



Preliminary
Stormwater Management Report

Life at the Woodland
Township of Otonabee-South
Monaghan
County of Peterborough

Residential Subdivision Development

D.M. Wills Project No. 19-10874



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Bancroft

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Prepared for:
Life at the Woodland Inc.

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1.0 Purpose

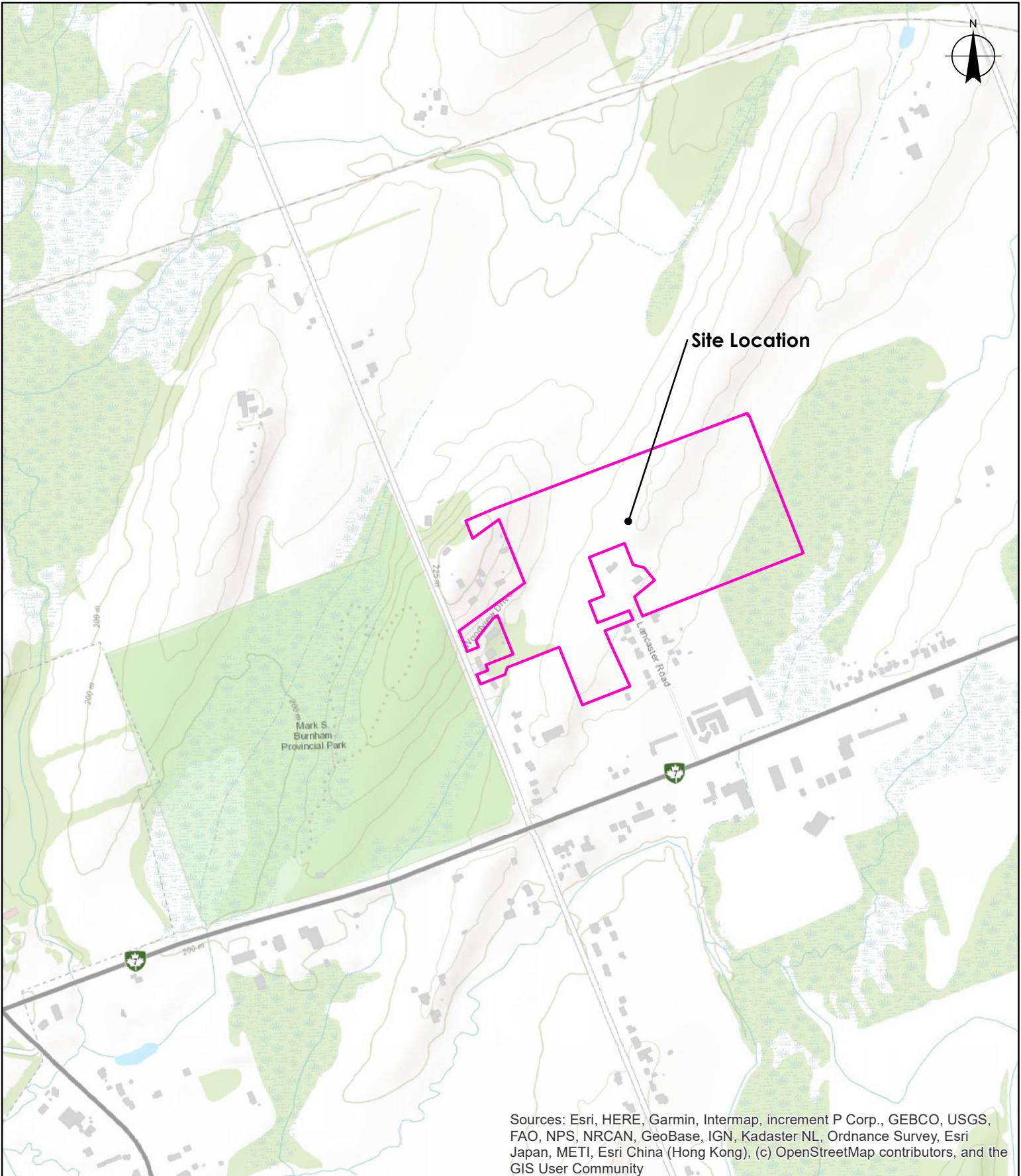
D.M. Wills Associates Limited (Wills) has been retained by Mr. Rubal Kundra of Life at the Woodland Inc. to prepare a Preliminary Stormwater Management Plan and Report for the proposed residential subdivision located on Part of Lot 27, Concession 10, Township of Otonabee-South Monaghan in the County of Peterborough.

The purpose of this report is to evaluate the impact of the proposed development on the stormwater runoff and to develop a preliminary plan for stormwater management that will permit the development to proceed with no adverse impacts to the receiving drainage systems. This report has been prepared specifically for the County of Peterborough (County) and the Otonabee Region Conservation Authority (ORCA) to address stormwater management for the development and to satisfy the statutory requirements.

2.0 Site Description

The subject property is located in the township of Otonabee-South Monaghan with access provided from Burnham Line, situated approximately 6 kilometres east of Peterborough. The subject site is legally described as a Part of Lot 27, Concession 10 in the Township of Otonabee-South Monaghan in the County of Peterborough and is approximately 17.67 ha in area. The property is bounded by agricultural land use to the north, Burnham Line and wooded area to the west, wetland and wooded area to the east and residential lots accessed by Lancaster Road to the south. An unevaluated wetland feature is located in the western portion of the property, which drains to two separate outlets. The location of the site is shown on **Figure 1**.

The proposed residential subdivision consists of twenty-seven (27) lots adjacent to the wetland buffer. The portion of the site within the wetland buffer is to remain in an undisturbed natural state. The development of the site will require the removal of vegetated areas and grasslands. A cul-de-sac roadway off Burnham Line will provide access for the proposed lots.



Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community

Figure 01
Location Plan



NAD83 UTM Zone 18

0 75 150 300 450 600
Meters

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Legend
— Property Limits

Drawn by: RC	Scale (Horz.) 1:10,000
Checked by: CPB	
Engineer: RC/CPB	Map Date Dec 2021
Project No. 10874	Map File No. 10874-DP01

According to the Soil Survey Complex of Ontario, the subject site is primarily composed of two types of surficial soils. The wetland portion of the site is composed of Foxboro Silt Loam with the remainder of the site composed of Otonabee Loam. According to the SCS method of classifying soils, these types of surficial soils correspond to Hydrologic Soils Groups C and B respectively.

A topographic survey of the subject property was completed by JBF Surveyors Ltd. (Project #7369) with the latest drawing version dated January 13, 2020, to determine existing elevations and the location of drainage features on the site. This information was used to determine drainage patterns and preliminary catchment area characteristics. A digital elevation model of the wetland was obtained from the South Central Ontario Orthophotography (SCOOP) under Land Information Ontario (LIO) database. The horizontal datum for the SCOOP is projected in UTM Zone 17 of the NAD83 Canadian Spatial Reference System and the vertical datum is sourced CGVD28. The SCOOP DEM raster has a resolution of 20 cm, however it was resampled into a raster cell of size 2 m. This data was produced to meet ASPRS Positional Accuracy Standards for Digital Geospatial Data (2014) with +/- 46.0cm actual VVA accuracy at the 95th percentile.

3.0 Methodology

The present hierarchy of watershed planning in Ontario can be described by the following in descending order: Watershed Plans, Sub-watershed Plans and individual Stormwater Management Plans. There is no Master Plan directing the stormwater management strategy for this watershed. As such, the proposed development was prepared as an individual Preliminary Stormwater Management Plan.

3.1 Site Specific Stormwater Design Criteria

A pre-consultation meeting was held to discuss the requirements of the Draft Plan Approval process. The following design criteria have been established from the pre-consultation meeting and with follow-up correspondence from the County and ORCA.

- To provide stormwater quality controls, to achieve "Enhanced" Level 1 protection as defined in the Stormwater Management Planning and Design Manual (March 2003).
- To provide stormwater quantity controls, to reduce the post development peak flow rates to the existing condition peak flow rates at each outlet location, for the 2 to 100-year design storms.
- To respect the recommended statutory setback requirements provided by the regulatory agency for the unevaluated wetland located within the property.
- To incorporate Low Impact Development (LID) features as part of the proposed stormwater management strategy.

3.2 Catchment Area Characterization

For the purpose of the preliminary SWM plan, the site will be analyzed as six (6) catchment areas based on the site topography under existing conditions. The existing catchment areas are shown on **Figure 2**. The internal wetland area will remain undisturbed and has not been included in the analysis.

