b>C</b>	0.22			
<b>CN (Nashyd)</b>	65.5			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
<b>Runoff Coefficient<sup>2</sup>, C</b>	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.22	n.a.
<b>SCS Curve No.<sup>3</sup>, CN</b>	B	74	65	61	58	50	85	98	65.5	61.0
<b>Initial Abstraction<sup>5</sup>, mm</b>		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.6	5.0

Time of Concentration <sup>6</sup>		
<b>Total Length</b>	165	m
<b>Average Slope</b>	4.1	%
<b>Airport</b>	23.0	min.
<b>Bransby - Williams</b>	7.5	min.
		Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
<b>Applicable Minimum<sup>7</sup></b>	15.0	min.
<b>Time to Peak</b>	15.4	min.
	0.26	hr.

Composite Parameters		
<b>Drainage Area</b>	0.58	ha
<b>Runoff Coefficient</b>	0.22	
<b>SCS Curve No.</b>	65.5	61.0
<b>Modified Curve No.<sup>4</sup>, CN*</b>	66.1	60.5
<b>Initial Abstraction.</b>	4.6	5.0

**Notes:**

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

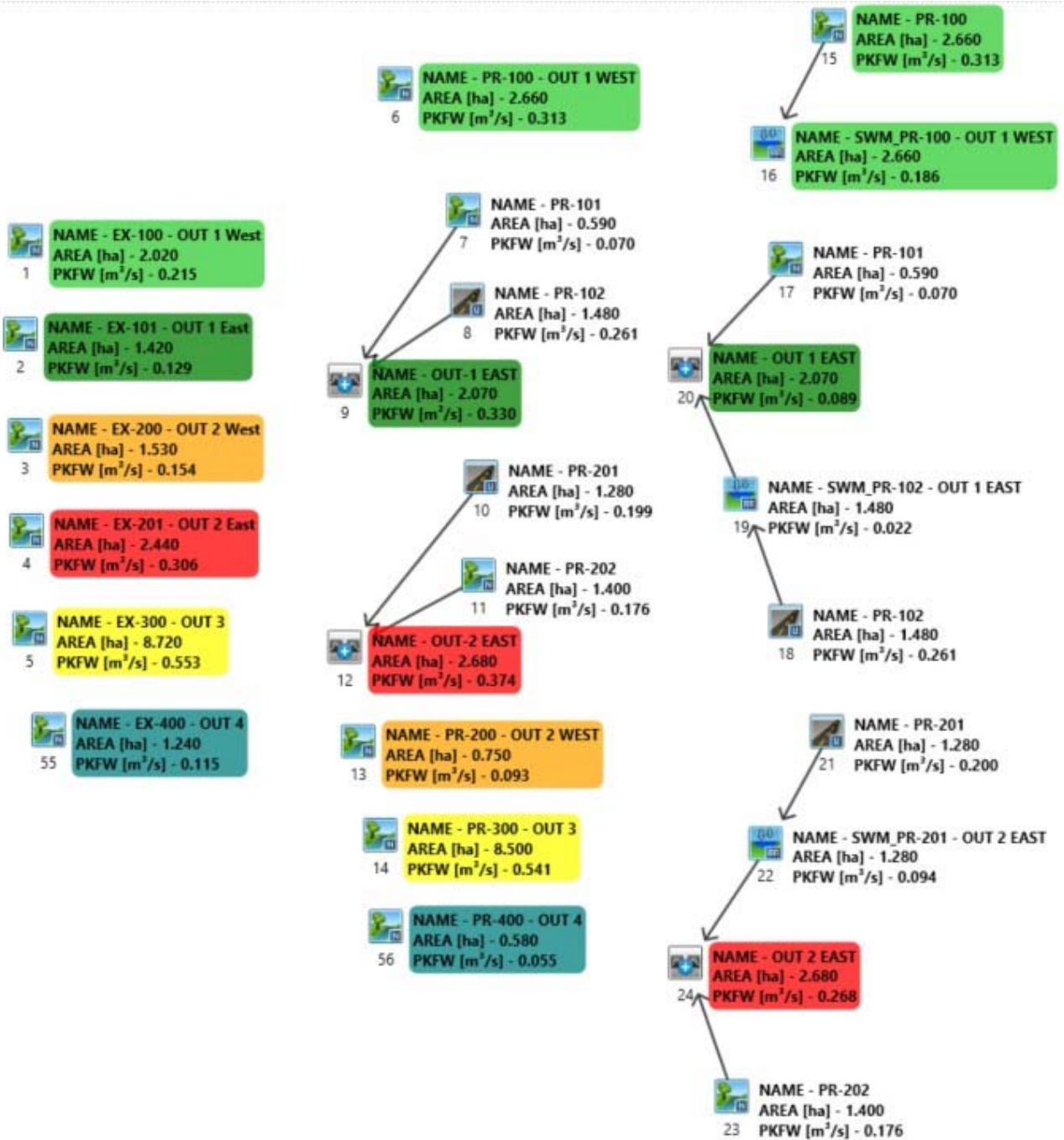
# Appendix B

---

Hydrologic Modelling



# VO3 Analysis



```

=====
V V I SSSSS U U A A L
V V I SS U U A A L
V V I SS U U A A A A L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

```

```

OOO TTTT TTTT H H Y Y M M OOO TM
O O T T H H Y Y MM MM O O
O O T T H H Y Y M M O O
OOO T T H H Y Y M M OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\VO Suite  
 3.0\VO2\voindat  
 Output filename:  
 C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-f4b8f2008ce1\Scenario.out  
 Summary filename:  
 C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-f4b8f2008ce1\Scenario.sum

DATE: 02-24-2022 TIME: 12:58:03

USER:

COMMENTS:

```

*****
** SIMULATION NUMBER: 1 **
*****

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
4.58	2.30	0.083	1.60	1.583	3.90	3.083	8.50
4.67	2.30	0.167	1.60	1.667	3.90	3.167	8.50
4.75	2.30	0.250	1.60	1.750	3.90	3.250	8.50
4.83	2.30	0.333	1.60	1.833	3.90	3.333	8.50
4.92	2.30	0.417	1.60	1.917	3.90	3.417	8.50
5.00	2.30	0.500	1.60	2.000	3.90	3.500	8.50
5.08	1.60	0.583	2.30	2.083	4.60	3.583	3.90
5.17	1.60	0.667	2.30	2.167	4.60	3.667	3.90
5.25	1.60	0.750	2.30	2.250	4.60	3.750	3.90
5.33	1.60	0.833	2.30	2.333	4.60	3.833	3.90
5.42	1.60	0.917	2.30	2.417	4.60	3.917	3.90
5.50	1.60	1.000	2.30	2.500	4.60	4.000	3.90
5.58	1.60	1.083	2.30	2.583	23.20	4.083	3.10
5.67	1.60	1.167	2.30	2.667	23.20	4.167	3.10
5.75	1.60	1.250	2.30	2.750	23.20	4.250	3.10
5.83	1.60	1.333	2.30	2.833	60.40	4.333	3.10
5.92	1.60	1.417	2.30	2.917	60.40	4.417	3.10
6.00	1.60	1.500	2.30	3.000	60.40	4.500	3.10

Unit Hyd Qpeak (cms)= 0.247  
 PEAK FLOW (cms)= 0.020 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 4.927  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.127

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| READ STORM |
|-----|
| f4b8f2008ce1\227bdd08 |
| Ptotal= 38.75 mm |
| Peterborough |
|-----|

```

Filename: C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-f4b8f2008ce1\227bdd08  
 Comments: 2-Year, 6 hour SCS Type II - Peterborough

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.60	1.75	3.90	3.25	8.50		
4.75	2.30	0.50	1.60	2.00	3.90	3.50	8.50
5.00	2.30	0.75	2.30	2.25	4.60	3.75	3.90
5.25	1.60	1.00	2.30	2.50	4.60	4.00	3.90
5.50	1.60	1.25	2.30	2.75	23.20	4.25	3.10
5.75	1.60	1.50	2.30	3.00	60.40	4.50	3.10
6.00	1.60						

```

-----
| CALIB |
| NASHYD (0002) | Area (ha)= 1.42 Curve Number
| (CN)= 63.1 |
| ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear
| Res.(N)= 3.00 |
|-----|
| U.H. Tp(hrs)= 0.22 |

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN TIME RAIN TIME RAIN TIME RAIN
hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr

```

```

-----
| CALIB |
| NASHYD (0001) | Area (ha)= 2.02 Curve Number
| (CN)= 61.5 |
| ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear
| Res.(N)= 3.00 |
|-----|
| U.H. Tp(hrs)= 0.17 |

```

Unit Hyd Qpeak (cms)= 0.454  
 PEAK FLOW (cms)= 0.042 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 5.793  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.149

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0015) | Area (ha)= 2.66 Curve Number
| (CN)= 64.8 |
| ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear
| Res.(N)= 3.00 |
|-----|
| U.H. Tp(hrs)= 0.17 |

```

Unit Hyd Qpeak (cms)= 0.598  
 PEAK FLOW (cms)= 0.063 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 6.680  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.172

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0016) |
| IN= 2--> OUT= 1 |
| DT= 5.0 min |
|-----|
| OUTFLOW STORAGE | OUTFLOW STORAGE

```

```

----- (cms) (ha.m.) | (cms)
(ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
0.0171 0.0001 0.0072 | 0.1306
0.0194 0.0065 0.0083 | 0.1492
0.0220 0.0242 0.0096 | 0.1656
0.0248 0.0501 0.0112 | 0.1806
0.0278 0.0806 0.0129 | 0.1944
0.0000 0.1098 0.0149 | 0.0000

```

```

R.V. AREA QPEAK TPEAK
(mm) (ha) (cms) (hrs)
INFLOW : ID= 2 (0015) 2.660 0.063 3.08
OUTFLOW: ID= 1 (0016) 2.660 0.020 3.58
3.97

```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 31.42
TIME SHIFT OF PEAK FLOW (min)= 30.00
MAXIMUM STORAGE USED (ha.m.)=
0.0093

```

```

-----
| CALIB |
| NASHYD (0004) | Area (ha)= 2.44 Curve Number
(CN)= 68.8
|ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

```

Unit Hyd Qpeak (cms)= 0.548
PEAK FLOW (cms)= 0.056 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 6.456
TOTAL RAINFALL (mm)= 38.750
RUNOFF COEFFICIENT = 0.167

```

```

| STANDHYD (0008) | Area (ha)= 1.48
|ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)=
23.00

```

```

IMPERVIOUS PVIOUS (i)
Surface Area (ha)= 0.34 1.14
Dep. Storage (mm)= 1.00 5.30
Average Slope (%)= 2.00 5.00
Length (m)= 99.33 40.00
Mannings n = 0.013 0.250
Max.Eff.Inten.(mm/hr)= 60.40 9.81
over (min) 5.00 20.00
Storage Coeff. (min)= 2.53 (ii) 16.10 (ii)
Unit Hyd. Tpeak (min)= 5.00 20.00
Unit Hyd. peak (cms)= 0.29 0.06

```

```

*TOTALS*
PEAK FLOW (cms)= 0.06 0.02
0.067 (iii)
TIME TO PEAK (hrs)= 3.00 3.25
3.00
RUNOFF VOLUME (mm)= 37.75 5.65
13.03
TOTAL RAINFALL (mm)= 38.75 38.75
38.75
RUNOFF COEFFICIENT = 0.97 0.15
0.34

```

\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
CN\* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD (0009) |
| 1 + 2 = 3 |
-----
ID1= 1 (0007): 0.59 0.014 3.08 6.76
+ ID2= 2 (0008): 1.48 0.067 3.00 13.03
=====

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0003) | Area (ha)= 1.53 Curve Number
(CN)= 61.7
|ID= 1 DT= 5.0 min | Ia (mm)= 8.70 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

```

Unit Hyd Qpeak (cms)= 0.344
PEAK FLOW (cms)= 0.025 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 4.793
TOTAL RAINFALL (mm)= 38.750
RUNOFF COEFFICIENT = 0.124

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0007) | Area (ha)= 0.59 Curve Number
(CN)= 65.0
|ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

```

Unit Hyd Qpeak (cms)= 0.133
PEAK FLOW (cms)= 0.014 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 6.762
TOTAL RAINFALL (mm)= 38.750
RUNOFF COEFFICIENT = 0.175

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

| CALIB |

```

ID = 3 (0009): 2.07 0.081 3.00 11.24

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0011) | Area (ha)= 1.40 Curve Number
(CN)= 67.1
|ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

```

Unit Hyd Qpeak (cms)= 0.315
PEAK FLOW (cms)= 0.037 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 7.323
TOTAL RAINFALL (mm)= 38.750
RUNOFF COEFFICIENT = 0.189

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD (0010) | Area (ha)= 1.28
|ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.(%)=
24.60

```

```

IMPERVIOUS PVIOUS (i)
Surface Area (ha)= 0.31 0.97
Dep. Storage (mm)= 1.00 5.80
Average Slope (%)= 1.00 6.60
Length (m)= 92.38 100.00
Mannings n = 0.013 0.250
Max.Eff.Inten.(mm/hr)= 60.40 6.94
over (min) 5.00 30.00
Storage Coeff. (min)= 2.98 (ii) 27.82 (ii)
Unit Hyd. Tpeak (min)= 5.00 30.00
Unit Hyd. peak (cms)= 0.28 0.04

```

\*TOTALS\*

PEAK FLOW (cms)= 0.05 0.01  
 0.056 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.42  
 3.00  
 RUNOFF VOLUME (mm)= 37.75 5.86  
 13.69  
 TOTAL RAINFALL (mm)= 38.75 38.75  
 38.75  
 RUNOFF COEFFICIENT = 0.97 0.15  
 0.35

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
 CN\* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0012)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0010):	1.28	0.056	3.00	13.69
+ ID2= 2 (0011):	1.40	0.037	3.08	7.32
=====				
ID = 3 (0012):	2.68	0.092	3.00	10.36

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0005)	Area (ha)	Curve Number (CN)	Ia (mm)	# of Linear Res. (N)	U.H. Tp (hrs)
		8.72	64.6	8.80	3.00	0.39

Unit Hyd Qpeak (cms)= 0.854

PEAK FLOW (cms)= 0.089 (i)  
 TIME TO PEAK (hrs)= 3.333

RUNOFF VOLUME (mm)= 5.303  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.137

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0014)	Area (ha)	Curve Number (CN)	Ia (mm)	# of Linear Res. (N)	U.H. Tp (hrs)
		8.50	64.4	8.40	3.00	0.39

Unit Hyd Qpeak (cms)= 0.832

PEAK FLOW (cms)= 0.089 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 5.393  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.139

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0006)	Area (ha)	Curve Number (CN)	Ia (mm)	# of Linear Res. (N)	U.H. Tp (hrs)
		2.66	64.8	4.80	3.00	0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.063 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 6.680  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.172

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0013)	Area (ha)	Curve Number (CN)	Ia (mm)	# of Linear Res. (N)	U.H. Tp (hrs)
		0.75	68.1	7.40	3.00	0.17

Unit Hyd Qpeak (cms)= 0.169

PEAK FLOW (cms)= 0.017 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 6.514  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.168

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0017)	Area (ha)	Curve Number (CN)	Ia (mm)	# of Linear Res. (N)	U.H. Tp (hrs)
		0.59	65.0	4.70	3.00	0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.014 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 6.762  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.175

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0018)	Area (ha)	Total Imp (%)	Dir. Conn. (%)
		1.48	23.00	

23.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)	0.34	1.14
Dep. Storage (mm)	1.00	5.30
Average Slope (%)	2.00	5.00
Length (m)	99.33	40.00
Mannings n	0.013	0.250

Max.Eff.Inten.(mm/hr) over (min)	60.40	9.81
Storage Coeff. (min)	2.53 (ii)	16.10 (ii)
Unit Hyd. Tpeak (min)	5.00	20.00
Unit Hyd. peak (cms)	0.29	0.06

\*TOTALS\*  
 PEAK FLOW (cms)= 0.06 0.02  
 0.067 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.25  
 3.00  
 RUNOFF VOLUME (mm)= 37.75 5.65  
 13.03  
 TOTAL RAINFALL (mm)= 38.75 38.75  
 38.75  
 RUNOFF COEFFICIENT = 0.97 0.15  
 0.34

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
 CN\* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0019)	IN= 2--> OUT= 1	DT= 5.0 min	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)
			0.0001	0.0074	0.0165

\*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.