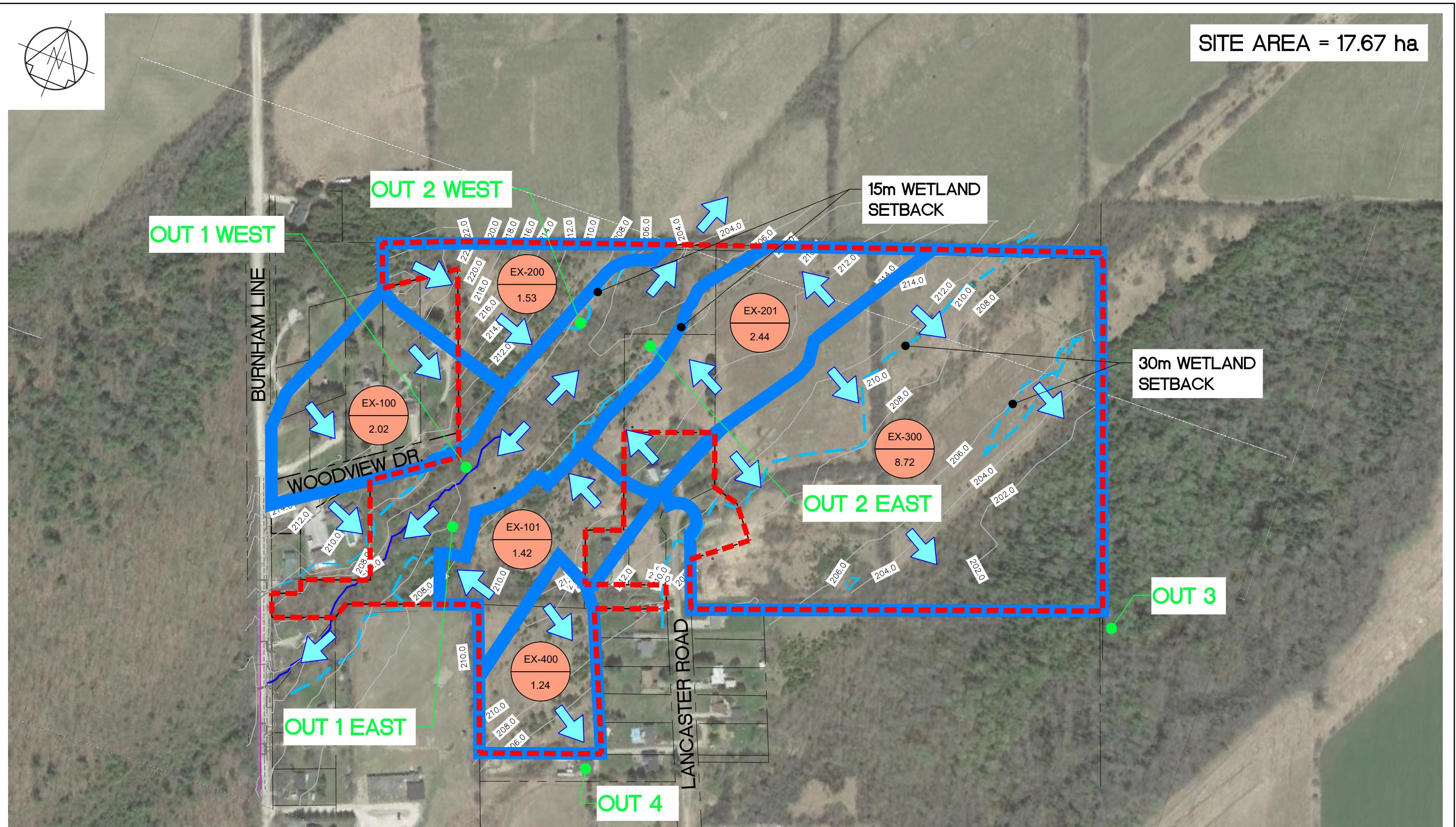
- Catchment area **EX-100** consists of 2.02 ha of land and includes the northwestern portion of the subject site and neighboring lots. This catchment consists of the current gravel access to the site from Burnham Line, wooded areas and rural residential lots. Runoff from this catchment currently flows overland to the wetland, discharging to **OUT-1 WEST**.
- Catchment area **EX-101** consists of 1.42 ha of land and includes the southwest portion of the site. This catchment is comprised of woodlots and grassed areas. Runoff from this catchment will flow overland northerly to the wetland, discharging to **OUT-1 EAST**.
- Catchment area **EX-200** consists of 1.53 ha of land and includes the northern portion of the site. This catchment is comprised of wooded areas and neighboring residential rear yards. Runoff from this catchment will flow overland towards the wetland, discharging to **OUT-2 WEST**.
- Catchment area **EX-201** consists of 2.44 ha of land and includes the north central portion of the site. This catchment consists of wood lots and grassed areas. Runoff from this catchment will drain northerly towards the wetland, discharging to **OUT-2 EAST**.
- Catchment **EX-300** consists of 8.72 ha of land located in the eastern portion of the site. This catchment is comprised of extensive grassed range type areas with a band of wooded areas and wetland area. The runoff generated within this catchment drains southeasterly to an unidentified wetland located southeast of the site (**OUT-3**).
- Catchment **EX-400** consists of 1.24 ha of land located in the south central portion of the subject property west of Lancaster Road. This catchment is comprised of grassed range with some wood pockets. The runoff generated within this catchment drains southerly overland towards the private properties on Lancaster Road (**OUT-4**).

Under the proposed condition, the catchment areas subject to land use change were delineated into eight (8) sub-catchment areas as shown on **Figure 3**.

- Catchment area **PR-100** consists of 2.66 ha of land and includes the northwest neighboring lots and proposed access road from Burnham Line. Runoff from this catchment will flow overland towards a proposed SWM facility for treatment and will then outlet to the wetland, discharging to **OUT-1 WEST**.
- Catchment area **PR-101** consists of 0.59 ha of land comprised of the rear lot yards located west of the proposed cul-de-sac. Runoff from this catchment will

drain uncontrolled towards the wetland as in the existing condition, discharging to **OUT-1 EAST**.

- Catchment area **PR-102** consists of 1.48 ha of land and includes the southern portion of the developed site comprised of the proposed roadway and cul-de-sac, and a portion of the proposed residential lots. Runoff from this catchment will flow overland to a proposed SWM facility for treatment and will then outlet to the wetland, discharging to **OUT-1 EAST**.
- Catchment area **PR-200** consists of 0.75 ha of land and includes the northern portion of the subject site. This catchment is comprised of proposed lots and a portion of the proposed roadway. Runoff from this catchment will drain towards a proposed SWM facility and will outlet to the wetland, discharging to **OUT-2 WEST**.
- Catchment area **PR-201** consists of 1.28 ha of land and includes a portion of the proposed roadway and residential lots. Runoff from this catchment will drain towards a proposed SWM facility and will outlet to the wetland, discharging to **OUT-2 EAST**.
- Catchment area **PR-202** consists of 1.40 ha of land and includes the northeastern portion of the site, consisting of the proposed roadway and lots. Runoff from this catchment will flow overland towards the wetland, discharging to **OUT-2 EAST**.
- Catchment **PR-300** consists of 8.50 ha of land includes the eastern portion of the site. This catchment is comprised of proposed lots and the existing wetland to the east. Runoff generated from this catchment will drain overland easterly to the existing wetland area (**OUT 3**) as in the existing condition.
- Catchment **PR-400** consists of 0.58 ha of land and includes the southern tip of the property, consisting of the rear yards of the proposed lots. Runoff from this catchment will drain overland, south easterly towards Lancaster Road as in the existing condition (**OUT 4**).



EX-100
0.22

CATCHMENT ID
CATCHMENT AREA (ha)
CATCHMENT BOUNDARY

— WETLAND SETBACK
- - - SUBJECT PROPERTY LINE

OUT OUTLET LOCATION
→ OVERLAND FLOW DIRECTION

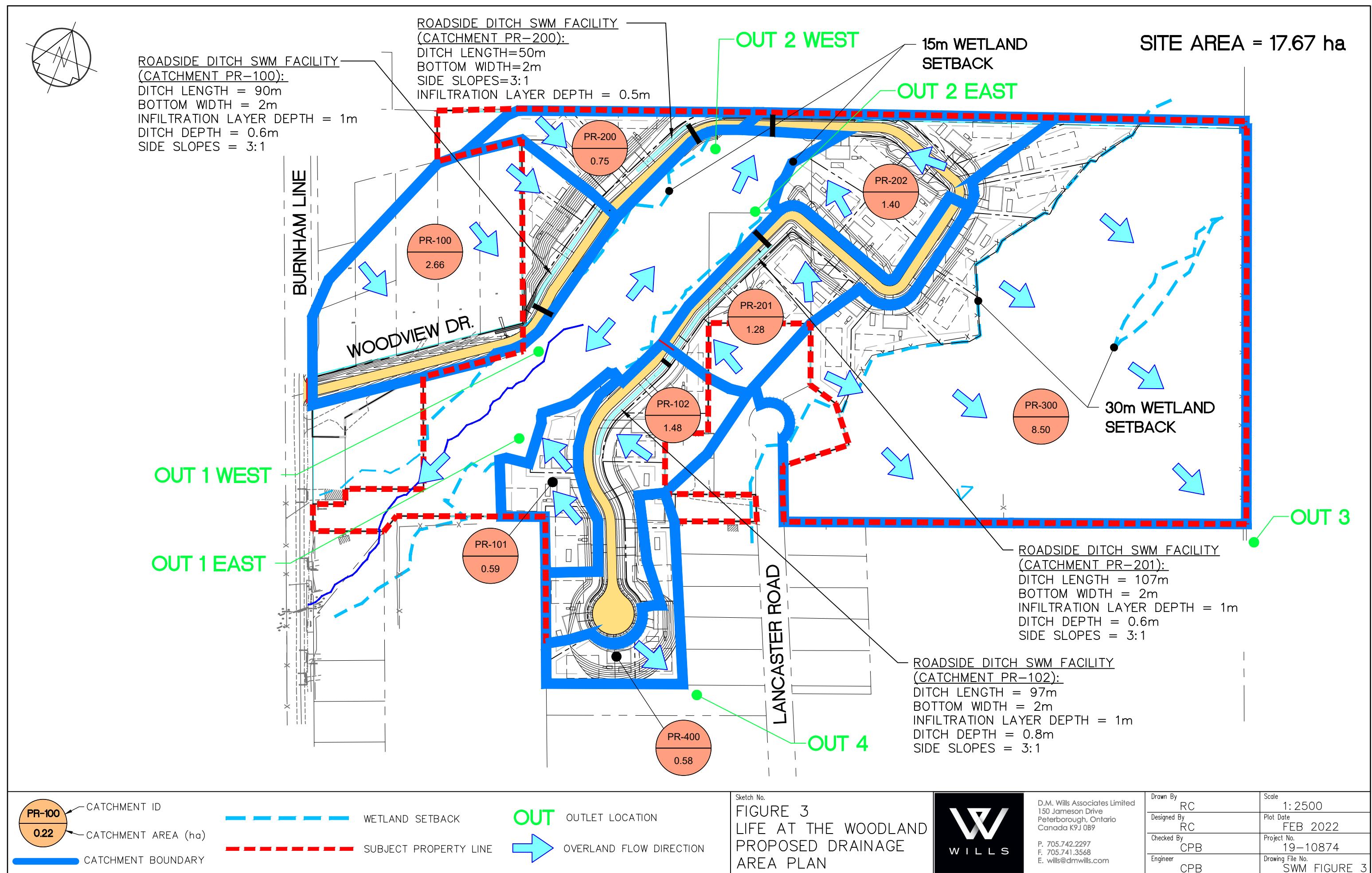
Sketch No. **FIGURE 2**
LIFE AT THE WOODLAND
EXISTING DRAINAGE
AREA PLAN



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Drawn By
RC
Designed By
RC
Checked By
CPB
Engineer
RC/CPB

Scale 1: 3000
Plot Date FEB 2022
Project No. 19-10874
Drawing File No. SWM FIGURE 2



The hydrologic parameters used for each catchment area, in both existing and proposed conditions, are summarized **Table 1** and documented in **Appendix A**.

Table 1 – Existing and Proposed Hydrologic Parameters

Standhyd ¹						
Catchment ID	Area (ha)	Impervious %	CN ^{*2}	Ia ³	Pervious Slope (%)	Impervious Slope (%)
PR-102	1.48	23	60.7	5.3	5.0	2.0
PR-201	1.28	24.6	62.5	5.8	6.6	1.0

Nashyd ¹					
Catchment ID	Area (ha)	Impervious %	CN ^{*2}	Ia ³	Tp ⁴ (hrs)
EX-100	2.02	1.9	61.5	5.3	0.17
EX-101	1.42	2.4	63.1	9.1	0.22
EX-200	1.53	0.0	61.7	8.7	0.17
EX-201	2.44	0.7	68.8	8.0	0.17
EX-300	8.72	0	64.6	8.8	0.39
EX-400	1.24	0	67.5	8.2	0.26
PR-100	2.66	9.7	64.8	4.8	0.17
PR-101	0.59	10.0	65.0	4.7	0.17
PR-200	0.75	16.1	68.1	7.4	0.17
PR-202	1.40	14.8	67.1	4.6	0.17
PR-300	8.50	1.6	64.4	8.4	0.39
PR-400	0.58	12.1	66.1	4.6	0.26

- Notes:
1. Command Line refers to the unit hydrograph used in the VO3 hydrologic model for the respective catchment area.
 2. CN* refers to the modified CN number adjusted to Antecedent Moisture Conditions II. Excludes Impervious Area for Standhyd.
 3. Ia refers to Initial Abstraction. Excludes Impervious Area for Standhyd.
 4. Tp refers to Time of Peak.

Hydrologic parameters such as soil infiltration properties, land use and runoff response were determined based on aerial photography, site reconnaissance and literature review. Topographic mapping and AutoCAD Civil 3D 2019 software were used to establish sub-catchment areas, land use and slopes. Rainfall data for the site is taken from the City of Peterborough Engineering Design Standards (April 2019) and is included in **Appendix A**.

4.0 Stormwater Management

4.1 Low Impact Development Design

As the practice of stormwater management has evolved, increasing emphasis has been placed on utilizing a treatment train approach to manage runoff as close to the source as possible. This design philosophy is often referred to as Low Impact Development (LID), where the ultimate goal is to maintain and mimic the natural hydrologic conditions. LID designs accomplish this by reducing the runoff volume generated by a site and implementing features that infiltrate, filter, evaporate, harvest and detain runoff, while also preventing pollution. ORCA encourages the use of LID features as part of the water quality design for a site and, therefore, opportunities to utilize these features have been investigated.

For infiltration based LID features, a minimum separation of 1.0 m is required from the bottom of feature to the higher of the seasonally high groundwater or bedrock elevation. As such, a geotechnical study with in-situ infiltration testing will ultimately be required to confirm the availability of minimum separation and observed infiltration rates.

LID features must also include an underdrain for infiltration rates less than 15 mm/hr. Sandy loam soils typically have infiltration rates from 30 to 50 mm/hr. and therefore underdrains are not anticipated to be required. This assumption can be confirmed once the in-situ infiltration rates have been established during detailed design.

A variety of LID features were considered for the development and evaluated based on site constraints, capital cost, maintenance considerations and water quality benefits. The preferred design selected are stone filled infiltration trenches with detention storage provided above the infiltration portion where required. These features will be incorporated as part of the roadside ditch system. The SWM facilities have been designed to achieve the necessary quality control targets.

4.2 Stormwater Quality Control

The proposed subdivision may cause additional pollutants to be conveyed off site. As such, the selection and sizing of the water quality measures are based on the procedures set out in the Stormwater Management Planning and Design Manual (MOE, March 2003) for Enhanced (Level 1) protection. As such, the goal of SWM is to preserve the natural hydrologic cycle. In addition, SWM measures should be assessed in the following order:

- Stormwater lot level controls
- Stormwater conveyance controls
- End-of-pipe SWM facilities

Stormwater lot level controls represent measures that are implemented on an individual lot basis such as soak-a-way pits, flatter grading and reduction of the impervious footprint.

Stormwater conveyance controls represent the conveyance systems used to transport stormwater runoff from the lots to the receiving waters such as pervious pipes, catchbasin treatment and grassed swales.

End-of-pipe SWM facilities represent the common urban SWM measures used to service numerous lots or whole subdivisions including wet ponds, wetlands, dry ponds, infiltration based facilities, Oil-Grit separators and filter systems.

4.2.1 Quality Control Summary

A SWM assessment was completed to evaluate the most appropriate measures to provide stormwater quality treatment for the proposed development. The following table summarizes the feasibility of each option for the proposed development.

Table 2 – Quality Control Feature Options Summary

Facility Description	Comments and Feasibility
Lot Level Controls <ul style="list-style-type: none">• Soak-Away Pits	<ul style="list-style-type: none">• Not a feasible option as a standalone water quality control for roadway runoff.
Conveyance Controls <ul style="list-style-type: none">• Pervious pipes• Catchbasin treatment• Grass Swales	<ul style="list-style-type: none">• Feasible option for water quality control.• Grassed swales can be considered as a viable option in combination with infiltration features to provide the necessary water quantity control.
End-of-Pipe Controls <ul style="list-style-type: none">• Wetlands• Wet Ponds• Dry Ponds• Infiltration Basins• Infiltration Trenches• Filter Strips• Sand Filters• Oil-Grit separators (OGS)	<ul style="list-style-type: none">• Not a feasible option due to site constraints and multiple outlets.• Wetlands are not feasible with available site area and configuration.• The increase in impervious area is not sufficient to consider a wet or dry pond facility as a viable option.• An OGS is not considered a viable option due to the outlet grade and configuration.• Infiltration basin/trench can be considered as viable options in combination with a conveyance feature to provide water quality control.• Filter systems are typically cumbersome, expensive and require extensive maintenance at regular intervals.