0.0238

0.0280	0.0045	0.0089	0.0180
0.0326	0.0084	0.0111	0.0193
0.0376	0.0110	0.0137	0.0206
0.0435	0.0131	0.0166	0.0218
0.0000	0.0149	0.0200	0.0000

R.V.	AREA	QPEAK	TPEAK	
(mm)	(ha)	(cms)	(hrs)	
13.03	INFLOW : ID= 2 (0018)	1.480	0.067	3.00
8.00	OUTFLOW: ID= 1 (0019)	1.480	0.010	3.83

PEAK FLOW REDUCTION [Qout/Qin](%)= 14.63  
 TIME SHIFT OF PEAK FLOW (min)= 50.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0125

ADD HYD (0020)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0017):	0.59	0.014	3.08	6.76
+ ID2= 2 (0019):	1.48	0.010	3.83	8.00
ID = 3 (0020):	2.07	0.020	3.08	7.65

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	(ha)=	Curve Number
NASHYD (0023)	Ia	(mm)=	# of Linear
(CN)= 67.1	1.40	4.60	
ID= 1 DT= 5.0 min			Res. (N)= 3.00

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0022)	OUTFLOW	STORAGE	OUTFLOW
IN= 2--> OUT= 1	(cms)	(ha.m.)	(cms)
DT= 5.0 min	(ha.m.)		
STORAGE	0.0001	0.0052	0.0843
**** WARNING : FIRST	0.0056	0.0066	0.0945
OUTFLOW IS NOT ZERO.	0.0202	0.0082	0.1036
0.0172	0.0402	0.0101	0.1121
0.0200	0.0595	0.0122	0.1199
0.0231	0.0728	0.0146	0.0000
0.0265			
0.0301			
0.0000			

R.V.	AREA	QPEAK	TPEAK	
(mm)	(ha)	(cms)	(hrs)	
13.82	INFLOW : ID= 2 (0021)	1.280	0.057	3.00
9.73	OUTFLOW: ID= 1 (0022)	1.280	0.019	3.08

PEAK FLOW REDUCTION [Qout/Qin](%)= 33.86  
 TIME SHIFT OF PEAK FLOW (min)= 5.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0081

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.037 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 7.323  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.189

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area	(ha)=	Curve Number
STANDHYD (0021)	Ia	(mm)=	# of Linear
ID= 1 DT= 5.0 min	1.28	25.00	Dir. Conn.(%)= 25.00

Surface Area	(ha)=	IMPERVIOUS	PERVIOUS (i)
Dep. Storage	(mm)=	0.32	0.96
Average Slope	(%)=	1.00	5.80
Length	(m)=	92.38	100.00
Mannings n	=	0.013	0.250
Max.Eff.Inten.(mm/hr)=	60.40	6.94	
over (min)=	5.00	30.00	
Storage Coeff. (min)=	2.98 (ii)	27.82 (ii)	
Unit Hyd. Tpeak (min)=	5.00	30.00	
Unit Hyd. peak (cms)=	0.28	0.04	

\*TOTALS\*

PEAK FLOW (cms)=	0.05	0.01
0.057 (iii)		
TIME TO PEAK (hrs)=	3.00	3.42
3.00		
RUNOFF VOLUME (mm)=	37.75	5.86
13.82		
TOTAL RAINFALL (mm)=	38.75	38.75
38.75		
RUNOFF COEFFICIENT =	0.97	0.15
0.36		

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

ADD HYD (0024)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0022):	1.28	0.019	3.08	9.73
+ ID2= 2 (0023):	1.40	0.037	3.08	7.32
ID = 3 (0024):	2.68	0.056	3.08	8.47

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	(ha)=	Curve Number
NASHYD (0055)	Ia	(mm)=	# of Linear
(CN)= 67.5	1.24	8.20	
ID= 1 DT= 5.0 min			Res. (N)= 3.00

U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.182

PEAK FLOW (cms)= 0.020 (i)  
 TIME TO PEAK (hrs)= 3.167  
 RUNOFF VOLUME (mm)= 6.101  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.157

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area	(ha)=	Curve Number
NASHYD (0056)	Ia	(mm)=	# of Linear
(CN)= 66.1	0.58	4.60	
ID= 1 DT= 5.0 min			Res. (N)= 3.00

U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.085

PEAK FLOW (cms)= 0.011 (i)  
 TIME TO PEAK (hrs)= 3.167  
 RUNOFF VOLUME (mm)= 7.087  
 TOTAL RAINFALL (mm)= 38.750  
 RUNOFF COEFFICIENT = 0.183

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 2 \*\*  
\*\*\*\*\*

-----  
 | READ STORM | Filename: C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-  
 f4b8f2008ce1\fcdf25c  
 | Ptotal= 52.45 mm |  
 Peterboroug  
 Comments: 5-Year, 6 hour SCS Type II -  
 -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
4.75	3.20	0.25	2.10	1.75	5.20	3.25	11.50
5.00	3.20	0.50	2.10	2.00	5.20	3.50	11.50
5.25	2.10	0.75	3.20	2.25	6.30	3.75	5.20
5.50	2.10	1.00	3.20	2.50	6.30	4.00	5.20
5.75	2.10	1.25	3.20	2.75	31.40	4.25	4.20
6.00	2.10	1.50	3.20	3.00	81.80	4.50	4.20

-----  
 | CALIB |  
 | NASHYD (0002) | Area (ha)= 1.42 Curve Number  
 (CN)= 63.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.22

PEAK FLOW (cms)= 0.042 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 9.780  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.186

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | NASHYD (0001) | Area (ha)= 2.02 Curve Number  
 (CN)= 61.5  
 |ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.454

PEAK FLOW (cms)= 0.078 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 10.745  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.205

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | NASHYD (0015) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.117 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 12.188  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.232

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME	RAIN	--- TRANSFORMED HYETOGRAPH ---					
		TIME	RAIN	TIME	RAIN		
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr		
4.58	3.20	0.083	2.10	1.583	5.20	3.083	11.50
4.67	3.20	0.167	2.10	1.667	5.20	3.167	11.50
4.75	3.20	0.250	2.10	1.750	5.20	3.250	11.50
4.83	3.20	0.333	2.10	1.833	5.20	3.333	11.50
4.92	3.20	0.417	2.10	1.917	5.20	3.417	11.50
5.00	3.20	0.500	2.10	2.000	5.20	3.500	11.50
5.08	2.10	0.583	3.20	2.083	6.30	3.583	5.20
5.17	2.10	0.667	3.20	2.167	6.30	3.667	5.20
5.25	2.10	0.750	3.20	2.250	6.30	3.750	5.20
5.33	2.10	0.833	3.20	2.333	6.30	3.833	5.20
5.42	2.10	0.917	3.20	2.417	6.30	3.917	5.20
5.50	2.10	1.000	3.20	2.500	6.30	4.000	5.20
5.58	2.10	1.083	3.20	2.583	31.40	4.083	4.20
5.67	2.10	1.167	3.20	2.667	31.40	4.167	4.20
5.75	2.10	1.250	3.20	2.750	31.40	4.250	4.20
5.83	2.10	1.333	3.20	2.833	81.80	4.333	4.20
5.92	2.10	1.417	3.20	2.917	81.80	4.417	4.20
6.00	2.10	1.500	3.20	3.000	81.80	4.500	4.20

Unit Hyd Qpeak (cms)= 0.247

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0016) |  
 | IN= 2---> OUT= 1 |  
 | DT= 5.0 min |  
 STORAGE  
 (ha.m.)  
 -----  
 (cms) (ha.m.) (cms)

\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0171 0.0001 0.0072 0.1306  
 0.0194 0.0065 0.0083 0.1492  
 0.0220 0.0242 0.0096 0.1656  
 0.0248 0.0501 0.0112 0.1806  
 0.0278 0.0806 0.0129 0.1944  
 0.0000 0.1098 0.0149 0.0000

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
12.19	INFLOW : ID= 2 (0015)	2.660	0.117 3.08
9.47	OUTFLOW : ID= 1 (0016)	2.660	0.068 3.25

PEAK FLOW REDUCTION [Qout/Qin](%)= 58.45  
 TIME SHIFT OF PEAK FLOW (min)= 10.00  
 MAXIMUM STORAGE USED (ha.m.)=  
 0.0123

-----  
 | CALIB |  
 | NASHYD (0004) | Area (ha)= 2.44 Curve Number  
 (CN)= 68.8  
 |ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear  
 Res. (N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.110 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 12.333
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.235

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.235

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0003) Area (ha)= 1.53 Curve Number
(CN)= 61.7
ID= 1 DT= 5.0 min Ia (mm)= 8.70 # of Linear
Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.344

PEAK FLOW (cms)= 0.052 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 9.469
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.181

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0007) Area (ha)= 0.59 Curve Number
(CN)= 65.0
ID= 1 DT= 5.0 min Ia (mm)= 4.70 # of Linear
Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.026 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 12.312

CALIB STANDHYD (0008) Area (ha)= 1.48
ID= 1 DT= 5.0 min Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 0.34 1.14
Dep. Storage (mm)= 1.00 5.30
Average Slope (%)= 2.00 5.00
Length (m)= 99.33 40.00
Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 81.80 18.50
over (min) 5.00 15.00
Storage Coeff. (min)= 2.24 (ii) 12.77 (ii)
Unit Hyd. Tpeak (min)= 5.00 15.00
Unit Hyd. peak (cms)= 0.30 0.08

\*TOTALS\*
PEAK FLOW (cms)= 0.08 0.04
0.107 (iii)
TIME TO PEAK (hrs)= 3.00 3.08
3.00
RUNOFF VOLUME (mm)= 51.45 10.51
19.92
TOTAL RAINFALL (mm)= 52.45 52.45
52.45
RUNOFF COEFFICIENT = 0.98 0.20

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN\* = 60.7 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0009)
1 + 2 = 3
AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
ID1= 1 (0007): 0.59 0.026 3.08 12.31
+ ID2= 2 (0008): 1.48 0.107 3.00 19.92
=====
ID = 3 (0009): 2.07 0.133 3.00 17.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0011) Area (ha)= 1.40 Curve Number
(CN)= 67.1
ID= 1 DT= 5.0 min Ia (mm)= 4.60 # of Linear
Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.067 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 13.234
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.252

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 81.80 15.49
over (min) 5.00 25.00
Storage Coeff. (min)= 2.64 (ii) 20.66 (ii)
Unit Hyd. Tpeak (min)= 5.00 25.00
Unit Hyd. peak (cms)= 0.29 0.05

\*TOTALS\*
PEAK FLOW (cms)= 0.07 0.02
0.083 (iii)
TIME TO PEAK (hrs)= 3.00 3.33
3.00
RUNOFF VOLUME (mm)= 51.45 10.93
20.89
TOTAL RAINFALL (mm)= 52.45 52.45
52.45
RUNOFF COEFFICIENT = 0.98 0.21
0.40

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN\* = 62.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0010) Area (ha)= 1.28
ID= 1 DT= 5.0 min Total Imp(%)= 24.60 Dir. Conn.(%)= 24.60

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 0.31 0.97
Dep. Storage (mm)= 1.00 5.80
Average Slope (%)= 1.00 6.60
Length (m)= 92.38 100.00

ADD HYD (0012)
1 + 2 = 3
AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
ID1= 1 (0010): 1.28 0.083 3.00 20.89
+ ID2= 2 (0011): 1.40 0.067 3.08 13.23
=====
ID = 3 (0012): 2.68 0.149 3.00 16.89

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB

NASHYD (0005) | Area (ha)= 8.72 Curve Number  
 (CN)= 64.6  
 |ID= 1 DT= 5.0 min | Ia (mm)= 8.80 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.854

PEAK FLOW (cms)= 0.184 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 10.419  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.199

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0014) | Area (ha)= 8.50 Curve Number  
 (CN)= 64.4  
 |ID= 1 DT= 5.0 min | Ia (mm)= 8.40 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.832

PEAK FLOW (cms)= 0.182 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 10.518  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.201

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0006) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0018) | Area (ha)= 1.48  
 |ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)	0.34	1.14
Dep. Storage (mm)	1.00	5.30
Average Slope (%)	2.00	5.00
Length (m)	99.33	40.00
Mannings n	0.013	0.250
Max.Eff.Inten.(mm/hr)	81.80	18.50
over (min)	5.00	15.00
Storage Coeff. (min)	2.24 (ii)	12.77 (ii)
Unit Hyd. Tpeak (min)	5.00	15.00
Unit Hyd. peak (cms)	0.30	0.08

\*TOTALS\*

PEAK FLOW (cms)= 0.08 0.04  
 0.107 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.08  
 3.00  
 RUNOFF VOLUME (mm)= 51.45 10.51  
 19.92  
 TOTAL RAINFALL (mm)= 52.45 52.45  
 52.45  
 RUNOFF COEFFICIENT = 0.98 0.20  
 0.38