A review of the above-mentioned BMPs indicates that a hybrid feature incorporating conveyance and infiltration is an appropriate method for achieving the necessary quality control required.

Based on Table 3.2 of the Stormwater Management Planning and Design Manual, the proposed SWM facilities were designed to provide the necessary "Enhanced" level of protection for the proposed development. **Table 3** provides a summary of the proposed SWM features and demonstrates how water quality protection can be achieved for the selected sub-catchments.

Table 3 – Proposed Water Quality Treatment Summary

Description	Quality Control Feasibility
Catchment – PR-100 <ul style="list-style-type: none"> • Stone filled infiltration trench located within roadside ditch system. 	<ul style="list-style-type: none"> • To achieve Level 1 (enhanced) protection, a storage volume of 66.5 m³ is required based on Table 3.2 of the SWM Manual (2.66 ha x 25 m³/ha) • Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.
Catchment – PR-102 <ul style="list-style-type: none"> • Stone filled infiltration trench located within roadside ditch system. 	<ul style="list-style-type: none"> • To achieve Level 1 (enhanced) protection, a storage volume of 37 m³ is required based on Table 3.2 of the SWM Manual (1.48 ha x 25 m³/ha) • Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.
Catchment – PR-200 <ul style="list-style-type: none"> • Stone filled infiltration trench located within roadside ditch system. 	<ul style="list-style-type: none"> • To achieve Level 1 (enhanced) protection, a storage volume of 19 m³ is required based on Table 3.2 of the SWM Manual (0.75 ha x 25 m³/ha) • Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.
Catchment – PR-201 <ul style="list-style-type: none"> • Stone filled infiltration trench located within roadside ditch system. 	<ul style="list-style-type: none"> • To achieve Level 1 (enhanced) protection, a storage volume of 32 m³ is required based on Table 3.2 of the SWM Manual (1.28 ha x 25 m³/ha) • Water quality target will be achieved by the provision of an outlet located above the dedicated stone filled infiltration layer.

4.3 Stormwater Quantity Control

4.3.1 Peak Flow Calculations

Peak flows were estimated using Visual Othymo version 3.0 (VO3) hydrologic modelling software

for each of the 2, 5, 10, 25, 50 and 100-year storm events. These calculations consider the 6-hour SCS storm duration as prescribed by the City of Peterborough Engineering Design Standards (April 2019). The schematic layout of the VO3 model and the simulation results are presented in **Appendix B**.

Table 4 – Existing and Uncontrolled Peak Flow Rates – OUT 1 and OUT 2

Return Period	Peak Flow Rates (m³/s)							
	OUT 1 WEST		OUT 1 EAST		OUT 2 WEST		OUT 2 EAST	
	EX ¹	UNC ²	EX ¹	UNC ²	EX ¹	UNC ²	EX ¹	UNC ²
2-Year	0.042	0.063	0.020	0.081	0.025	0.017	0.056	0.092
5-Year	0.078	0.117	0.042	0.133	0.052	0.034	0.110	0.149
<u>10-Year</u>	0.107	0.159	0.060	0.171	0.073	0.046	0.151	0.196
<u>25-Year</u>	0.147	0.216	0.086	0.238	0.103	0.064	0.210	0.257
<u>50-Year</u>	0.180	0.264	0.107	0.283	0.128	0.078	0.257	0.320
<u>100-Year</u>	0.215	0.313	0.129	0.330	0.154	0.093	0.306	0.374

- Notes:
1. EX refers to the existing development condition. (NHYD = 1, 2, 3, 4)
 2. UNC refers to the proposed conditions without SWM controls. (NYHD = 6, 9, 13, 12)

As shown in **Table 4**, the proposed uncontrolled flows to **OUT 1 WEST**, **OUT 1 EAST** and **OUT 2 EAST** exceed the existing condition levels without the use of SWM controls, and therefore stormwater quantity controls will be required for these outlet locations. The proposed uncontrolled flows to **OUT 2 WEST** are reduced due to a reduction in drainage area discharging to that location in the proposed condition. As a result, stormwater quantity controls will not be required for **OUT 2 WEST**. The outlet locations are shown on **Figure 2** and **Figure 3**.

Table 5 – Existing and Uncontrolled Peak Flow Rates – OUT 3 and OUT 4

Return Period	Peak Flow Rates (m³/s)			
	OUT 3		OUT 4	
	EX ¹	UNC ²		
2-Year	0.089	0.089	0.020	0.011
5-Year	0.184	0.182	0.040	0.021
10-Year	0.261	0.256	0.056	0.028
25-Year	0.369	0.361	0.078	0.038
50-Year	0.458	0.448	0.096	0.047
100-Year	0.553	0.541	0.115	0.055

- Notes:
1. EX refers to the existing development condition. (NHYD = 5, 55)
 2. UNC refers to the proposed condition without SWM controls. (NYHD = 14, 56)

In the post development condition for Outlet 3 (**OUT 3**), a portion of the overall developed site, including six (6) residential homes and backyards, will be directed to

the outlet. In the post development condition for Outlet 4 (**OUT 4**), a portion of the rear yards at the southern tip of the property will be directed to the outlet. A review of the hydrologic parameters and modelling indicates a reduction in drainage area to both **OUT 3** and **OUT 4**, offsetting the increase in impervious area. As a result and as outlined in **Table 5**, there is no increase in peak flow rates discharging to **OUT 3** and **OUT 4**, and therefore no stormwater quantity controls will be required for either outlet.

4.3.2 Quantity Control Summary

In accordance with the design criteria established in **Section 3.1**, quantity controls are required to ensure that post-development flow rates do not exceed existing conditions, for each outlet, up to the 100-year storm. The VO3 model is used to estimate the required storage volume to provide the necessary quantity control without overtopping. A preliminary design of the combination stone filled infiltration trenches / detention ditches have been completed to confirm that sufficient stage storage can be provided. The flow regulation can be achieved by means of an outlet control structure for each facility.

4.4 Stormwater Management Facilities

SWM facilities will be required for the development to achieve the necessary quality and quantity control targets. As discussed in **Table 3**, stone filled infiltration trenches will provide the necessary water quality control for each outlet location. As necessary, an open detention portion will be provided above the infiltration trench as part of the roadside ditch system, and will be controlled by a dedicated outlet structure within each facility.

4.4.1 Design Overview

The preliminary selection of the SWM facilities was designed based on the required volume targets, outlet configuration and site topography. A review of **Table 6** provides a summary of each SWM facility for each outlet location.

Table 6 – Proposed Stormwater Management Facility Summary

Catchment	Outlet ID	Design Summary
PR-100	OUT-1 WEST	<ul style="list-style-type: none"> • 1.0 m deep stone filled infiltration trench, 2.0 m in width and 90 m in length • Required storage volume of stone filled trench for quality control is 66.5 m³, with 72 m³ provided. • Total storage volume required for quantity control is 261 m³, with 278 m³ provided at 0.6 m depth. • One stage outlet control is assumed in the preliminary calculations, multi-stage will be considered during detailed design to maximize outlet efficiency and reduce facility size.
PR-102	OUT-1 EAST	<ul style="list-style-type: none"> • 1.0m deep stone filled infiltration trench, 2.0 m in width and 97 m in length • Required storage volume of stone filled trench for quality control is 37 m³, with 74 m³ provided. • Total storage volume required for quantity control is 433 m³, with 435 m³ provided at 0.8m depth. • One stage outlet control is assumed in the preliminary calculations, multi-stage will be considered during detailed design to maximize outlet efficiency and reduce facility size.
PR-200	OUT-2 WEST	<ul style="list-style-type: none"> • 0.5 m deep stone filled infiltration trench, 2.0 m in width and 50 m in length. • Required storage volume of stone filled trench for quality control is 19 m³, with 21 m³ provided. • Stormwater quantity control not required for PR-200.
PR-201	OUT-2 EAST	<ul style="list-style-type: none"> • 1.0 m deep stone filled infiltration trench, 2.0 m in width and 107 m in length • Required storage volume of stone filled trench for quality control is 32 m³, with 52 m³ provided. • Total storage volume required for quantity control is 200 m³, with 301 m³ provided at 0.6 m depth. • One stage outlet control is assumed in the preliminary calculations, multi-stage will be considered during detailed design to maximize outlet efficiency and reduce facility size.