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 60.7 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0019) |

PEAK FLOW (cms)= 0.117 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 12.188  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.232

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0013) | Area (ha)= 0.75 Curve Number  
 (CN)= 68.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 7.40 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.169

PEAK FLOW (cms)= 0.034 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 12.328  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.235

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0017) | Area (ha)= 0.59 Curve Number  
 (CN)= 65.0  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.026 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 12.312  
 TOTAL RAINFALL (mm)= 52.450  
 RUNOFF COEFFICIENT = 0.235

IN= 2---> OUT= 1 |  
 DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW  
 STORAGE  
 (ha.m.) (cms) (ha.m.) | (cms)

\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0001 0.0074 | 0.0165  
 0.0238 0.0045 0.0089 | 0.0180  
 0.0280 0.0084 0.0111 | 0.0193  
 0.0326 0.0110 0.0137 | 0.0206  
 0.0376 0.0131 0.0166 | 0.0218  
 0.0435 0.0149 0.0200 | 0.0000  
 0.0000

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
INFLOW : ID= 2 (0018)	1.480	0.107	3.00
19.92			
OUTFLOW : ID= 1 (0019)	1.480	0.014	3.83
14.89			

PEAK FLOW REDUCTION [Qout/Qin](%)= 13.40  
 TIME SHIFT OF PEAK FLOW (min)= 50.00  
 MAXIMUM STORAGE USED (ha.m.)=

ADD HYD (0020) |  
 | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0017): 0.59 0.026 3.08 12.31  
 + ID2= 2 (0019): 1.48 0.014 3.83 14.89  
 ID = 3 (0020): 2.07 0.038 3.08 14.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0023) | Area (ha)= 1.40 Curve Number
(CN)= 67.1
|ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.067 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 13.234
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.252

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD (0021) | Area (ha)= 1.28
|ID= 1 DT= 5.0 min | Total Imp(%)= 25.00 Dir. Conn.(%)=
25.00
-----
IMPERVIOUS PVIOUS (i)
Surface Area (ha)= 0.32 0.96
Dep. Storage (mm)= 1.00 5.80
Average Slope (%)= 1.00 6.60
Length (m)= 92.38 100.00
Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 81.80 15.49
over (min) 5.00 25.00
Storage Coeff. (min)= 2.64 (ii) 20.66 (ii)
Unit Hyd. Tpeak (min)= 5.00 25.00
Unit Hyd. peak (cms)= 0.29 0.05

```

```

*TOTALS*
PEAK FLOW (cms)= 0.07 0.02
0.084 (iii)
TIME TO PEAK (hrs)= 3.00 3.33
3.00

```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 50.74
TIME SHIFT OF PEAK FLOW (min)= 5.00
MAXIMUM STORAGE USED (ha.m.)=

```

0.0105

```

-----
| ADD HYD (0024) |
| 1 + 2 = 3 |
-----
ID1= 1 (0022): 1.28 0.043 3.08 16.96
+ ID2= 2 (0023): 1.40 0.067 3.08 13.23
-----
ID = 3 (0024): 2.68 0.110 3.08 15.01

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0055) | Area (ha)= 1.24 Curve Number
(CN)= 67.5
|ID= 1 DT= 5.0 min | Ia (mm)= 8.20 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.182

PEAK FLOW (cms)= 0.040 (i)
TIME TO PEAK (hrs)= 3.167
RUNOFF VOLUME (mm)= 11.748
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.224

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0056) | Area (ha)= 0.58 Curve Number
(CN)= 66.1
|ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
Res.(N)= 3.00

```

```

RUNOFF VOLUME (mm)= 51.45 10.93
21.05
TOTAL RAINFALL (mm)= 52.45 52.45
52.45
RUNOFF COEFFICIENT = 0.98 0.21
0.40

```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
CN\* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0022) |
| IN= 2--> OUT= 1 |
| DT= 5.0 min |
STORAGE OUTFLOW STORAGE OUTFLOW
(ha.m.) (cms) (ha.m.) (cms)
-----
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
0.0172 0.0001 0.0052 0.0843
0.0200 0.0056 0.0066 0.0945
0.0231 0.0202 0.0082 0.1036
0.0265 0.0402 0.0101 0.1121
0.0301 0.0595 0.0122 0.1199
0.0000 0.0728 0.0146 0.0000

AREA QPEAK TPEAK
R.V. (ha) (cms) (hrs)
(mm)
INFLOW : ID= 2 (0021) 1.280 0.084 3.00
21.05
OUTFLOW: ID= 1 (0022) 1.280 0.043 3.08
16.96

```

U.H. Tp(hrs)= 0.26

```

Unit Hyd Qpeak (cms)= 0.085

PEAK FLOW (cms)= 0.021 (i)
TIME TO PEAK (hrs)= 3.167
RUNOFF VOLUME (mm)= 12.845
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.245

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

*****
** SIMULATION NUMBER: 3 **
*****

```

```

-----
| READ STORM |
| |
| Ptotal= 61.60 mm |
-----
Filename: C:\Users\mwilson\AppData
Local\Temp\
ad98c7d6-b765-49b3-b3b5-
f4b8f2008cel\b881660d
Comments: 10-Year, 6 hour SCS Type II -
Peterborou

-----
TIME RAIN TIME RAIN TIME RAIN TIME RAIN
hrs mm/hr hrs mm/hr | hrs mm/hr | hrs mm/hr |
4.75 3.70 0.25 2.50 | 1.75 6.20 | 3.25 13.50 |
5.00 3.70 0.50 2.50 | 2.00 6.20 | 3.50 13.50 |
5.25 2.50 0.75 3.70 | 2.25 7.40 | 3.75 6.20 |
5.50 2.50 1.00 3.70 | 2.50 7.40 | 4.00 6.20 |
5.75 2.50 1.25 3.70 | 2.75 36.90 | 4.25 4.90 |
6.00 2.50 1.50 3.70 | 3.00 95.90 | 4.50 4.90 |
-----

```

```

-----
| CALIB          |
| NASHYD (0002) | Area (ha)= 1.42 Curve Number
(CN)= 63.1
|ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.22

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME	RAIN	--- TRANSFORMED HYETOGRAPH ---					
		TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	2.50	1.583	6.20	3.083	13.50		
4.58	3.70	1.667	6.20	3.167	13.50		
4.67	3.70	1.750	6.20	3.250	13.50		
4.75	3.70	1.833	6.20	3.333	13.50		
4.83	3.70	1.917	6.20	3.417	13.50		
4.92	3.70	2.000	6.20	3.500	13.50		
5.00	3.70	2.083	7.40	3.583	6.20		
5.08	2.50	2.167	7.40	3.667	6.20		
5.17	2.50	2.250	7.40	3.750	6.20		
5.25	2.50	2.333	7.40	3.833	6.20		
5.33	2.50	2.417	7.40	3.917	6.20		
5.42	2.50	2.500	7.40	4.000	6.20		
5.50	2.50	2.583	36.90	4.083	4.90		
5.58	2.50	2.667	36.90	4.167	4.90		
5.67	2.50	2.750	36.90	4.250	4.90		
5.75	2.50						

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.159 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 16.505  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.268

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0016) |
| IN= 2--> OUT= 1 |
| DT= 5.0 min      |
STORAGE
-----
(ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.

```

OUTFLOW	STORAGE	OUTFLOW
(cms)	(ha.m.)	(cms)
0.0001	0.0072	0.1306
0.0065	0.0083	0.1492
0.0242	0.0096	0.1656
0.0501	0.0112	0.1806
0.0806	0.0129	0.1944
0.1098	0.0149	0.0000

```

R.V.
(mm)
INFLOW : ID= 2 (0015) 2.660 0.159 3.08
OUTFLOW: ID= 1 (0016) 2.660 0.104 3.25
13.79

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 65.62  
 TIME SHIFT OF PEAK FLOW (min)= 10.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0146

5.83	2.50	1.333	3.70	2.833	95.90	4.333	4.90
		1.417	3.70	2.917	95.90	4.417	4.90
5.92	2.50	1.500	3.70	3.000	95.90	4.500	4.90
6.00	2.50						

Unit Hyd Qpeak (cms)= 0.247

PEAK FLOW (cms)= 0.060 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 13.692  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.222

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB          |
| NASHYD (0001) | Area (ha)= 2.02 Curve Number
(CN)= 61.5
|ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.17

```

Unit Hyd Qpeak (cms)= 0.454

PEAK FLOW (cms)= 0.107 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 14.669  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.238

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB          |
| NASHYD (0015) | Area (ha)= 2.66 Curve Number
(CN)= 64.8
|ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.17

```

```

-----
| CALIB          |
| NASHYD (0004) | Area (ha)= 2.44 Curve Number
(CN)= 68.8
|ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.17

```

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.151 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 16.960  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.275

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB          |
| NASHYD (0003) | Area (ha)= 1.53 Curve Number
(CN)= 61.7
|ID= 1 DT= 5.0 min | Ia (mm)= 8.70 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.17

```

Unit Hyd Qpeak (cms)= 0.344

PEAK FLOW (cms)= 0.073 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 13.242  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.215

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB          |
| NASHYD (0007) | Area (ha)= 0.59 Curve Number
(CN)= 65.0

```

| ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17  
 Unit Hyd Qpeak (cms)= 0.133  
 PEAK FLOW (cms)= 0.035 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 16.657  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.270

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD (0008) | Area (ha)= 1.48  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00  
 -----  
 IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= 0.34 1.14  
 Dep. Storage (mm)= 1.00 5.30  
 Average Slope (%)= 2.00 5.00  
 Length (m)= 99.33 40.00  
 Mannings n = 0.013 0.250  
 Max.Eff.Inten.(mm/hr)= 95.90 28.35  
 over (min)= 5.00 15.00  
 Storage Coeff. (min)= 2.10 (ii) 10.98 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 15.00  
 Unit Hyd. peak (cms)= 0.31 0.09

\*TOTALS\*  
 PEAK FLOW (cms)= 0.09 0.05  
 0.136 (iii) TIME TO PEAK (hrs)= 3.00 3.08  
 3.00 RUNOFF VOLUME (mm)= 60.60 14.36  
 24.99 TOTAL RAINFALL (mm)= 61.60 61.60  
 61.60 RUNOFF COEFFICIENT = 0.98 0.23  
 0.41

| ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.(%)= 24.60  
 -----  
 IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= 0.31 0.97  
 Dep. Storage (mm)= 1.00 5.80  
 Average Slope (%)= 1.00 6.60  
 Length (m)= 92.38 100.00  
 Mannings n = 0.013 0.250  
 Max.Eff.Inten.(mm/hr)= 95.90 26.51  
 over (min)= 5.00 20.00  
 Storage Coeff. (min)= 2.48 (ii) 17.02 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 20.00  
 Unit Hyd. peak (cms)= 0.29 0.06

\*TOTALS\*  
 PEAK FLOW (cms)= 0.08 0.04  
 0.108 (iii) TIME TO PEAK (hrs)= 3.00 3.17  
 3.00 RUNOFF VOLUME (mm)= 60.60 14.96  
 26.18 TOTAL RAINFALL (mm)= 61.60 61.60  
 61.60 RUNOFF COEFFICIENT = 0.98 0.24  
 0.42

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | ADD HYD (0012) |  
 | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0010): 1.28 0.108 3.00 26.18  
 + ID2= 2 (0011): 1.40 0.090 3.08 17.83  
 -----  
 ID = 3 (0012): 2.68 0.196 3.00 21.82

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | ADD HYD (0009) |  
 | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0007): 0.59 0.035 3.08 16.66  
 + ID2= 2 (0008): 1.48 0.136 3.00 24.99  
 -----  
 ID = 3 (0009): 2.07 0.171 3.00 22.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB |  
 | NASHYD (0011) | Area (ha)= 1.40 Curve Number  
 (CN)= 67.1  
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17  
 Unit Hyd Qpeak (cms)= 0.315  
 PEAK FLOW (cms)= 0.090 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 17.833  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.289

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD (0010) | Area (ha)= 1.28

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB |  
 | NASHYD (0005) | Area (ha)= 8.72 Curve Number  
 (CN)= 64.6  
 | ID= 1 DT= 5.0 min | Ia (mm)= 8.80 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.39  
 Unit Hyd Qpeak (cms)= 0.854  
 PEAK FLOW (cms)= 0.261 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 14.519  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.236

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | NASHYD (0014) | Area (ha)= 8.50 Curve Number  
 (CN)= 64.4  
 | ID= 1 DT= 5.0 min | Ia (mm)= 8.40 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.832  
 PEAK FLOW (cms)= 0.256 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 14.616  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.237

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |

NASHYD (0006) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.17  
 Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.159 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 16.505  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.268

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 NASHYD (0013) | Area (ha)= 0.75 Curve Number  
 (CN)= 68.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 7.40 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.17  
 Unit Hyd Qpeak (cms)= 0.169

PEAK FLOW (cms)= 0.046 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 16.902  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.274

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 NASHYD (0017) | Area (ha)= 0.59 Curve Number  
 (CN)= 65.0  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0019) |  
 |IN= 2--> OUT= 1 |  
 |DT= 5.0 min |  
 STORAGE  
 (ha.m.)

\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)
0.0001	0.0074	0.0165
0.0238	0.0045	0.0180
0.0280	0.0084	0.0193
0.0326	0.0110	0.0206
0.0376	0.0131	0.0218
0.0435	0.0149	0.0200
0.0000		

R.V. (mm)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)
INFLOW : ID= 2 (0018)	1.480	0.136	3.00
24.99			
OUTFLOW: ID= 1 (0019)	1.480	0.017	3.83
19.96			

PEAK FLOW REDUCTION [Qout/Qin](%)= 12.25  
 TIME SHIFT OF PEAK FLOW (min)= 50.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0241

ADD HYD (0020)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				

PEAK FLOW (cms)= 0.035 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 16.657  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.270

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 STANDHYD (0018) | Area (ha)= 1.48  
 |ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.34	1.14
Dep. Storage (mm)=	1.00	5.30
Average Slope (%)=	2.00	5.00
Length (m)=	99.33	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	95.90	28.35
over (min)	5.00	15.00
Storage Coeff. (min)=	2.10 (ii)	10.98 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.31	0.09

\*TOTALS\*  
 PEAK FLOW (cms)= 0.09 0.05  
 0.136 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.08  
 3.00  
 RUNOFF VOLUME (mm)= 60.60 14.36  
 24.99  
 TOTAL RAINFALL (mm)= 61.60 61.60  
 61.60  
 RUNOFF COEFFICIENT = 0.98 0.23

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 60.7 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

ID1= 1 (0017):	0.59	0.035	3.08	16.66
+ ID2= 2 (0019):	1.48	0.017	3.83	19.96
ID = 3 (0020):	2.07	0.049	3.08	19.02

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB  
 NASHYD (0023) | Area (ha)= 1.40 Curve Number  
 (CN)= 67.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
 Res.(N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.090 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 17.833  
 TOTAL RAINFALL (mm)= 61.600  
 RUNOFF COEFFICIENT = 0.289

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 STANDHYD (0021) | Area (ha)= 1.28  
 |ID= 1 DT= 5.0 min | Total Imp(%)= 25.00 Dir. Conn.(%)= 25.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.32	0.96
Dep. Storage (mm)=	1.00	5.80
Average Slope (%)=	1.00	6.60
Length (m)=	92.38	100.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	95.90	26.51
over (min)	5.00	20.00
Storage Coeff. (min)=	2.48 (ii)	17.02 (ii)
Unit Hyd. Tpeak (min)=	5.00	20.00
Unit Hyd. peak (cms)=	0.29	0.06



5.50	2.90	1.000	4.40	2.500	8.80	4.000	7.30
5.58	2.90	1.083	4.40	2.583	43.70	4.083	5.80
5.67	2.90	1.167	4.40	2.667	43.70	4.167	5.80
5.75	2.90	1.250	4.40	2.750	43.70	4.250	5.80
5.83	2.90	1.333	4.40	2.833	113.70	4.333	5.80
5.92	2.90	1.417	4.40	2.917	113.70	4.417	5.80
6.00	2.90	1.500	4.40	3.000	113.70	4.500	5.80

Unit Hyd Qpeak (cms)= 0.247

PEAK FLOW (cms)= 0.086 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 19.144  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.263

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 NASHYD (0001) | Area (ha)= 2.02 Curve Number  
 (CN)= 61.5  
 ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear  
 Res. (N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.454

PEAK FLOW (cms)= 0.147 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 20.094  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.276

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

OUTFLOW: ID= 1 (0016) 2.660 0.140 3.25  
 19.71

PEAK FLOW REDUCTION [Qout/Qin](%)= 64.86  
 TIME SHIFT OF PEAK FLOW (min)= 10.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0185

CALIB  
 NASHYD (0004) | Area (ha)= 2.44 Curve Number  
 (CN)= 68.8  
 ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear  
 Res. (N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.210 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 23.305  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.320

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 NASHYD (0003) | Area (ha)= 1.53 Curve Number  
 (CN)= 61.7  
 ID= 1 DT= 5.0 min | Ia (mm)= 8.70 # of Linear  
 Res. (N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.344

PEAK FLOW (cms)= 0.103 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 18.510  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.254

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 NASHYD (0015) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res. (N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.216 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 22.424  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.308

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0016)  
 IN= 2--> OUT= 1  
 DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW  
 STORAGE (cms) (ha.m.) | (cms)

0.0171	0.0001	0.0072	0.1306
0.0194	0.0065	0.0083	0.1492
0.0220	0.0242	0.0096	0.1656
0.0248	0.0501	0.0112	0.1806
0.0278	0.0806	0.0129	0.1944
0.0000	0.1098	0.0149	0.0000

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
INFLOW : ID= 2 (0015)	2.660	0.216	3.08
22.42			

CALIB  
 NASHYD (0007) | Area (ha)= 0.59 Curve Number  
 (CN)= 65.0  
 ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  
 Res. (N)= 3.00

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.048 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 22.611  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.310

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 STANDHYD (0008) | Area (ha)= 1.48  
 ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.34	1.14
Dep. Storage (mm)=	1.00	5.30
Average Slope (%)=	2.00	5.00
Length (m)=	99.33	40.00
Mannings n =	0.013	0.250
Max. Eff. Inten. (mm/hr)=	113.70	38.86
over (min)	5.00	10.00
Storage Coeff. (min)=	1.96 (ii)	9.79 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00
Unit Hyd. Tpeak (cms)=	0.31	0.11

\*TOTALS\*  
 PEAK FLOW (cms)= 0.11 0.08  
 0.190 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.08  
 3.00

RUNOFF VOLUME (mm)= 71.90 19.69  
 31.70  
 TOTAL RAINFALL (mm)= 72.90 72.90  
 72.90  
 RUNOFF COEFFICIENT = 0.99 0.27  
 0.43

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
 CN\* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0009)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0007):	0.59	0.048	3.08	22.61
+ ID2= 2 (0008):	1.48	0.190	3.00	31.70
=====				
ID = 3 (0009):	2.07	0.238	3.00	29.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0011) | Area (ha)= 1.40 Curve Number  
 (CN)= 67.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315  
 PEAK FLOW (cms)= 0.123 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 24.104  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.331

ADD HYD (0012)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0010):	1.28	0.135	3.00	33.15
+ ID2= 2 (0011):	1.40	0.123	3.08	24.10
=====				
ID = 3 (0012):	2.68	0.257	3.00	28.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0005) | Area (ha)= 8.72 Curve Number  
 (CN)= 64.6  
 |ID= 1 DT= 5.0 min | Ia (mm)= 8.80 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.854  
 PEAK FLOW (cms)= 0.369 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 20.209  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.277

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0014) | Area (ha)= 8.50 Curve Number  
 (CN)= 64.4  
 |ID= 1 DT= 5.0 min | Ia (mm)= 8.40 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.832  
 PEAK FLOW (cms)= 0.361 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 20.300  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.278

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANHYD (0010) | Area (ha)= 1.28  
 |ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.(%)= 24.60

IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= 0.31 0.97  
 Dep. Storage (mm)= 1.00 5.80  
 Average Slope (%)= 1.00 6.60  
 Length (m)= 92.38 100.00  
 Mannings n = 0.013 0.250  
 Max.Eff.Inten.(mm/hr)= 113.70 36.62  
 over (min)= 5.00 20.00  
 Storage Coeff. (min)= 2.31 (ii) 15.09 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 20.00  
 Unit Hyd. peak (cms)= 0.30 0.07

\*TOTALS\*  
 PEAK FLOW (cms)= 0.10 0.06  
 0.135 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.17  
 3.00  
 RUNOFF VOLUME (mm)= 71.90 20.51  
 33.15  
 TOTAL RAINFALL (mm)= 72.90 72.90  
 72.90  
 RUNOFF COEFFICIENT = 0.99 0.28  
 0.45

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
 CN\* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0006) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598  
 PEAK FLOW (cms)= 0.216 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 22.424  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.308

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0013) | Area (ha)= 0.75 Curve Number  
 (CN)= 68.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 7.40 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.169  
 PEAK FLOW (cms)= 0.064 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 23.172  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.318

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB

| NASHYD (0017) | Area (ha)= 0.59 Curve Number  
 (CN)= 65.0  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133  
 PEAK FLOW (cms)= 0.048 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 22.611  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.310

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD (0018) | Area (ha)= 1.48  
 |ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.34	1.14
Dep. Storage (mm)=	1.00	5.30
Average Slope (%)=	2.00	5.00
Length (m)=	99.33	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	113.70	38.86
over (min)	5.00	10.00
Storage Coeff. (min)=	1.96 (ii)	9.79 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00
Unit Hyd. peak (cms)=	0.31	0.11

\*TOTALS\*  
 PEAK FLOW (cms)= 0.11 0.08  
 0.190 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.08  
 3.00  
 RUNOFF VOLUME (mm)= 71.90 19.69  
 31.70  
 TOTAL RAINFALL (mm)= 72.90 72.90  
 72.90

RUNOFF COEFFICIENT = 0.99 0.27  
 0.43

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 60.7 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0019) |  
 | IN= 2---> OUT= 1 |  
 | DT= 5.0 min |  
 STORAGE  
 ----- (cms) (ha.m.) | (cms)  
 (ha.m.)

\*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0001 0.0074 | 0.0165  
 0.0238 0.0045 0.0089 | 0.0180  
 0.0280 0.0084 0.0111 | 0.0193  
 0.0326 0.0110 0.0137 | 0.0206  
 0.0376 0.0131 0.0166 | 0.0218  
 0.0435 0.0149 0.0200 | 0.0000  
 0.0000  
 AREA QPEAK TPEAK  
 R.V. (ha) (cms) (hrs)  
 (mm)  
 INFLOW : ID= 2 (0018) 1.480 0.190 3.00  
 31.70  
 OUTFLOW: ID= 1 (0019) 1.480 0.019 3.92  
 26.67

PEAK FLOW REDUCTION [Qout/Qin](%)= 9.99  
 TIME SHIFT OF PEAK FLOW (min)= 55.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0313

Length (m)= 92.38 100.00  
 Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 113.70 36.62  
 over (min) 5.00 20.00  
 Storage Coeff. (min)= 2.31 (ii) 15.09 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 20.00  
 Unit Hyd. peak (cms)= 0.30 0.07

\*TOTALS\*  
 PEAK FLOW (cms)= 0.10 0.06  
 0.137 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.17  
 3.00  
 RUNOFF VOLUME (mm)= 71.90 20.51  
 33.35  
 TOTAL RAINFALL (mm)= 72.90 72.90  
 72.90  
 RUNOFF COEFFICIENT = 0.99 0.28  
 0.46

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 62.5 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0022) |  
 | IN= 2---> OUT= 1 |  
 | DT= 5.0 min |  
 STORAGE  
 ----- (cms) (ha.m.) | (cms)  
 (ha.m.)

\*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0172 0.0001 0.0052 | 0.0843  
 0.0200 0.0056 0.0066 | 0.0945  
 0.0231 0.0202 0.0082 | 0.1036  
 0.0265 0.0402 0.0101 | 0.1121

-----  
 | CALIB |  
 | NASHYD (0023) | Area (ha)= 1.40 Curve Number  
 (CN)= 67.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315  
 PEAK FLOW (cms)= 0.123 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 24.104  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.331

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD (0021) | Area (ha)= 1.28  
 |ID= 1 DT= 5.0 min | Total Imp(%)= 25.00 Dir. Conn.(%)= 25.00  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.32	0.96
Dep. Storage (mm)=	1.00	5.80
Average Slope (%)=	1.00	6.60

0.0301            0.0595    0.0122 |    0.1199  
 0.0728    0.0146 |    0.0000  
 0.0000

R.V.  
 (mm)  
 INFLOW : ID= 2 (0021)    1.280    0.137    3.00  
 33.35  
 OUTFLOW: ID= 1 (0022)    1.280    0.071    3.17  
 29.27

PEAK FLOW REDUCTION [Qout/Qin](%)= 52.21  
 TIME SHIFT OF PEAK FLOW (min)= 10.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0144

RUNOFF VOLUME (mm)= 22.370  
 TOTAL RAINFALL (mm)= 72.900  
 RUNOFF COEFFICIENT = 0.307

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | ADD HYD (0024) |  
 | 1 + 2 = 3 |

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0022):	1.28	0.071	3.17	29.27
+ ID2= 2 (0023):	1.40	0.123	3.08	24.10
=====				
ID = 3 (0024):	2.68	0.194	3.08	26.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB (0055) |  
 | NASHYD (0055) | Area (ha)= 1.24 Curve Number  
 (CN)= 67.5  
 |ID= 1 DT= 5.0 min | Ia (mm)= 8.20 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.182  
 PEAK FLOW (cms)= 0.078 (i)  
 TIME TO PEAK (hrs)= 3.167

-----  
 | READ STORM |  
 | | File name: C:\Users\mwilson\AppData  
 | | Local\Temp\  
 | | ad98c7d6-b765-49b3-b3b5-  
 | | f4b8f2008c61\4694a7c7  
 | | Ptotal= 81.47 mm |  
 | | Comments: 50-Year, 6 hour SCS Type II -  
 | | Peterborough  
 -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	3.30	1.75	8.10	3.25	17.90		
4.75	4.90						

5.00	4.90	0.50	3.30	2.00	8.10	3.50	17.90
5.25	3.30	0.75	4.90	2.25	9.80	3.75	8.10
5.50	3.30	1.00	4.90	2.50	9.80	4.00	8.10
5.75	3.30	1.25	4.90	2.75	48.90	4.25	6.50
6.00	3.30	1.50	4.90	3.00	127.00	4.50	6.50

5.25	3.30	0.750	4.90	2.250	9.80	3.750	8.10
5.33	3.30	0.833	4.90	2.333	9.80	3.833	8.10
5.42	3.30	0.917	4.90	2.417	9.80	3.917	8.10
5.50	3.30	1.000	4.90	2.500	9.80	4.000	8.10
5.58	3.30	1.083	4.90	2.583	48.90	4.083	6.50
5.67	3.30	1.167	4.90	2.667	48.90	4.167	6.50
5.75	3.30	1.250	4.90	2.750	48.90	4.250	6.50
5.83	3.30	1.333	4.90	2.833	127.00	4.333	6.50
5.92	3.30	1.417	4.90	2.917	127.00	4.417	6.50
6.00	3.30	1.500	4.90	3.000	127.00	4.500	6.50

Unit Hyd Qpeak (cms)= 0.247

PEAK FLOW (cms)= 0.107 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 23.680  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.291

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB (0002) |  
 | NASHYD (0002) | Area (ha)= 1.42 Curve Number  
 (CN)= 63.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.22

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

-----  
 | CALIB (0002) |  
 | NASHYD (0002) | Area (ha)= 1.42 Curve Number  
 (CN)= 63.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.22

-----  
 | CALIB (0001) |  
 | NASHYD (0001) | Area (ha)= 2.02 Curve Number  
 (CN)= 61.5  
 |ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.454  
 PEAK FLOW (cms)= 0.180 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 24.585  
 TOTAL RAINFALL (mm)= 81.475

-----  
 | CALIB (0001) |  
 | NASHYD (0001) | Area (ha)= 2.02 Curve Number  
 (CN)= 61.5  
 |ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.454  
 PEAK FLOW (cms)= 0.180 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 24.585  
 TOTAL RAINFALL (mm)= 81.475

RUNOFF COEFFICIENT = 0.302

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0015) Area (ha)= 2.66 Curve Number (CN)= 64.8 ID= 1 DT= 5.0 min Ia (mm)= 4.80 # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.264 (i) TIME TO PEAK (hrs)= 3.083 RUNOFF VOLUME (mm)= 27.291 TOTAL RAINFALL (mm)= 81.475 RUNOFF COEFFICIENT = 0.335

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0016) IN= 2--> OUT= 1 DT= 5.0 min STORAGE (ha.m.)

\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.