A review of **Table 6** indicates that sufficient storage volumes can be provided within the SWM facilities to meet the LID, water quality and water quantity control requirements. A geotechnical study of the site is recommended during the detailed design phase to

determine actual infiltration rates and groundwater levels to confirm the final dimensions of the proposed facility and to include a shallow infiltration bottom to the proposed facilities.

4.4.2 Proposed Release Rates

The proposed peak flow rates for from the preliminary SWM facilities with respect to design storm events are shown in **Table** below.

Table 7 – Existing and Proposed Peak Flow Summary

Return Period	Peak Flow Rates (m^3/s)							
	OUT 1 WEST		OUT 1 EAST		OUT 2 WEST		OUT 2 EAST	
	EX ¹	PR ²	EX ¹	PR ²	EX ¹	PR ²	EX ¹	PR ²
2-Year	0.042	0.020	0.020	0.020	0.025	0.017	0.056	0.056
5-Year	0.078	0.068	0.042	0.038	0.052	0.034	0.110	0.110
10-Year	0.107	0.104	0.060	0.049	0.073	0.046	0.151	0.149
25-Year	0.147	0.140	0.086	0.065	0.103	0.064	0.210	0.194
50-Year	0.180	0.165	0.107	0.077	0.128	0.078	0.257	0.232
100-Year	0.215	0.186	0.129	0.089	0.154	0.093	0.306	0.268

- Notes:
1. EX refers to the existing development condition. (NHYD = 1, 2, 3, 4)
 2. PR refers to the proposed conditions with controlled flows from the proposed control facility. (NYHD = 16, 20, 13, 24)

A review of **Table 7** indicates the proposed SWM facilities will provide the required quantity controls such that the proposed development will not increase peak flow rates at each outlet location. Stage-Storage-Discharge calculations are provide for each facility in **Appendix D**. It is noted that these facilities have been conservatively designed using a single outlet control. During detailed design, the outlet configuration and infiltration storage depth for each facility will be optimized to reduce the storage volume requirements.

5.0 Conclusion

As the proposed residential subdivision will alter existing drainage patterns, a preliminary stormwater management report has been prepared to address the requirements of the County of Peterborough and ORCA.

Low Impact Development considerations and stormwater quality controls such as stone filled infiltration trenches within the roadway corridor can be provided to achieve "Enhanced" Level 1 protection as defined in the Stormwater Management Planning and Design Manual (March 2003).

Water quantity controls can be provided by the stone filled infiltration ditches within the roadway corridor with outlet control structures providing detention control to existing condition levels.

Preliminary Stormwater Management Report
Life at the Woodland Subdivision



If you require any further information, or have any questions, please do not hesitate to contact the undersigned.

Respectfully submitted,



Chris Proctor-Bennett, P.Eng.
Group Leader, Stormwater Management

Mark Wilson, A.Sc.T.
Water Resources Designer

A handwritten signature of "Mark Wilson" in black ink.

MW/CPB/jl

Statement of Limitations

This report has been prepared by D.M. Wills Associates Limited on behalf of Mr. Rubal Kundra of Life at the Woodland Inc. to address the requirements of the County of Peterborough and ORCA.

The conclusions and recommendations in this report are based on available background documentation and discussions with applicable agencies at the time of preparation.

The report is intended to determine the feasibility of the proposed development with respect to Stormwater Management of the Site. The design information provided in this report is preliminary in nature and should not be used for site plan application or construction purposes.

Any use that a third party makes of this report other than a Preliminary Stormwater Management Report for the proposed development is the responsibility of such third parties. D.M. Wills Associates Limited accepts no responsibility for damages, if any, suffered by a third party as a result of decisions made or action taken based on using this report for purposes other than a Preliminary Stormwater Management Report for the proposed Life at the Woodland residential subdivision.

Appendix A

Rainfall Data and Hydrology



City Of Peterborough – Engineering Design Standards

B.1 Storm Sewer System

City of Peterborough Standard Drawings and Specifications shall be adhered to at all times. Where the City has no standard or specification, the City of Peterborough recognizes the July 1984 release of the Ministry of Environment Guidelines for the Design of Storm Sewer Systems as the guidelines by which all storm sewer work shall conform to. Otherwise, OPSS or OPSD shall apply.

B.1.1 Definition and Use

Storm systems may consist of one or any combination of pipes, ditches, culverts, open channels and storm water management facilities that convey storm water.

Storm sewers shall be designed to collect storm water discharge from pervious and impervious areas both on private and public lands. Storm drainage connected to buildings on private property requires a building permit before installation.

B.1.2 Location and Alignment

All works to be constructed within a City road allowance are to be located in accordance with the appropriate City of Peterborough Drawing from standards USD100.01 thru USD100.13. The City must approve locating works in non-standard locations.

Storm sewers connected to buildings on private property are regulated by Part 7 of the OBC. Where there are no specific regulations in the OBC, details from this document shall apply.

Connections to existing storm sewer systems shall be made at manholes. Where no manhole is present a new manhole is required on the City's main. Connections between storm sewer pipes on private property, where not at a manhole or catchbasin, shall be made with manufactured 'Tees' and only with approval from the City engineering department and only if sewer is not defined as a *building sewer* 200mm or greater. Control manholes for private sewers shall be placed on the front property line or just inside the property if placement on the property line is not possible.

B.1.3 Drainage / Sub Drainage Area Plans

Drainage/sub-drainage area limits for sewer designs are to be in accordance with approved grading plans to the proposed maintenance holes (or catchbasins if applicable) located on the R.O.W.

Note: All areas and runoff coefficients are to be shown for each drainage/sub-drainage areas.

City Of Peterborough – Engineering Design Standards

B.1.4 External Watershed Limits and Drainage Areas

When design abuts undeveloped areas, identify the external watershed limit to be designed for, typically following contour lines. Developed external areas should encompass the entire sewershed.

Note: All areas, runoff coefficients and time of concentrations are to be shown for all drainage areas within external watershed limits.

B.1.5 Design Chart

Storm sewer design calculations are to be completed on an appropriate Storm Sewer Design chart.

B.1.6 Design Requirements and Location

The City of Peterborough rainfall data based upon 2002 AES Peterborough Airport IDF shall be used for the development of rainfall intensities for storm sewer design. Alternatively, IDF curve parameters A, B, and C provided in Table B.1.7.1 may be used.

Storm sewers shall be designed as a separate sewer system. Effluent from sanitary sewers or any potentially contaminated drainage from industrial, agricultural or commercial operations shall not be discharged into storm sewers. Contaminated drainage means, the introduction of any foreign, undesirable physical, chemical or biological substance into the environment, which results or is likely to result in deleterious effects.

Storm sewers shall be designed as deep storm sewers with approximately 3.0m of cover where private gravity service connections are required. An acceptable alternative to the deep sewer system is the provision of a separate foundation drainage system (generally with smaller pipes) with gravity service connections as well as a traditional storm sewer system with shallow pipes. Where physical constraints do not allow for either above noted system, a shallow system may be approved with pipe typically 1.25m deep.

The alignment of the storm varies depending on the type of road and whether or not deep storm sewers are to be implemented. Typically, deep storm sewers are offset 1.5m on one side of the centreline with the sanitary sewer offset 1.5m from the other side of the centreline. Shallow storm sewers, particularly those less than 450mm in diameter, are typically located 0.31 metres within the curb face. Storm sewers are generally to the north or west of the centerline.

MOE Guidelines require 0.5m vertical or 2.5m horizontal clearances between sewers and watermains. In some circumstances it may be prudent for the PUC/City jointly to decide by what means/best practice one main crosses the other in addition to MOE

City Of Peterborough – Engineering Design Standards

design guidelines. Watermain bends may be required at sewer/watermain pipe crossings while sometimes it may be more appropriate to change the grade of a sewer, depending on the circumstances.

The capacity of the minor storm sewer systems shall typically be designed to carry the peak flow resulting from a one (1) in five (5) year rainfall event. Where gravity foundation service connections exist, the five year design flow must not exceed 80% of the just full pipe capacity.

Where gravity service connections exist or are proposed, a 100 year hydraulic grade line analysis must be undertaken, to determine peak 100 year water levels within a potentially surcharged storm sewer system. A minimum freeboard of 0.50m must be provided between the computed 100 year hydraulic grade line and the minimum basement floor level in conjunction with the use of backflow preventers. Where the change in grade has the potential for hydraulic jumps, additional freeboard shall be provided. The implementation of flow regulating ICDs may be permitted by the City Engineer to reduce 100 year storm sewer flows on a case by case basis only at low points in the road, however in all instances, the 5 year flow must pass through the ICD unencumbered with minimal backwater head and no surface ponding. Pipe sizes should be increased elsewhere to accommodate the 100 year flow with appropriate hydraulic grade line elevations.