Table with 4 columns: Time (hrs), Outflow (cms), Storage (ha.m.), Outflow (cms). Rows include values like 0.0171, 0.0194, 0.0220, 0.0248, 0.0278, 0.0000.

TIME TO PEAK (hrs)= 3.083 RUNOFF VOLUME (mm)= 22.900 TOTAL RAINFALL (mm)= 81.475 RUNOFF COEFFICIENT = 0.281

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0007) Area (ha)= 0.59 Curve Number (CN)= 65.0 ID= 1 DT= 5.0 min Ia (mm)= 4.70 # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.059 (i) TIME TO PEAK (hrs)= 3.083 RUNOFF VOLUME (mm)= 27.504 TOTAL RAINFALL (mm)= 81.475 RUNOFF COEFFICIENT = 0.338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0008) Area (ha)= 1.48 Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00

Table with 3 columns: Parameter, IMPERVIOUS, PERVIOUS (i). Rows include Surface Area, Dep. Storage, Average Slope, Length, Mannings n, Max. Eff. Inten., Storage Coeff., Unit Hyd. Tpeak, Unit Hyd. peak.

Table with 4 columns: R.V. (mm), AREA (ha), QPEAK (cms), TPEAK (hrs). Rows include INFLOW: ID= 2 (0015) and OUTFLOW: ID= 1 (0016).

PEAK FLOW REDUCTION [Qout/Qin](%)= 62.53 TIME SHIFT OF PEAK FLOW (min)= 10.00 MAXIMUM STORAGE USED (ha.m.)=

0.0220

CALIB NASHYD (0004) Area (ha)= 2.44 Curve Number (CN)= 68.8 ID= 1 DT= 5.0 min Ia (mm)= 8.00 # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.257 (i) TIME TO PEAK (hrs)= 3.083 RUNOFF VOLUME (mm)= 28.513 TOTAL RAINFALL (mm)= 81.475 RUNOFF COEFFICIENT = 0.350

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0003) Area (ha)= 1.53 Curve Number (CN)= 61.7 ID= 1 DT= 5.0 min Ia (mm)= 8.70 # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.344

PEAK FLOW (cms)= 0.128 (i)

\*TOTALS\* PEAK FLOW (cms)= 0.12 0.11 0.225 (iii) TIME TO PEAK (hrs)= 3.00 3.08 3.00 RUNOFF VOLUME (mm)= 80.48 24.11 37.07 TOTAL RAINFALL (mm)= 81.48 81.48 81.48 RUNOFF COEFFICIENT = 0.99 0.30 0.46

\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES: CN\* = 60.7 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Table with 5 columns: ADD HYD (0009), AREA (ha), QPEAK (cms), TPEAK (hrs), R.V. (mm). Rows include ID1= 1 (0007), ID2= 2 (0008), ID = 3 (0009).

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0011) Area (ha)= 1.40 Curve Number (CN)= 67.1 ID= 1 DT= 5.0 min Ia (mm)= 4.60 # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.149 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 29.236  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 CALIB  
 STANDHYD (0010) | Area (ha)= 1.28  
 ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.(%)= 24.60  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.31	0.97
Dep. Storage (mm)=	1.00	5.80
Average Slope (%)=	1.00	6.60
Length (m)=	92.38	100.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	127.00	44.89
over (min)	5.00	15.00
Storage Coeff. (min)=	2.21 (ii)	13.99 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.30	0.08

\*TOTALS\*  
 PEAK FLOW (cms)= 0.11 0.07  
 0.172 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.08  
 3.00  
 RUNOFF VOLUME (mm)= 80.48 25.11  
 38.72  
 TOTAL RAINFALL (mm)= 81.48 81.48  
 81.48  
 RUNOFF COEFFICIENT = 0.99 0.31  
 0.48

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

PEAK FLOW (cms)= 0.448 (i)  
 TIME TO PEAK (hrs)= 3.250  
 RUNOFF VOLUME (mm)= 25.010  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.307

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 CALIB  
 NASHYD (0006) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598  
 PEAK FLOW (cms)= 0.264 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 27.291  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.335

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 CALIB  
 NASHYD (0013) | Area (ha)= 0.75 Curve Number  
 (CN)= 68.1  
 ID= 1 DT= 5.0 min | Ia (mm)= 7.40 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.169  
 PEAK FLOW (cms)= 0.078 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 28.320  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.348

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 ADD HYD (0012)  
 1 + 2 = 3  
 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0010): 1.28 0.172 3.00 38.72  
 + ID2= 2 (0011): 1.40 0.149 3.08 29.24  
 -----  
 ID = 3 (0012): 2.68 0.320 3.00 33.77

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 CALIB  
 NASHYD (0005) | Area (ha)= 8.72 Curve Number  
 (CN)= 64.6  
 ID= 1 DT= 5.0 min | Ia (mm)= 8.80 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.854  
 PEAK FLOW (cms)= 0.458 (i)  
 TIME TO PEAK (hrs)= 3.250  
 RUNOFF VOLUME (mm)= 24.926  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.306

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 CALIB  
 NASHYD (0014) | Area (ha)= 8.50 Curve Number  
 (CN)= 64.4  
 ID= 1 DT= 5.0 min | Ia (mm)= 8.40 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.832

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 CALIB  
 NASHYD (0017) | Area (ha)= 0.59 Curve Number  
 (CN)= 65.0  
 ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133  
 PEAK FLOW (cms)= 0.059 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 27.504  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 CALIB  
 STANDHYD (0018) | Area (ha)= 1.48  
 ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.34	1.14
Dep. Storage (mm)=	1.00	5.30
Average Slope (%)=	2.00	5.00
Length (m)=	99.33	40.00
Mannings n =	0.013	0.250

Max.Eff.Inten.(mm/hr)=	127.00	47.44
over (min)	5.00	10.00
Storage Coeff. (min)=	1.88 (ii)	9.10 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00
Unit Hyd. peak (cms)=	0.32	0.12

\*TOTALS\*  
 PEAK FLOW (cms)= 0.12 0.11  
 0.225 (iii)

TIME TO PEAK (hrs)= 3.00 3.08  
 3.00 RUNOFF VOLUME (mm)= 80.48 24.11  
 37.07 TOTAL RAINFALL (mm)= 81.48 81.48  
 81.48 RUNOFF COEFFICIENT = 0.99 0.30  
 0.46

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
CN\* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0019) |  
 | IN= 2--> OUT= 1 |  
 | DT= 5.0 min |  
 STORAGE | OUTFLOW STORAGE | OUTFLOW  
 ----- (cms) (ha.m.) | (cms)  
 (ha.m.)  
 \*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0238 0.0001 0.0074 | 0.0165  
 0.0280 0.0045 0.0089 | 0.0180  
 0.0326 0.0084 0.0111 | 0.0193  
 0.0376 0.0110 0.0137 | 0.0206  
 0.0435 0.0131 0.0166 | 0.0218  
 0.0000 0.0149 0.0200 | 0.0000  
  
 AREA QPEAK TPEAK  
 R.V. (ha) (cms) (hrs)  
 (mm) INFLOW : ID= 2 (0018) 1.480 0.225 3.00  
 37.07

OUTFLOW: ID= 1 (0019) 1.480 0.020 4.00  
 32.04

PEAK FLOW REDUCTION [Qout/Qin](%)= 9.12  
 TIME SHIFT OF PEAK FLOW (min)= 60.00  
 0.0372 MAXIMUM STORAGE USED (ha.m.)=

-----  
 | ADD HYD (0020) |  
 | 1 + 2 = 3 |  
 ----- AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0017): 0.59 0.059 3.08 27.50  
 + ID2= 2 (0019): 1.48 0.020 4.00 32.04  
 =====  
 ID = 3 (0020): 2.07 0.077 3.08 30.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB |  
 | NASHYD (0023) | Area (ha)= 1.40 Curve Number  
 (CN)= 67.1  
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
 Res. (N)= 3.00  
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.149 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 29.236  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD (0021) | Area (ha)= 1.28

| ID= 1 DT= 5.0 min | Total Imp(%)= 25.00 Dir. Conn.(%)= 25.00

-----  
 IMPERVIOUS PVIOUS (i)  
 Surface Area (ha)= 0.32 0.96  
 Dep. Storage (mm)= 1.00 5.80  
 Average Slope (%)= 1.00 6.60  
 Length (m)= 92.38 100.00  
 Mannings n = 0.013 0.250  
  
 Max.Eff.Inten.(mm/hr)= 127.00 44.89  
 over (min) 5.00 15.00  
 Storage Coeff. (min)= 2.21 (ii) 13.99 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 15.00  
 Unit Hyd. peak (cms)= 0.30 0.08

\*TOTALS\*  
 PEAK FLOW (cms)= 0.11 0.07  
 0.173 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.08  
 3.00 RUNOFF VOLUME (mm)= 80.47 25.11  
 38.94 TOTAL RAINFALL (mm)= 81.48 81.48  
 81.48 RUNOFF COEFFICIENT = 0.99 0.31  
 0.48

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
CN\* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0022) |  
 | IN= 2--> OUT= 1 |  
 | DT= 5.0 min |  
 STORAGE | OUTFLOW STORAGE | OUTFLOW  
 ----- (cms) (ha.m.) | (cms)  
 (ha.m.)  
 \*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.

0.0172 0.0001 0.0052 | 0.0843  
 0.0200 0.0056 0.0066 | 0.0945  
 0.0231 0.0202 0.0082 | 0.1036  
 0.0265 0.0402 0.0101 | 0.1121  
 0.0301 0.0595 0.0122 | 0.1199  
 0.0000 0.0728 0.0146 | 0.0000

AREA QPEAK TPEAK  
 R.V. (ha) (cms) (hrs)  
 (mm) INFLOW : ID= 2 (0021) 1.280 0.173 3.00  
 38.94 OUTFLOW: ID= 1 (0022) 1.280 0.085 3.17  
 34.86

PEAK FLOW REDUCTION [Qout/Qin](%)= 48.84  
 TIME SHIFT OF PEAK FLOW (min)= 10.00  
 0.0174 MAXIMUM STORAGE USED (ha.m.)=

-----  
 | ADD HYD (0024) |  
 | 1 + 2 = 3 |  
 ----- AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0022): 1.28 0.085 3.17 34.86  
 + ID2= 2 (0023): 1.40 0.149 3.08 29.24  
 =====  
 ID = 3 (0024): 2.68 0.232 3.08 31.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB |  
 | NASHYD (0055) | Area (ha)= 1.24 Curve Number  
 (CN)= 67.5

| ID= 1 DT= 5.0 min | Ia (mm)= 8.20 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.26  
 -----  
 Unit Hyd Qpeak (cms)= 0.182  
 PEAK FLOW (cms)= 0.096 (i)  
 TIME TO PEAK (hrs)= 3.167  
 RUNOFF VOLUME (mm)= 27.435  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.337

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | NASHYD (0056) | Area (ha)= 0.58 Curve Number  
 (CN)= 66.1  
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.26  
 -----  
 Unit Hyd Qpeak (cms)= 0.085  
 PEAK FLOW (cms)= 0.047 (i)  
 TIME TO PEAK (hrs)= 3.167  
 RUNOFF VOLUME (mm)= 28.510  
 TOTAL RAINFALL (mm)= 81.475  
 RUNOFF COEFFICIENT = 0.350

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

\*\*\*\*\*  
 \*\* SIMULATION NUMBER: 6 \*\*  
 \*\*\*\*\*

-----  
 | READ STORM | Filename: C:\Users\mwilson\AppData  
 | | Local\Temp\  
 | | ad98c7d6-b765-49b3-b3b5-  
 f4b8f2008ce1\3ec6332a

4.83	5.40	0.333	3.60	1.833	9.00	3.333	19.80
4.92	5.40	0.417	3.60	1.917	9.00	3.417	19.80
5.00	5.40	0.500	3.60	2.000	9.00	3.500	19.80
5.08	3.60	0.583	5.40	2.083	10.80	3.583	9.00
5.08	3.60	0.667	5.40	2.167	10.80	3.667	9.00
5.17	3.60	0.750	5.40	2.250	10.80	3.750	9.00
5.25	3.60	0.833	5.40	2.333	10.80	3.833	9.00
5.33	3.60	0.917	5.40	2.417	10.80	3.917	9.00
5.42	3.60	1.000	5.40	2.500	10.80	4.000	9.00
5.50	3.60	1.083	5.40	2.583	53.90	4.083	7.20
5.58	3.60	1.167	5.40	2.667	53.90	4.167	7.20
5.67	3.60	1.250	5.40	2.750	53.90	4.250	7.20
5.75	3.60	1.333	5.40	2.833	140.20	4.333	7.20
5.83	3.60	1.417	5.40	2.917	140.20	4.417	7.20
5.92	3.60	1.500	5.40	3.000	140.20	4.500	7.20
6.00	3.60						

Unit Hyd Qpeak (cms)= 0.247  
 PEAK FLOW (cms)= 0.129 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 28.444  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.316

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | NASHYD (0001) | Area (ha)= 2.02 Curve Number  
 (CN)= 61.5

| Ptotal= 89.93 mm | Comments: 100-Year, 6 hour SCS Type II -  
 Peterboro

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	3.60	1.75	9.00	3.25	19.80		
4.75	5.40	0.50	3.60	2.00	9.00	3.50	19.80
5.00	5.40	0.75	5.40	2.25	10.80	3.75	9.00
5.25	3.60	1.00	5.40	2.50	10.80	4.00	9.00
5.50	3.60	1.25	5.40	2.75	53.90	4.25	7.20
5.75	3.60	1.50	5.40	3.00	140.20	4.50	7.20
6.00	3.60						

-----  
 | CALIB |  
 | NASHYD (0002) | Area (ha)= 1.42 Curve Number  
 (CN)= 63.1  
 | ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.22

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME  
 STEP.