The major system design shall be based on a one in 100 year rainfall event and should include assessment of road sags and boulevard overflows into stormwater management ponds and watercourses. The maximum ponding depth shall not exceed 300mm as measure to the centerline of the road.

B.1.7 Peak Flow Calculation and Storm Sewer Design

The design area shall include all areas, which reasonably or naturally drain to the system. To calculate the peak rate of runoff from an area, the Rational Method shall be used as follows:

$$Q = K \cdot A \cdot i \cdot C$$

Where:

'Q' - is peak flow (l/s)

'K' - is 2.78

'A' - is the area (hectares)

'i' - is the rainfall intensity (mm/hour) calculated as follows:

$$i = \frac{A}{(Tc + B)^C}$$

or as directly derived from 2002 Peterborough Airport IDF curves

Where: A, B and C are per Table B.1.7.1.

Table B.1.7.1

	A	B	C
2 Year	662	7.5	0.79
5 Year	1098	10.1	0.83
10 Year	1560	13	0.86
25 Year	2010	14	0.88
50 Year	2200	14.6	0.87
100 Year	2507	14.8	0.88

Please note that the above A, B, C values shall be used for storm sewer design only, or other calculations design storms of less than 3 hours duration. Stormwater Management Reports should use rainfall directly from the 2006 Peterborough Airport IDF curves.

The time of concentration (Tc) should be calculated rather than relying upon arbitrary minimum and maximum times. Where this is not practical, a ten (10) minute time of concentration (Tc) shall be used except when the zoning requires the use of a runoff coefficient of 0.75 or higher in which case five (5) minute time of concentration (Tc) shall be used.

'C' - is the co-efficient of run-off

The runoff co-efficient or "C" for storm drainage unless otherwise specified or adequately proven through calculation, shall be per Table B.1.7.2 for the 5 year design.

Table B.1.7.2

Parks – over 4.0 ha	0.20
Parks – 4.0 ha and under	0.25
Single family residential-15m lots	0.55
Single family residential-12m lots	0.65
Single family residential-9m lots	0.75
Semi-detached	0.80
Townhouses	0.85
Apartments	0.90
Schools and Churches / Industrial	Varies
Commercial	0.90
Heavily Developed Areas	0.90
Asphalt, Concrete, Roofed Areas	0.95

City Of Peterborough – Engineering Design Standards

25 to 100 year runoff co-efficients shall be increased to account for soil saturation. Increase co-efficients for the 25, 50, and 100 year storms by 10%, 20%, and 25% respectively up to a maximum value of 0.95.

B.1.7.1 Flow Velocities and Minimum Slope

Storm sewer flow velocities shall not be less than 0.8 m/s when flowing full or 0.6m/s at design depth. Minimum longitudinal slope shall be 0.5%. The preferred maximum velocity is 3.0 m/s with an absolute maximum acceptable velocity of 6.0 m/s.

B.1.7.2 Pipe Cover

The minimum depth of cover to pipe crown shall be 1.2 m. Excessive cover should be avoided except under special circumstances.

Minimum pipe cover for deep sewers shall be based upon providing gravity connections including hydraulic grade line freeboard for storm services.

For concrete pipe, the maximum allowable cover permitted on concrete pipe to be constructed is to be based on OPSD 807.010, 807.030, 807.040 and 807.050. Where the pipe required exceeds the OPSD charts, a pipe design sealed by a Professional Engineer must be submitted to the City for approval.

For flexible pipe, the maximum allowable cover permitted shall be as per OPSD or manufacturers specifications.

B.1.7.3 Gravity Pipe Design

The minimum pipe diameter for storm sewers shall be 250 mm. Minimum pipe diameter for catchbasins leads shall be 250mm with the exception of double catchbasins which shall be 300mm.

The obvert of the inlet pipe at all maintenance holes shall be higher than or equal to the obvert of the outlet pipe. Appropriate invert elevation drops to account for the velocity head, transition and bend losses within manholes should be provided.

An outlet pipe from a manhole is not permitted to be smaller than the incoming pipe even if the outlet pipe has adequate capacity due to greater slope. Allowances may be granted by the City Engineer in special circumstances to allow a smaller outlet pipes on privately owned property in the event other regulatory agencies (e.g. MTO) require this for stormwater retention.

The Manning equation shall be used to calculate the required hydraulic capacity of a gravity sewer as follows:

6 Hour SCS Type II Intensity Hyetographs
 2006 Peterborough Airport Weather Station
 (mm/hr)

Time (min.)	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
0	0	0	0	0	0	0
15	1.6	2.1	2.5	2.9	3.3	3.6
30	1.6	2.1	2.5	2.9	3.3	3.6
45	2.3	3.2	3.7	4.4	4.9	5.4
60	2.3	3.2	3.7	4.4	4.9	5.4
75	2.3	3.2	3.7	4.4	4.9	5.4
90	2.3	3.2	3.7	4.4	4.9	5.4
105	3.9	5.2	6.2	7.3	8.1	9.0
120	3.9	5.2	6.2	7.3	8.1	9.0
135	4.6	6.3	7.4	8.8	9.8	10.8
150	4.6	6.3	7.4	8.8	9.8	10.8
165	23.2	31.4	36.9	43.7	48.9	53.9
180	60.4	81.78	95.9	113.7	127.0	140.2
195	8.5	11.5	13.5	16.0	17.9	19.8
210	8.5	11.5	13.5	16.0	17.9	19.8
225	3.9	5.2	6.2	7.3	8.1	9.0
240	3.9	5.2	6.2	7.3	8.1	9.0
255	3.1	4.2	4.9	5.8	6.5	7.2
270	3.1	4.2	4.9	5.8	6.5	7.2
285	2.3	3.2	3.7	4.4	4.9	5.4
300	2.3	3.2	3.7	4.4	4.9	5.4
315	1.6	2.1	2.5	2.9	3.3	3.6
330	1.6	2.1	2.5	2.9	3.3	3.6
345	1.6	2.1	2.5	2.9	3.3	3.6
360	1.6	2.1	2.5	2.9	3.3	3.6

Hydrologic Parameters for EX-100			Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: MW / CPB Date: 22-Feb-22		

Land Use			Rainfall Data																																						
<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th>Internal</th> <th>External</th> <th></th> </tr> </thead> <tbody> <tr> <td>Agriculture</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Range</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Grass</td> <td>0.35</td> <td>1.47</td> <td>ha</td> </tr> <tr> <td>Woods</td> <td>0.10</td> <td>0.06</td> <td>ha</td> </tr> <tr> <td>Wetland</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Gravel</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Impervious</td> <td>0.00</td> <td>0.04</td> <td>ha</td> </tr> <tr> <td>SUM</td> <td>0.45</td> <td>1.57</td> <td></td> </tr> </tbody> </table>				Internal	External		Agriculture	0.00	0.00	ha	Range	0.00	0.00	ha	Grass	0.35	1.47	ha	Woods	0.10	0.06	ha	Wetland	0.00	0.00	ha	Gravel	0.00	0.00	ha	Impervious	0.00	0.04	ha	SUM	0.45	1.57		Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm		
	Internal	External																																							
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			Drainage Area 2.02 ha Impervious Area 0.04 ha Percent Impervious 1.9% Connected Impervious 1.9%																																						
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	Pervious	Impervious																																							
Hydrologic Soil Group ¹	B	B																																							
Soil Type	0	0																																							
C	0.21	0.21																																							
CN (Nashyd)	60.3	61.8																																							

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.21	n.a.
	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.21	
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	60.3	60.3
	B	74	65	61	58	50	85	98	61.8	
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	5.3	5.4

Time of Concentration ⁶	
Pervious Length	125 m
Slope	15.2 %
Airport	13.2 min.
Bransby - Williams	3.9 min. Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	10.1 min. 0.17 hr.

Composite Parameters	
Drainage Area	2.02 ha
Runoff Coefficient	0.21
SCS Curve No.	61.5 60.8
Modified Curve No. ⁴ , CN*	61.5 60.7
Initial Abstraction.	5.3 5.4

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for EX-101									Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: MW / CPB Date: 22-Feb-22								

Land Use					Rainfall Data				
					Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm				
Agriculture 0.00 0.00 ha Range 0.21 0.07 ha Grass 0.08 0.00 ha Woods 0.96 0.07 ha Wetland 0.00 0.00 ha Gravel 0.00 0.00 ha Impervious 0.03 0.00 ha SUM 1.27 0.14					Drainage Area 1.42 ha Impervious Area 0.03 ha Percent Impervious 2.4% Connected Impervious 0.2%				
Hydrologic Soil Group¹ B B Soil Type 0 0 C 0.15 0.17 CN (Nashyd) 60.4 61.5					Pervious Length 110 m US Elev 212.2 m DS Elev 207.5 m Slope 4.3 % Rolling				

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient², C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.15	n.a.
	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.17	
SCS Curve No.³, CN	B	74	65	61	58	50	85	98	60.4	59.4
	B	74	65	61	58	50	85	98	61.5	
Initial Abstraction⁵, mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	9.1	9.3

Time of Concentration ⁶		
Total Length	110	m
Average Slope	4.3	%
Airport	20.1	min.
Bransby - Williams	4.5	min.
	Flat: 0-2% Slopes	
	Rolling: 2-6% Slopes	
	Hilly: >6% Slopes	
Applicable Minimum⁷	15.0	min.
Time to Peak	13.5	min.
	0.22	hr.

Composite Parameters		
Drainage Area	1.42 ha	
Runoff Coefficient	0.15	
SCS Curve No.	60.5	59.6
Modified Curve No.⁴, CN*	63.1	62.7
Initial Abstraction.	9.1	9.3

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. Connected Impervious is estimated using the Sutherland Equation with a Watershed Selection Criteria of Somewhat Connected

Hydrologic Parameters for EX-200									Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: MW / CPB Date: 22-Feb-22								

Land Use					Rainfall Data				
					Gauging Station = Peterborough				
					12 hr, 100 Yr Rainfall = 90.4 mm				
					Drainage Area 1.53 ha Impervious Area 0.00 ha Percent Impervious 0.0% Connected Impervious 0.0%				
					Pervious Length 130 m US Elev 225.9 m DS Elev 211.6 m Slope 11.0 % Steep				
Hydrologic Soil Group ¹		B	B						
Soil Type		0	0						
C		0.27	0.23						
CN (Nashyd)		58.6	59.8						

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.27	n.a.
	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.23	
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	58.6	58.6
	B	74	65	61	58	50	85	98	59.8	
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.7	8.7

Time of Concentration ⁶		
Total Length	130	m
Average Slope	11.0	%
Airport Bransby - Williams	14.1 4.4	min. min.
	Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes	
Applicable Minimum ⁷	15.0	min.
Time to Peak	10.1 0.17	min. hr.

Composite Parameters	
Drainage Area	1.53 ha
Runoff Coefficient	0.26
SCS Curve No.	58.8 58.8
Modified Curve No. ⁴ , CN*	61.7 61.7
Initial Abstraction.	8.7 8.7

Notes:

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for EX-201			Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: MW / CPB Date: 22-Feb-22		

Land Use			Rainfall Data																																						
<table> <thead> <tr> <th></th> <th>Internal</th> <th>External</th> <th></th> </tr> </thead> <tbody> <tr> <td>Agriculture</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Range</td> <td>2.16</td> <td>0.24</td> <td>ha</td> </tr> <tr> <td>Grass</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Woods</td> <td>0.02</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Wetland</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Gravel</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Impervious</td> <td>0.00</td> <td>0.02</td> <td>ha</td> </tr> <tr> <td>SUM</td> <td>2.18</td> <td>0.26</td> <td></td> </tr> </tbody> </table>				Internal	External		Agriculture	0.00	0.00	ha	Range	2.16	0.24	ha	Grass	0.00	0.00	ha	Woods	0.02	0.00	ha	Wetland	0.00	0.00	ha	Gravel	0.00	0.00	ha	Impervious	0.00	0.02	ha	SUM	2.18	0.26		Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm		
	Internal	External																																							
Agriculture	0.00	0.00	ha																																						
Range	2.16	0.24	ha																																						
Grass	0.00	0.00	ha																																						
Woods	0.02	0.00	ha																																						
Wetland	0.00	0.00	ha																																						
Gravel	0.00	0.00	ha																																						
Impervious	0.00	0.02	ha																																						
SUM	2.18	0.26																																							
			Drainage Area 2.44 ha Impervious Area 0.02 ha Percent Impervious 0.7% Connected Impervious 0.7%																																						
<table> <thead> <tr> <th>Hydrologic Soil Group¹</th> <th>B</th> <th>B</th> </tr> <tr> <th>Soil Type</th> <th>0</th> <th>0</th> </tr> <tr> <th>C</th> <th>0.30</th> <th>0.34</th> </tr> <tr> <th>CN (Nashyd)</th> <th>64.9</th> <th>67.3</th> </tr> </thead> </table>			Hydrologic Soil Group ¹	B	B	Soil Type	0	0	C	0.30	0.34	CN (Nashyd)	64.9	67.3	Pervious Length 100 m US Elev 213.2 m DS Elev 206.6 m Slope 6.6 % Hilly																										
Hydrologic Soil Group ¹	B	B																																							
Soil Type	0	0																																							
C	0.30	0.34																																							
CN (Nashyd)	64.9	67.3																																							

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.30	n.a.
	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.34	
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	64.9	64.9
	B	74	65	61	58	50	85	98	67.3	
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.0	8.0

Time of Concentration ⁶	
Total Length	100 m
Average Slope	6.6 %
Airport Bransby - Williams	13.9 min. 3.6 min.
	Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	10.1 min. 0.17 hr.

Composite Parameters	
Drainage Area	2.44 ha
Runoff Coefficient	0.30
SCS Curve No.	65.2 64.9
Modified Curve No. ⁴ , CN*	68.8 68.5
Initial Abstraction.	8.0 8.0

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for EX-300			Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22		

Land Use			Rainfall Data		
Internal			Gauging Station = Peterborough		
Agriculture 0.00 ha Range 5.25 ha Grass 0.00 ha Woods 3.47 ha Wetland 0.00 ha Gravel 0.00 ha Impervious 0.00 ha SUM 8.72			12 hr, 100 Yr Rainfall = 90.4 mm		
			Drainage Area 8.72 ha Impervious Area 0.00 ha Percent Impervious 0.0% Connected Impervious 0.0%		
Hydrologic Soil Group¹ B Soil Type 0 C 0.18 CN (Nashyd) 62.2			Pervious Length 330 m US Elev 213.5 m DS Elev 200.9 m Slope 3.8 % Rolling		

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.18	n.a.
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	62.2	62.2
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.8	8.8

Time of Concentration ⁶	
Total Length	330 m
Average Slope	3.8 %
Airport Bransby - Williams	35.2 min. 11.6 min. Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	23.6 min. 0.39 hr.

Composite Parameters	
Drainage Area	8.72 ha
Runoff Coefficient	0.18
SCS Curve No.	62.2 62.2
Modified Curve No. ⁴ , CN*	64.6 64.6
Initial Abstraction.	8.8 8.8

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for EX-400			Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22		

Land Use			Rainfall Data		
Internal			Gauging Station = Peterborough		
Agriculture 0.00 ha Range 1.09 ha Grass 0.00 ha Woods 0.15 ha Wetland 0.00 ha Gravel 0.00 ha Impervious 0.00 ha SUM 1.24			12 hr, 100 Yr Rainfall = 90.4 mm		
			Drainage Area 1.24 ha Impervious Area 0.00 ha Percent Impervious 0.0% Connected Impervious 0.0%		
Hydrologic Soil Group¹ B Soil Type 0 C 0.21 CN (Nashyd) 64.2			Pervious Length 165 m US Elev 211.6 m DS Elev 204.8 m Slope 4.1 % Rolling		

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.21	n.a.
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	64.2	64.2
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.2	8.2

Time of Concentration ⁶	
Total Length	165 m
Average Slope	4.1 %
Airport Bransby - Williams	23.5 min. 6.9 min. Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	15.7 min. 0.26 hr.

Composite Parameters	
Drainage Area	1.24 ha
Runoff Coefficient	0.21
SCS Curve No.	64.2 64.2
Modified Curve No. ⁴ , CN*	67.5 67.5
Initial Abstraction.	8.2 8.2

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for PR-100			Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22		