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.60	1.583	9.00	3.083	19.80		
4.58	5.40	0.167	3.60	1.667	9.00	3.167	19.80
4.67	5.40	0.250	3.60	1.750	9.00	3.250	19.80
4.75	5.40						

| ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17  
 -----  
 Unit Hyd Qpeak (cms)= 0.454  
 PEAK FLOW (cms)= 0.215 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 29.289  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.326

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | NASHYD (0015) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res. (N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598  
 PEAK FLOW (cms)= 0.313 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 32.364  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.360

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0016) |  
 | IN= 2---> OUT= 1 |  
 | DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW  
 STORAGE  
 (cms) (ha.m.) | (cms)  
 (ha.m.)  
 \*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0171 0.0001 0.0072 | 0.1306

	0.0065	0.0083	0.1492
0.0194			
	0.0242	0.0096	0.1656
0.0220			
	0.0501	0.0112	0.1806
0.0248			
	0.0806	0.0129	0.1944
0.0278			
	0.1098	0.0149	0.0000
0.0000			

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
INFLOW : ID= 2 (0015)	2.660	0.313	3.08
32.36			
OUTFLOW: ID= 1 (0016)	2.660	0.186	3.25
29.65			

PEAK FLOW REDUCTION [Qout/Qin](%)= 59.59  
 TIME SHIFT OF PEAK FLOW (min)= 10.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0261

-----

CALIB	Area	(ha)	Curve Number
NASHYD (0004)	2.44		
(CN)= 68.8			
ID= 1 DT= 5.0 min	8.00		# of Linear
Res.(N)= 3.00			
U.H. Tp(hrs)=	0.17		

-----

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.306 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 33.929  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.377

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Surface Area	(ha)=	0.34	1.14
Dep. Storage	(mm)=	1.00	5.30
Average Slope	(%)=	2.00	5.00
Length	(m)=	99.33	40.00
Mannings n	=	0.013	0.250
Max.Eff.Inten.(mm/hr)=	140.20	56.45	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.81 (ii)	8.54 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.32	0.12	

\*TOTALS\*

PEAK FLOW	(cms)=	0.13	0.13
0.261 (iii)			
TIME TO PEAK	(hrs)=	3.00	3.00
3.00			
RUNOFF VOLUME	(mm)=	88.92	28.75
42.59			
TOTAL RAINFALL	(mm)=	89.93	89.93
89.93			
RUNOFF COEFFICIENT	=	0.99	0.32
0.47			

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

ADD HYD	AREA	QPEAK	TPEAK	R.V.
(0009)	(ha)	(cms)	(hrs)	(mm)
1 + 2 = 3				
ID1= 1 (0007):	0.59	0.070	3.08	32.60
+ ID2= 2 (0008):	1.48	0.261	3.00	42.59
ID = 3 (0009):	2.07	0.330	3.00	39.74

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

CALIB	Area	(ha)	Curve Number
NASHYD (0003)	1.53		
(CN)= 61.7			
ID= 1 DT= 5.0 min	8.70		# of Linear
Res.(N)= 3.00			
U.H. Tp(hrs)=	0.17		

-----

Unit Hyd Qpeak (cms)= 0.344

PEAK FLOW (cms)= 0.154 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 27.518  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.306

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

CALIB	Area	(ha)	Curve Number
NASHYD (0007)	0.59		
(CN)= 65.0			
ID= 1 DT= 5.0 min	4.70		# of Linear
Res.(N)= 3.00			
U.H. Tp(hrs)=	0.17		

-----

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.070 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 32.601  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.363

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

CALIB	Area	(ha)	Total Imp(%)	Dir. Conn.(%)
STANDHYD (0008)	1.48		23.00	
ID= 1 DT= 5.0 min	23.00			23.00

-----

IMPERVIOUS PERVIOUS (i)

-----

CALIB	Area	(ha)	Curve Number
NASHYD (0011)	1.40		
(CN)= 67.1			
ID= 1 DT= 5.0 min	4.60		# of Linear
Res.(N)= 3.00			
U.H. Tp(hrs)=	0.17		

-----

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.176 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 34.567  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.384

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

CALIB	Area	(ha)	Total Imp(%)	Dir. Conn.(%)
STANDHYD (0010)	1.28		24.60	
ID= 1 DT= 5.0 min	24.60			24.60

-----

Surface Area	(ha)=	0.31	0.97
Dep. Storage	(mm)=	1.00	5.80
Average Slope	(%)=	1.00	6.60
Length	(m)=	92.38	100.00
Mannings n	=	0.013	0.250
Max.Eff.Inten.(mm/hr)=	140.20	53.60	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.13 (ii)	13.10 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.31	0.08	

\*TOTALS\*

PEAK FLOW	(cms)=	0.12	0.09
0.199 (iii)			
TIME TO PEAK	(hrs)=	3.00	3.08
3.00			



0.0376            0.0110    0.0137    |    0.0206  
 0.0435            0.0131    0.0166    |    0.0218  
 0.0000            0.0149    0.0200    |    0.0000

R.V.                    AREA        QPEAK        TPEAK  
                           (ha)        (cms)        (hrs)  
 (mm)                    INFLOW : ID= 2 (0018)    1.480    0.261    3.00  
 42.59                    OUTFLOW: ID= 1 (0019)    1.480    0.022    4.08  
 37.56

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.34  
 TIME SHIFT OF PEAK FLOW (min)= 65.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0433

-----  
 | ADD HYD (0020) |  
1 + 2 = 3
 ID1= 1 (0017):    0.59    0.070    3.08    32.60  
 + ID2= 2 (0019):    1.48    0.022    4.08    37.56  
 -----  
 ID = 3 (0020):    2.07    0.089    3.08    36.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB                    |  
 | NASHYD (0023) | Area (ha)= 1.40    Curve Number  
 (CN)= 67.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.60    # of Linear  
 Res.(N)= 3.00  
 -----  
                           U.H. Tp(hrs)= 0.17  
 Unit Hyd Qpeak (cms)= 0.315

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0022) |  
 | IN= 2---> OUT= 1 |  
 | DT= 5.0 min |  
 STORAGE  
 (ha.m.)  
 \*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0172            0.0001    0.0052    |    0.0843  
 0.0200            0.0056    0.0066    |    0.0945  
 0.0231            0.0202    0.0082    |    0.1036  
 0.0265            0.0402    0.0101    |    0.1121  
 0.0301            0.0595    0.0122    |    0.1199  
 0.0000            0.0728    0.0146    |    0.0000

R.V.                    AREA        QPEAK        TPEAK  
                           (ha)        (cms)        (hrs)  
 (mm)                    INFLOW : ID= 2 (0021)    1.280    0.200    3.00  
 44.66                    OUTFLOW: ID= 1 (0022)    1.280    0.094    3.25  
 40.58

PEAK FLOW REDUCTION [Qout/Qin](%)= 46.97  
 TIME SHIFT OF PEAK FLOW (min)= 15.00  
 MAXIMUM STORAGE USED (ha.m.)=

0.0200

-----  
 | ADD HYD (0024) |  
1 + 2 = 3
 ID1= 1 (0022):    1.28    0.094    3.25    40.58

PEAK FLOW (cms)= 0.176 (i)  
 TIME TO PEAK (hrs)= 3.083  
 RUNOFF VOLUME (mm)= 34.567  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.384

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB                    |  
 | STANDHYD (0021) | Area (ha)= 1.28  
 |ID= 1 DT= 5.0 min | Total Imp(%)= 25.00    Dir. Conn.(%)= 25.00  
 -----

IMPERVIOUS            PERVIOUS (i)  
 Surface Area (ha)= 0.32    0.96  
 Dep. Storage (mm)= 1.00    5.80  
 Average Slope (%)= 1.00    6.60  
 Length (m)= 92.38    100.00  
 Mannings n = 0.013    0.250

Max.Eff.Inten.(mm/hr)= 140.20    53.60  
                           over (min)    5.00    15.00  
 Storage Coeff. (min)= 2.13 (ii)    13.10 (ii)  
 Unit Hyd. Tpeak (min)= 5.00    15.00  
 Unit Hyd. peak (cms)= 0.31    0.08

\*TOTALS\*  
 PEAK FLOW (cms)= 0.12    0.09  
 0.200 (iii)  
 TIME TO PEAK (hrs)= 3.00    3.08  
 3.00  
 RUNOFF VOLUME (mm)= 88.92    29.92  
 44.66  
 TOTAL RAINFALL (mm)= 89.93    89.93  
 89.93  
 RUNOFF COEFFICIENT = 0.99    0.33  
 0.50

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 62.5    Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.

+ ID2= 2 (0023):    1.40    0.176    3.08    34.57  
 -----  
 ID = 3 (0024):    2.68    0.268    3.08    37.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB                    |  
 | NASHYD (0055) | Area (ha)= 1.24    Curve Number  
 (CN)= 67.5  
 |ID= 1 DT= 5.0 min | Ia (mm)= 8.20    # of Linear  
 Res.(N)= 3.00  
 -----  
                           U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.182

PEAK FLOW (cms)= 0.115 (i)  
 TIME TO PEAK (hrs)= 3.167  
 RUNOFF VOLUME (mm)= 32.714  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.364

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB                    |  
 | NASHYD (0056) | Area (ha)= 0.58    Curve Number  
 (CN)= 66.1  
 |ID= 1 DT= 5.0 min | Ia (mm)= 4.60    # of Linear  
 Res.(N)= 3.00  
 -----  
                           U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.085

PEAK FLOW (cms)= 0.055 (i)  
 TIME TO PEAK (hrs)= 3.167  
 RUNOFF VOLUME (mm)= 33.746  
 TOTAL RAINFALL (mm)= 89.925  
 RUNOFF COEFFICIENT = 0.375

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

\*\*\*\*\*  
 \*\* SIMULATION NUMBER: 7 \*\*  
 \*\*\*\*\*

CHICAGO STORM | IDF curve parameters: A= 405.000  
 Ptotal= 24.91 mm | B= 3.000  
 C= 0.760  
 used in: INTENSITY = A / (t + B)^C  
 Duration of storm = 4.00 hrs  
 Storm time step = 10.00 min  
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
3.17	2.07	0.17	1.76	1.17	11.75	2.17	3.88
3.33	1.93	0.33	2.00	1.33	57.66	2.33	3.35
3.50	1.81	0.50	2.32	1.50	15.20	2.50	2.96
3.67	1.71	0.67	2.81	1.67	8.31	2.67	2.66
3.83	1.62	0.83	3.61	1.83	5.91	2.83	2.42
4.00	1.54	1.00	5.28	2.00	4.66	3.00	2.23

CALIB |  
 NASHYD (0002) | Area (ha)= 1.42 Curve Number  
 (CN)= 63.1  
 ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear  
 Res. (N)= 3.00  
 U.H. Tp(hrs)= 0.22

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear  
 Res. (N)= 3.00  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.454  
 PEAK FLOW (cms)= 0.012 (i)  
 TIME TO PEAK (hrs)= 1.500  
 RUNOFF VOLUME (mm)= 2.144  
 TOTAL RAINFALL (mm)= 24.906  
 RUNOFF COEFFICIENT = 0.086

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB |  
 NASHYD (0015) | Area (ha)= 2.66 Curve Number  
 (CN)= 64.8  
 ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
 Res. (N)= 3.00  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598  
 PEAK FLOW (cms)= 0.019 (i)  
 TIME TO PEAK (hrs)= 1.500  
 RUNOFF VOLUME (mm)= 2.548  
 TOTAL RAINFALL (mm)= 24.906  
 RUNOFF COEFFICIENT = 0.102

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0016) |  
 IN= 2--> OUT= 1 |  
 DT= 5.0 min | OUTFLOW STORAGE OUTFLOW  
 STORAGE (cms) (ha.m.) (cms)  
 (ha.m.)  
 \*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0001 0.0072 | 0.1306

0.0171

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN		
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr		
0.083	1.76	1.083	11.75	2.083	3.88		
3.08	2.07	0.167	1.76	1.167	11.75	2.167	3.88
3.17	2.07	0.250	2.00	1.250	57.66	2.250	3.35
3.25	1.93	0.333	2.00	1.333	57.66	2.333	3.35
3.33	1.93	0.417	2.32	1.417	15.20	2.417	2.96
3.42	1.81	0.500	2.32	1.500	15.20	2.500	2.96
3.50	1.81	0.583	2.81	1.583	8.31	2.583	2.66
3.58	1.71	0.667	2.81	1.667	8.31	2.667	2.66
3.67	1.71	0.750	3.61	1.750	5.91	2.750	2.42
3.75	1.62	0.833	3.61	1.833	5.91	2.833	2.42
3.83	1.62	0.917	5.28	1.917	4.66	2.917	2.23
3.92	1.54	1.000	5.28	2.000	4.66	3.000	2.23
4.00	1.54						

Unit Hyd Qpeak (cms)= 0.247

PEAK FLOW (cms)= 0.004 (i)  
 TIME TO PEAK (hrs)= 1.667  
 RUNOFF VOLUME (mm)= 1.518  
 TOTAL RAINFALL (mm)= 24.906  
 RUNOFF COEFFICIENT = 0.061

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB |  
 NASHYD (0001) | Area (ha)= 2.02 Curve Number  
 (CN)= 61.5

0.0194	0.0065	0.0083	0.1492
0.0220	0.0242	0.0096	0.1656
0.0248	0.0501	0.0112	0.1806
0.0278	0.0806	0.0129	0.1944
0.0000	0.1098	0.0149	0.0000

R.V. AREA QPEAK TPEAK  
 (mm) (ha) (cms) (hrs)  
 INFLOW : ID= 2 (0015) 2.660 0.019 1.50  
 2.55 OUTFLOW: ID= 1 (0016) 2.660 0.000 4.58  
 0.03  
 PEAK FLOW REDUCTION [Qout/Qin](%)= 0.50  
 TIME SHIFT OF PEAK FLOW (min)=185.00  
 MAXIMUM STORAGE USED (ha.m.)=  
 0.0067

CALIB |  
 NASHYD (0004) | Area (ha)= 2.44 Curve Number  
 (CN)= 68.8  
 ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear  
 Res. (N)= 3.00  
 U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.012 (i)  
 TIME TO PEAK (hrs)= 1.583  
 RUNOFF VOLUME (mm)= 2.156  
 TOTAL RAINFALL (mm)= 24.906  
 RUNOFF COEFFICIENT = 0.087

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0003) | Area (ha)= 1.53 Curve Number
(CN)= 61.7
|ID= 1 DT= 5.0 min | Ia (mm)= 8.70 # of Linear
Res.(N)= 3.00
-----

```

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.344

```

PEAK FLOW (cms)= 0.005 (i)
TIME TO PEAK (hrs)= 1.583
RUNOFF VOLUME (mm)= 1.505
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.060

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0007) | Area (ha)= 0.59 Curve Number
(CN)= 65.0
|ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear
Res.(N)= 3.00
-----

```

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

```

PEAK FLOW (cms)= 0.004 (i)
TIME TO PEAK (hrs)= 1.500
RUNOFF VOLUME (mm)= 2.591
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.104

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD (0008) | Area (ha)= 1.48
|ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)=
23.00
-----

```

IMPERVIOUS PVIOUS (i)

```

-----
| CALIB |
| NASHYD (0011) | Area (ha)= 1.40 Curve Number
(CN)= 67.1
|ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
Res.(N)= 3.00
-----

```

U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

```

PEAK FLOW (cms)= 0.011 (i)
TIME TO PEAK (hrs)= 1.500
RUNOFF VOLUME (mm)= 2.836
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.114

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD (0010) | Area (ha)= 1.28
|ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.(%)=
24.60
-----

```

IMPERVIOUS PVIOUS (i)

```

Surface Area (ha)= 0.31 0.97
Dep. Storage (mm)= 1.00 5.80
Average Slope (%)= 1.00 6.60
Length (m)= 92.38 100.00
Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 57.66 1.57
over (min) 5.00 50.00
Storage Coeff. (min)= 3.04 (ii) 48.01 (ii)
Unit Hyd. Tpeak (min)= 5.00 50.00
Unit Hyd. peak (cms)= 0.27 0.02

```

```

*TOTALS*
PEAK FLOW (cms)= 0.05 0.00
0.049 (iii)
TIME TO PEAK (hrs)= 1.33 2.33
1.33

```

```

Surface Area (ha)= 0.34 1.14
Dep. Storage (mm)= 1.00 5.30
Average Slope (%)= 2.00 5.00
Length (m)= 99.33 40.00
Mannings n = 0.013 0.250

```

```

Max.Eff.Inten.(mm/hr)= 57.66 1.95
over (min) 5.00 30.00
Storage Coeff. (min)= 2.58 (ii) 28.49 (ii)
Unit Hyd. Tpeak (min)= 5.00 30.00
Unit Hyd. peak (cms)= 0.29 0.04

```

```

*TOTALS*
PEAK FLOW (cms)= 0.05 0.00
0.054 (iii)
TIME TO PEAK (hrs)= 1.33 1.92
1.33
RUNOFF VOLUME (mm)= 23.91 2.09
7.09
TOTAL RAINFALL (mm)= 24.91 24.91
24.91
RUNOFF COEFFICIENT = 0.96 0.08
0.28

```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

```

(i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
CN* = 60.7 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
| ADD HYD (0009) |
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
ID1= 1 (0007): 0.59 0.004 1.50 2.59
+ ID2= 2 (0008): 1.48 0.054 1.33 7.09
=====
ID = 3 (0009): 2.07 0.057 1.33 5.81

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

RUNOFF VOLUME (mm)= 23.91 2.13
7.46
TOTAL RAINFALL (mm)= 24.91 24.91
24.91
RUNOFF COEFFICIENT = 0.96 0.09
0.30

```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

```

(i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
CN* = 62.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
| ADD HYD (0012) |
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
ID1= 1 (0010): 1.28 0.049 1.33 7.46
+ ID2= 2 (0011): 1.40 0.011 1.50 2.84
=====
ID = 3 (0012): 2.68 0.056 1.33 5.05

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0005) | Area (ha)= 8.72 Curve Number
(CN)= 64.6
|ID= 1 DT= 5.0 min | Ia (mm)= 8.80 # of Linear
Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.39

```

Unit Hyd Qpeak (cms)= 0.854

```

PEAK FLOW (cms)= 0.021 (i)
TIME TO PEAK (hrs)= 1.917
RUNOFF VOLUME (mm)= 1.670
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.067

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
| CALIB |  
| NASHYD (0014) | Area (ha)= 8.50 Curve Number  
(CN)= 64.4  
|ID= 1 DT= 5.0 min | Ia (mm)= 8.40 # of Linear  
Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.832

PEAK FLOW (cms)= 0.022 (i)  
TIME TO PEAK (hrs)= 1.917  
RUNOFF VOLUME (mm)= 1.736  
TOTAL RAINFALL (mm)= 24.906  
RUNOFF COEFFICIENT = 0.070

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
| CALIB |  
| NASHYD (0006) | Area (ha)= 2.66 Curve Number  
(CN)= 64.8  
|ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear  
Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.019 (i)  
TIME TO PEAK (hrs)= 1.500  
RUNOFF VOLUME (mm)= 2.548  
TOTAL RAINFALL (mm)= 24.906  
RUNOFF COEFFICIENT = 0.102

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
| CALIB |

| NASHYD (0013) | Area (ha)= 0.75 Curve Number  
(CN)= 68.1  
|ID= 1 DT= 5.0 min | Ia (mm)= 7.40 # of Linear  
Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.169

PEAK FLOW (cms)= 0.004 (i)  
TIME TO PEAK (hrs)= 1.500  
RUNOFF VOLUME (mm)= 2.237  
TOTAL RAINFALL (mm)= 24.906  
RUNOFF COEFFICIENT = 0.090

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
| CALIB |  
| NASHYD (0017) | Area (ha)= 0.59 Curve Number  
(CN)= 65.0  
|ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  
Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.004 (i)  
TIME TO PEAK (hrs)= 1.500  
RUNOFF VOLUME (mm)= 2.591  
TOTAL RAINFALL (mm)= 24.906  
RUNOFF COEFFICIENT = 0.104

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
| CALIB |  
| STANDHYD (0018) | Area (ha)= 1.48  
|ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00  
-----

Surface Area (ha)= IMPERVIOUS 0.34 PERVIOUS (i) 1.14  
Dep. Storage (mm)= 1.00 5.30

Average Slope (%)= 2.00 5.00  
Length (m)= 99.33 40.00  
Mannings n = 0.013 0.250  
  
Max.Eff.Inten.(mm/hr)= 57.66 1.95  
over (min) 5.00 30.00  
Storage Coeff. (min)= 2.58 (ii) 28.49 (ii)  
Unit Hyd. Tpeak (min)= 5.00 30.00  
Unit Hyd. peak (cms)= 0.29 0.04

\*TOTALS\*

PEAK FLOW (cms)= 0.05 0.00  
0.054 (iii)  
TIME TO PEAK (hrs)= 1.33 1.92  
1.33  
RUNOFF VOLUME (mm)= 23.91 2.09  
7.09  
TOTAL RAINFALL (mm)= 24.91 24.91  
24.91  
RUNOFF COEFFICIENT = 0.96 0.08  
0.28

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
| RESERVOIR (0019) |  
| IN= 2---> OUT= 1 |  
| DT= 5.0 min |  
STORAGE  
-----  
(ha.m.)

\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
0.0238 0.0001 0.0074 | 0.0165  
0.0280 0.0045 0.0089 | 0.0180  
0.0326 0.0084 0.0111 | 0.0193

0.0376 0.0110 0.0137 | 0.0206  
0.0435 0.0131 0.0166 | 0.0218  
0.0000 0.0149 0.0200 | 0.0000  
  
R.V. AREA QPEAK TPEAK  
(mm) (ha) (cms) (hrs)  
7.09 INFLOW : ID= 2 (0018) 1.480 0.054 1.33  
2.06 OUTFLOW: ID= 1 (0019) 1.480 0.003 3.50

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.96  
TIME SHIFT OF PEAK FLOW (min)=130.00  
0.0085 MAXIMUM STORAGE USED (ha.m.)=

-----  
| ADD HYD (0020) |  
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
+ ID1= 1 (0017): 0.59 0.004 1.50 2.59  
+ ID2= 2 (0019): 1.48 0.003 3.50 2.06  
=====

ID = 3 (0020): 2.07 0.004 1.50 2.21  
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
| CALIB |  
| NASHYD (0023) | Area (ha)= 1.40 Curve Number  
(CN)= 67.1  
|ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.011 (i)  
 TIME TO PEAK (hrs)= 1.500  
 RUNOFF VOLUME (mm)= 2.836  
 TOTAL RAINFALL (mm)= 24.906  
 RUNOFF COEFFICIENT = 0.114

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD (0021) | Area (ha)= 1.28  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 25.00 Dir. Conn.(%)= 25.00  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.32	0.96
Dep. Storage (mm)=	1.00	5.80
Average Slope (%)=	1.00	6.60
Length (m)=	92.38	100.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	57.66	1.57
over (min)	5.00	50.00
Storage Coeff. (min)=	3.04 (ii)	48.01 (ii)
Unit Hyd. Tpeak (min)=	5.00	50.00
Unit Hyd. peak (cms)=	0.27	0.02

\*TOTALS\*  
 PEAK FLOW (cms)= 0.05 0.00  
 0.050 (iii)  
 TIME TO PEAK (hrs)= 1.33 2.33  
 1.33  
 RUNOFF VOLUME (mm)= 23.91 2.13  
 7.55  
 TOTAL RAINFALL (mm)= 24.91 24.91  
 24.91  
 RUNOFF COEFFICIENT = 0.96 0.09  
 0.30

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 62.5 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.

+ ID2= 2 (0023):	1.40	0.011	1.50	2.84
=====				
ID = 3 (0024):	2.68	0.011	1.50	3.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 | CALIB |  
 | NASHYD (0055) | Area (ha)= 1.24 Curve Number  
 (CN)= 67.5  
 | ID= 1 DT= 5.0 min | Ia (mm)= 8.20 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.182  
 PEAK FLOW (cms)= 0.005 (i)  
 TIME TO PEAK (hrs)= 1.667  
 RUNOFF VOLUME (mm)= 2.006  
 TOTAL RAINFALL (mm)= 24.906  
 RUNOFF COEFFICIENT = 0.081

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | NASHYD (0056) | Area (ha)= 0.58 Curve Number  
 (CN)= 66.1  
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  
 Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.085  
 PEAK FLOW (cms)= 0.003 (i)  
 TIME TO PEAK (hrs)= 1.667  
 RUNOFF VOLUME (mm)= 2.735  
 TOTAL RAINFALL (mm)= 24.906  
 RUNOFF COEFFICIENT = 0.110

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR (0022) |  
 | IN= 2---> OUT= 1 |  
 | DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW  
 STORAGE  
 (ha.m.) (cms) (ha.m.) | (cms)

\*\*\*\*\* WARNING : FIRST OUTFLOW IS NOT ZERO.  
 0.0172 0.0001 0.0052 | 0.0843  
 0.0200 0.0056 0.0066 | 0.0945  
 0.0231 0.0202 0.0082 | 0.1036  
 0.0265 0.0402 0.0101 | 0.1121  
 0.0301 0.0595 0.0122 | 0.1199  
 0.0000 0.0728 0.0146 | 0.0000

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
7.55 INFLOW : ID= 2 (0021)	1.280	0.050	1.33
3.46 OUTFLOW: ID= 1 (0022)	1.280	0.004	2.75

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.63  
 TIME SHIFT OF PEAK FLOW (min)= 85.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0063

-----  
 | ADD HYD (0024) |  
1 + 2 = 3
 ID1= 1 (0022): 1.28 0.004 2.75 3.46

FINISH

# Appendix C

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Stormwater Facility Design



### 3.3.2 Water Quality Sizing Criteria

The volumetric water quality criteria are presented in Table 3.2. The values are based on a 24 hour drawdown time and a design which conforms to the guidance provided in this manual. Requirements differ with SWMP type to reflect differences in removal efficiencies. Of the specified storage volume for wet facilities, 40 m<sup>3</sup>/ha is extended detention, while the remainder represents the permanent pool.

**Table 3.2 Water Quality Storage Requirements based on Receiving Waters<sup>1, 2</sup>**

Protection Level	SWMP Type	Storage Volume (m <sup>3</sup> /ha) for Impervious Level			
		35%	55%	70%	85%
<i>Enhanced</i> 80% long-term S.S. removal	Infiltration	25	30	35	40
	Wetlands	80	105	120	140
	Hybrid Wet Pond/Wetland	110	150	175	195
	Wet Pond	140	190	225	250
<i>Normal</i> 70% long-term S.S. removal	Infiltration	20	20	25	30
	Wetlands	60	70	80	90
	Hybrid Wet Pond/Wetland	75	90	105	120
	Wet Pond	90	110	130	150
<i>Basic</i> 60% long-term S.S. removal	Infiltration	20	20	20	20
	Wetlands	60	60	60	60
	Hybrid Wet Pond/Wetland	60	70	75	80
	Wet Pond	60	75	85	95
	Dry Pond (Continuous Flow)	90	150	200	240

<sup>1</sup>Table 3.2 does not include every available SWMP type. Any SWMP type that can be demonstrated to the approval agencies to meet the required long-term suspended solids removal for the selected protection levels under the conditions of the site is acceptable for water quality objectives. The sizing for these SWMP types is to be determined based on performance results that have been peer-reviewed. The designer and those who review the design should be fully aware of the assumptions and sampling methodologies used in formulating performance predictions and their implications for the design.

<sup>2</sup>Hybrid Wet Pond/Wetland systems have 50-60% of their permanent pool volume in deeper portions of the facility (e.g., forebay, wet pond).

**Stage-Storage-Discharge: PR-100 Roadside Ditch**



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** MW / CPB  
**Date:** February 23, 2022

Storage Summary		
Top of Dead Storage:	1.00	m
Dead Storage Volume:	71.6	m <sup>3</sup>
Active Storage Volume:	206.5	m <sup>3</sup>

Outlet Capacity Summary				
Type	Diameter	Slope	Peak Flow	% Full

Discharge Summary			
Stage	Type	Invert Elev (m)	Diameter / Width (mm) (m)
1	Orifice Tube: Vertical	1.00	325

**Stage-Storage-Discharge Summary Table**

Elevation	Stage	Stage 1 Orifice Tube					Total Storage	Total Discharge	Notes
m	m		m <sup>3</sup> /s				ha*m	m <sup>3</sup> /s	
1.00	0.00	0.000					0.0072	0.000	
1.01	0.01	0.000					0.0073	0.000	
1.02	0.02	0.001					0.0075	0.001	
1.03	0.03	0.002					0.0077	0.002	
1.04	0.04	0.003					0.0079	0.003	
1.05	0.05	0.005					0.0081	0.005	
1.06	0.06	0.006					0.0083	0.006	
1.07	0.07	0.009					0.0085	0.009	
1.08	0.08	0.011					0.0087	0.011	
1.09	0.09	0.014					0.0089	0.014	
1.10	0.10	0.017					0.0091	0.017	
1.11	0.11	0.021					0.0094	0.021	<= 2 Yr: 93 m <sup>3</sup> (1.11m)
1.12	0.12	0.024					0.0096	0.024	
1.13	0.13	0.028					0.0099	0.028	
1.14	0.14	0.032					0.0101	0.032	
1.15	0.15	0.036					0.0104	0.036	
1.16	0.16	0.041					0.0106	0.041	
1.17	0.17	0.045					0.0109	0.045	
1.18	0.18	0.050					0.0112	0.050	
1.19	0.19	0.055					0.0115	0.055	
1.20	0.20	0.060					0.0117	0.060	
1.21	0.21	0.065					0.0120	0.065	
1.22	0.22	0.070					0.0123	0.070	<= 5 Yr: 123 m <sup>3</sup> (1.22m)
1.23	0.23	0.075					0.0126	0.075	
1.24	0.24	0.081					0.0129	0.081	
1.25	0.25	0.086					0.0133	0.086	
1.26	0.26	0.091					0.0136	0.091	
1.27	0.27	0.096					0.0139	0.096	
1.28	0.28	0.101					0.0142	0.101	
1.29	0.29	0.105					0.0146	0.105	
1.30	0.30	0.110					0.0149	0.110	<= 10 Yr: 146 m <sup>3</sup> (1.3m)
1.31	0.31	0.114					0.0153	0.114	
1.32	0.32	0.117					0.0156	0.117	
1.33	0.33	0.120					0.0160	0.120	
1.34	0.34	0.124					0.0163	0.124	
1.35	0.35	0.127					0.0167	0.127	
1.36	0.36	0.131					0.0171	0.131	
1.37	0.37	0.134					0.0175	0.134	
1.38	0.38	0.137					0.0178	0.137	
1.39	0.39	0.140					0.0182	0.140	
1.40	0.40	0.143					0.0186	0.143	<= 25 Yr: 185 m <sup>3</sup> (1.4m)
1.41	0.41	0.146					0.0190	0.146	
1.42	0.42	0.149					0.0194	0.149	
1.43	0.43	0.152					0.0199	0.152	
1.44	0.44	0.155					0.0203	0.155	
1.45	0.45	0.158					0.0207	0.158	
1.46	0.46	0.160					0.0211	0.160	
1.47	0.47	0.163					0.0216	0.163	
1.48	0.48	0.166					0.0220	0.166	<= 50 Yr: 220 m <sup>3</sup> (1.48m)

**Stage-Storage-Discharge Summary Table**

<b>Elevation</b>	<b>Stage</b>	<b>Stage 1 Orifice Tube</b>					<b>Total Storage</b>	<b>Total Discharge</b>	<b>Notes</b>
<b>m</b>	<b>m</b>		<b>m<sup>3</sup>/s</b>				<b>ha*m</b>	<b>m<sup>3</sup>/s</b>	
1.49	0.49	<b>0.168</b>					<b>0.0225</b>	<b>0.168</b>	<= 100 Yr: 261 m <sup>3</sup> (1.57m)
1.50	0.50	<b>0.171</b>					<b>0.0229</b>	<b>0.171</b>	
1.51	0.51	<b>0.173</b>					<b>0.0234</b>	<b>0.173</b>	
1.52	0.52	<b>0.176</b>					<b>0.0239</b>	<b>0.176</b>	
1.53	0.53	<b>0.178</b>					<b>0.0243</b>	<b>0.178</b>	
1.54	0.54	<b>0.181</b>					<b>0.0248</b>	<b>0.181</b>	
1.55	0.55	<b>0.183</b>					<b>0.0253</b>	<b>0.183</b>	
1.56	0.56	<b>0.185</b>					<b>0.0258</b>	<b>0.185</b>	
1.57	0.57	<b>0.188</b>					<b>0.0263</b>	<b>0.188</b>	
1.58	0.58	<b>0.190</b>					<b>0.0268</b>	<b>0.190</b>	
1.59	0.59	<b>0.192</b>					<b>0.0273</b>	<b>0.192</b>	
1.60	0.60	<b>0.194</b>					<b>0.0278</b>	<b>0.194</b>	

**Stage-Storage-Discharge: PR-102 Roadside Ditch**



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** MW / CPB  
**Date:** February 23, 2022

Storage Summary		
Top of Dead Storage:	1.00	m
Dead Storage Volume:	78.3	m <sup>3</sup>
Active Storage Volume:	356.7	m <sup>3</sup>

Outlet Capacity Summary				
Type	Diameter	Slope	Peak Flow	% Full

Discharge Summary			
Stage	Type	Invert Elev (m)	Diameter / Width (mm) (m)
1	Orifice Tube: Vertical	1.00	95

**Stage-Storage-Discharge Summary Table**

Elevation	Stage	Stage 1 Orifice Tube					Total Storage	Total Discharge	Notes
m	m		m <sup>3</sup> /s				ha*m	m <sup>3</sup> /s	
1.00	0.00	0.000					0.0074	0.000	
1.01	0.01	0.000					0.0073	0.000	
1.02	0.02	0.000					0.0075	0.000	
1.03	0.03	0.001					0.0077	0.001	
1.04	0.04	0.001					0.0080	0.001	
1.05	0.05	0.002					0.0082	0.002	
1.06	0.06	0.003					0.0084	0.003	
1.07	0.07	0.004					0.0086	0.004	<= 25 mm: 85 m <sup>3</sup> (1.07m)
1.08	0.08	0.005					0.0089	0.005	
1.09	0.09	0.005					0.0091	0.005	
1.10	0.10	0.006					0.0094	0.006	
1.11	0.11	0.006					0.0097	0.006	
1.12	0.12	0.007					0.0099	0.007	
1.13	0.13	0.007					0.0102	0.007	
1.14	0.14	0.008					0.0105	0.008	
1.15	0.15	0.008					0.0108	0.008	
1.16	0.16	0.008					0.0111	0.008	
1.17	0.17	0.009					0.0114	0.009	
1.18	0.18	0.009					0.0117	0.009	
1.19	0.19	0.009					0.0120	0.009	
1.20	0.20	0.010					0.0123	0.010	
1.21	0.21	0.010					0.0126	0.010	
1.22	0.22	0.010					0.0130	0.010	
1.23	0.23	0.011					0.0133	0.011	
1.24	0.24	0.011					0.0137	0.011	
1.25	0.25	0.011					0.0140	0.011	
1.26	0.26	0.012					0.0144	0.012	
1.27	0.27	0.012					0.0147	0.012	
1.28	0.28	0.012					0.0151	0.012	
1.29	0.29	0.012					0.0155	0.012	
1.30	0.30	0.013					0.0158	0.013	
1.31	0.31	0.013					0.0162	0.013	
1.32	0.32	0.013					0.0166	0.013	
1.33	0.33	0.013					0.0170	0.013	
1.34	0.34	0.014					0.0174	0.014	
1.35	0.35	0.014					0.0178	0.014	
1.36	0.36	0.014					0.0183	0.014	
1.37	0.37	0.014					0.0187	0.014	
1.38	0.38	0.014					0.0191	0.014	
1.39	0.39	0.015					0.0196	0.015	
1.40	0.40	0.015					0.0200	0.015	
1.41	0.41	0.015					0.0204	0.015	
1.42	0.42	0.015					0.0209	0.015	
1.43	0.43	0.016					0.0214	0.016	
1.44	0.44	0.016					0.0218	0.016	
1.45	0.45	0.016					0.0223	0.016	
1.46	0.46	0.016					0.0228	0.016	
1.47	0.47	0.016					0.0233	0.016	
1.48	0.48	0.017					0.0238	0.017	

<= 25 mm: 85 m<sup>3</sup> (1.07m)

<= 2 Yr: 125 m<sup>3</sup> (1.21m)

<= 5 Yr: 190 m<sup>3</sup> (1.38m)

**Stage-Storage-Discharge Summary Table**

Elevation	Stage	Stage 1 Orifice Tube						Total Storage	Total Discharge	Notes
m	m		m <sup>3</sup> /s					ha*m	m <sup>3</sup> /s	
1.49	0.49	0.017						0.0243	0.017	<= 10 Yr: 241 m <sup>3</sup> (1.49m)
1.50	0.50	0.017						0.0248	0.017	
1.51	0.51	0.017						0.0253	0.017	
1.52	0.52	0.017						0.0258	0.017	
1.53	0.53	0.017						0.0263	0.017	
1.54	0.54	0.018						0.0269	0.018	
1.55	0.55	0.018						0.0274	0.018	
1.56	0.56	0.018						0.0280	0.018	
1.57	0.57	0.018						0.0285	0.018	
1.58	0.58	0.018						0.0291	0.018	
1.59	0.59	0.019						0.0296	0.019	
1.60	0.60	0.019						0.0302	0.019	
1.61	0.61	0.019						0.0308	0.019	
1.62	0.62	0.019						0.0314	0.019	
1.63	0.63	0.019						0.0320	0.019	
1.64	0.64	0.019						0.0326	0.019	
1.65	0.65	0.019						0.0332	0.019	
1.66	0.66	0.020						0.0338	0.020	
1.67	0.67	0.020						0.0344	0.020	
1.68	0.68	0.020						0.0350	0.020	
1.69	0.69	0.020						0.0356	0.020	
1.70	0.70	0.020						0.0363	0.020	
1.71	0.71	0.020						0.0369	0.020	
1.72	0.72	0.021						0.0376	0.021	
1.73	0.73	0.021						0.0382	0.021	
1.74	0.74	0.021						0.0389	0.021	
1.75	0.75	0.021						0.0396	0.021	
1.76	0.76	0.021						0.0402	0.021	
1.77	0.77	0.021						0.0409	0.021	
1.78	0.78	0.021						0.0416	0.021	
1.79	0.79	0.022						0.0425	0.022	
1.80	0.80	0.022						0.0435	0.022	

**Stage-Storage-Discharge: PR-201 Roadside Ditch**



**Project No:** 19-10874  
**Project Name:** Life at the Woodland  
**Designed/Checked By:** MW / CPB  
**Date:** February 23, 2022

Storage Summary		
Top of Dead Storage:	1.00	m
Dead Storage Volume:	51.9	m <sup>3</sup>
Active Storage Volume:	248.7	m <sup>3</sup>

Outlet Capacity Summary				
Type	Diameter	Slope	Peak Flow	% Full

Discharge Summary			
Stage	Type	Invert Elev (m)	Diameter / Width (mm) (m)
1	Orifice Tube: Vertical	1.00	250

**Stage-Storage-Discharge Summary Table**

Elevation	Stage	Stage 1 Orifice Tube					Total Storage	Total Discharge	Notes
m	m		m <sup>3</sup> /s				ha*m	m <sup>3</sup> /s	
1.00	0.00	0.000					0.0052	0.000	
1.01	0.01	0.000					0.0054	0.000	
1.02	0.02	0.001					0.0056	0.001	
1.03	0.03	0.001					0.0058	0.001	
1.04	0.04	0.003					0.0061	0.003	
1.05	0.05	0.004					0.0063	0.004	<= 25 mm: 63 m <sup>3</sup> (1.05m)
1.06	0.06	0.006					0.0066	0.006	
1.07	0.07	0.007					0.0068	0.007	
1.08	0.08	0.010					0.0071	0.010	
1.09	0.09	0.012					0.0074	0.012	
1.10	0.10	0.015					0.0076	0.015	
1.11	0.11	0.017					0.0079	0.017	
1.12	0.12	0.020					0.0082	0.020	<= 2 Yr: 81 m <sup>3</sup> (1.12m)
1.13	0.13	0.023					0.0085	0.023	
1.14	0.14	0.027					0.0088	0.027	
1.15	0.15	0.030					0.0091	0.030	
1.16	0.16	0.033					0.0094	0.033	
1.17	0.17	0.037					0.0097	0.037	
1.18	0.18	0.040					0.0101	0.040	
1.19	0.19	0.044					0.0104	0.044	
1.20	0.20	0.047					0.0108	0.047	<= 5 Yr: 105 m <sup>3</sup> (1.2m)
1.21	0.21	0.051					0.0111	0.051	
1.22	0.22	0.054					0.0115	0.054	
1.23	0.23	0.057					0.0118	0.057	
1.24	0.24	0.059					0.0122	0.059	
1.25	0.25	0.061					0.0126	0.061	<= 10 Yr: 122 m <sup>3</sup> (1.25m)
1.26	0.26	0.064					0.0130	0.064	
1.27	0.27	0.066					0.0133	0.066	
1.28	0.28	0.068					0.0137	0.068	
1.29	0.29	0.071					0.0141	0.071	
1.30	0.30	0.073					0.0146	0.073	<= 25 Yr: 144 m <sup>3</sup> (1.3m)
1.31	0.31	0.075					0.0150	0.075	
1.32	0.32	0.077					0.0154	0.077	
1.33	0.33	0.079					0.0158	0.079	
1.34	0.34	0.081					0.0163	0.081	
1.35	0.35	0.083					0.0167	0.083	
1.36	0.36	0.084					0.0172	0.084	
1.37	0.37	0.086					0.0176	0.086	<= 50 Yr: 174 m <sup>3</sup> (1.37m)
1.38	0.38	0.088					0.0181	0.088	
1.39	0.39	0.090					0.0186	0.090	
1.40	0.40	0.091					0.0190	0.091	
1.41	0.41	0.093					0.0195	0.093	
1.42	0.42	0.094					0.0200	0.094	<= 100 Yr: 200 m <sup>3</sup> (1.42m)
1.43	0.43	0.096					0.0205	0.096	
1.44	0.44	0.098					0.0210	0.098	
1.45	0.45	0.099					0.0215	0.099	
1.46	0.46	0.101					0.0221	0.101	
1.47	0.47	0.102					0.0226	0.102	
1.48	0.48	0.104					0.0231	0.104	

**Stage-Storage-Discharge Summary Table**

<b>Elevation</b>	<b>Stage</b>	<b>Stage 1 Orifice Tube</b>						<b>Total Storage</b>	<b>Total Discharge</b>	<b>Notes</b>
<b>m</b>	<b>m</b>		<b>m<sup>3</sup>/s</b>					<b>ha*m</b>	<b>m<sup>3</sup>/s</b>	
1.49	0.49	<b>0.105</b>						<b>0.0237</b>	<b>0.105</b>	
1.50	0.50	<b>0.107</b>						<b>0.0242</b>	<b>0.107</b>	
1.51	0.51	<b>0.108</b>						<b>0.0248</b>	<b>0.108</b>	
1.52	0.52	<b>0.109</b>						<b>0.0253</b>	<b>0.109</b>	
1.53	0.53	<b>0.111</b>						<b>0.0259</b>	<b>0.111</b>	
1.54	0.54	<b>0.112</b>						<b>0.0265</b>	<b>0.112</b>	
1.55	0.55	<b>0.113</b>						<b>0.0270</b>	<b>0.113</b>	
1.56	0.56	<b>0.115</b>						<b>0.0276</b>	<b>0.115</b>	
1.57	0.57	<b>0.116</b>						<b>0.0282</b>	<b>0.116</b>	
1.58	0.58	<b>0.117</b>						<b>0.0288</b>	<b>0.117</b>	
1.59	0.59	<b>0.119</b>						<b>0.0294</b>	<b>0.119</b>	
1.60	0.60	<b>0.120</b>						<b>0.0301</b>	<b>0.120</b>	

# Appendix D

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Drawings