Land Use			Rainfall Data																																						
<table border="1"> <thead> <tr> <th></th> <th>Internal</th> <th>External</th> <th>ha</th> </tr> </thead> <tbody> <tr> <td>Agriculture</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Range</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Grass</td> <td>0.87</td> <td>1.47</td> <td>ha</td> </tr> <tr> <td>Woods</td> <td>0.00</td> <td>0.06</td> <td>ha</td> </tr> <tr> <td>Wetland</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Gravel</td> <td>0.00</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Impervious</td> <td>0.22</td> <td>0.04</td> <td>ha</td> </tr> <tr> <td>SUM</td> <td>1.09</td> <td>1.57</td> <td></td> </tr> </tbody> </table>				Internal	External	ha	Agriculture	0.00	0.00	ha	Range	0.00	0.00	ha	Grass	0.87	1.47	ha	Woods	0.00	0.06	ha	Wetland	0.00	0.00	ha	Gravel	0.00	0.00	ha	Impervious	0.22	0.04	ha	SUM	1.09	1.57		Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm		
	Internal	External	ha																																						
Agriculture	0.00	0.00	ha																																						
Range	0.00	0.00	ha																																						
Grass	0.87	1.47	ha																																						
Woods	0.00	0.06	ha																																						
Wetland	0.00	0.00	ha																																						
Gravel	0.00	0.00	ha																																						
Impervious	0.22	0.04	ha																																						
SUM	1.09	1.57																																							
			Drainage Area 2.66 ha Impervious Area 0.26 ha Percent Impervious 9.7% Connected Impervious 9.7%																																						
<table border="1"> <thead> <tr> <th>Hydrologic Soil Group¹</th> <th>B</th> <th>B</th> </tr> <tr> <th>Soil Type</th> <th>0</th> <th>0</th> </tr> <tr> <th>C</th> <th>0.33</th> <th>0.21</th> </tr> <tr> <th>CN (Nashyd)</th> <th>68.5</th> <th>61.8</th> </tr> </thead> </table>			Hydrologic Soil Group ¹	B	B	Soil Type	0	0	C	0.33	0.21	CN (Nashyd)	68.5	61.8	<table border="1"> <thead> <tr> <th>Pervious</th> <th>Impervious</th> </tr> </thead> <tbody> <tr> <td>Length 125</td> <td>8 m</td> </tr> <tr> <td>US Elev 226.5</td> <td>207.5 m</td> </tr> <tr> <td>DS Elev 207.5</td> <td>207.3 m</td> </tr> <tr> <td>Slope 15.2</td> <td>2.0 %</td> </tr> <tr> <td>Steep</td> <td>Flat</td> </tr> </tbody> </table>			Pervious	Impervious	Length 125	8 m	US Elev 226.5	207.5 m	DS Elev 207.5	207.3 m	Slope 15.2	2.0 %	Steep	Flat												
Hydrologic Soil Group ¹	B	B																																							
Soil Type	0	0																																							
C	0.33	0.21																																							
CN (Nashyd)	68.5	61.8																																							
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DS Elev 207.5	207.3 m																																								
Slope 15.2	2.0 %																																								
Steep	Flat																																								

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.33	n.a.
	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.21	
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	68.5	61.0
	B	74	65	61	58	50	85	98	61.8	
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.8	5.1

Time of Concentration ⁶	
Pervious Length	125 m
Slope	15.2 %
Airport Bransby - Williams	12.5 min. 3.7 min. Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	10.1 min. 0.17 hr.

Composite Parameters	
Drainage Area	2.66 ha
Runoff Coefficient	0.26
SCS Curve No.	64.5 60.9
Modified Curve No. ⁴ , CN*	64.8 60.6
Initial Abstraction.	4.8 5.1

Notes:

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for PR-101					Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22				

Land Use				Rainfall Data									
Controlled Lots		Uncontrolled Lots		Roadway	External	Gauging Station = Peterborough							
Agriculture		0.00		0.00		ha							
Range		0.00		0.00		ha							
Grass		0.53		ha									
Woods		0.00		0.00		ha							
Wetland		0.00		0.00		ha							
Gravel		0.00		0.00		ha							
Impervious		0.00		0.06		ha							
SUM		0.00		0.59									
Hydrologic Soil Group¹ B B Soil Type 0 0 C 0.21 CN (Nashyd) 64.7													
Pervious Impervious Length 40 5 m US Elev 212.2 211.0 m DS Elev 210.2 210.9 m Slope 5.0 2.0 % Rolling Flat													

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.21	n.a.
	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90		
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	64.7	61.0
	B	74	65	61	58	50	85	98		
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.7	5.0

Time of Concentration ⁶	
Total Length	45 m
Average Slope	4.7 %
Airport Bransby - Williams	11.7 min. 2.0 min.
Applicable Minimum ⁷	15.0 min.
Time to Peak	10.1 min. 0.17 hr.

Composite Parameters	
Drainage Area	0.59 ha
Runoff Coefficient	0.21
SCS Curve No.	64.7 61.0
Modified Curve No. ⁴ , CN*	65.0 60.5
Initial Abstraction.	4.7 5.0

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. Connected Impervious does not include areas that discharge to pervious surfaces.

Hydrologic Parameters for PR-102						Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22					

Land Use				Rainfall Data		
Controlled Lots Agriculture 0.00 Range 0.00 Grass 0.70 Woods 0.00 Wetland 0.00 Gravel 0.00 Impervious 0.08 SUM 0.78				Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm		
Roadway 0.00 0.29 0.08 0.07 0.00 0.00 0.23 0.52				Drainage Area 1.48 ha Impervious Area 0.35 ha Percent Impervious 23.3% Connected Impervious 23.3%		
External 0.00 0.00 0.00 0.00 0.00 0.00 0.03 0.18				Pervious Length 40 m US Elev 212.2 m DS Elev 210.2 m Slope 5.0 % Rolling		
Hydrologic Soil Group¹ B B B Soil Type 0 0 0 C 0.21 0.48 0.26 CN (Nashyd) 64.7 77.7 66.6				Impervious 5 m 211.0 m 210.9 m 2.0 % Flat		

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.21	n.a.
	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.48	
	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.26	
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	64.7	61.0
	B	74	65	61	58	50	85	98	77.7	61.0
	B	74	65	61	58	50	85	98	66.6	59.6
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.5	5.3

Time of Concentration ⁶	
Total Length	45 m
Average Slope	4.7 %
Airport Bransby - Williams	10.4 min. 1.8 min. Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	10.1 min. 0.17 hr.

Composite Parameters	
Drainage Area	1.48 ha
Runoff Coefficient	0.31
SCS Curve No.	69.5 60.8
Modified Curve No. ⁴ , CN*	70.8 60.7
Initial Abstraction.	4.5 5.3

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for PR-200			Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22		

Land Use			Rainfall Data																													
<table border="1"> <thead> <tr> <th></th> <th>Internal</th> <th>External</th> </tr> </thead> <tbody> <tr> <td>Agriculture</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Range</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Grass</td> <td>0.20</td> <td>ha</td> </tr> <tr> <td>Woods</td> <td>0.43</td> <td>ha</td> </tr> <tr> <td>Wetland</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Gravel</td> <td>0.00</td> <td>ha</td> </tr> <tr> <td>Impervious</td> <td>0.12</td> <td>ha</td> </tr> <tr> <td>SUM</td> <td>0.75</td> <td></td> </tr> </tbody> </table>				Internal	External	Agriculture	0.00	ha	Range	0.00	ha	Grass	0.20	ha	Woods	0.43	ha	Wetland	0.00	ha	Gravel	0.00	ha	Impervious	0.12	ha	SUM	0.75		Gauging Station = Peterborough 12 hr, 100 Yr Rainfall = 90.4 mm		
	Internal	External																														
Agriculture	0.00	ha																														
Range	0.00	ha																														
Grass	0.20	ha																														
Woods	0.43	ha																														
Wetland	0.00	ha																														
Gravel	0.00	ha																														
Impervious	0.12	ha																														
SUM	0.75																															
			Drainage Area 0.75 ha Impervious Area 0.12 ha Percent Impervious 16.1% Connected Impervious 16.1%																													
<table border="1"> <thead> <tr> <th>Hydrologic Soil Group¹</th> <th>B</th> </tr> <tr> <th>Soil Type</th> <th>0</th> </tr> <tr> <th>C</th> <th>0.36</th> </tr> <tr> <th>CN (Nashyd)</th> <th>65.2</th> </tr> </thead> </table>			Hydrologic Soil Group ¹	B	Soil Type	0	C	0.36	CN (Nashyd)	65.2	<table border="1"> <thead> <tr> <th>Pervious</th> <th>Impervious</th> </tr> </thead> <tbody> <tr> <td>Length 130</td> <td>8 m</td> </tr> <tr> <td>US Elev 225.9</td> <td>210.0 m</td> </tr> <tr> <td>DS Elev 211.6</td> <td>209.8 m</td> </tr> <tr> <td>Slope 11.0</td> <td>2.0 %</td> </tr> <tr> <td>Steep</td> <td>Flat</td> </tr> </tbody> </table>			Pervious	Impervious	Length 130	8 m	US Elev 225.9	210.0 m	DS Elev 211.6	209.8 m	Slope 11.0	2.0 %	Steep	Flat							
Hydrologic Soil Group ¹	B																															
Soil Type	0																															
C	0.36																															
CN (Nashyd)	65.2																															
Pervious	Impervious																															
Length 130	8 m																															
US Elev 225.9	210.0 m																															
DS Elev 211.6	209.8 m																															
Slope 11.0	2.0 %																															
Steep	Flat																															

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.57	0.35	0.19	0.29	0.05	0.76	0.90	0.36	n.a.
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	65.2	59.0
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	7.4	8.4

Time of Concentration ⁶	
Total Length	138 m
Average Slope	10.5 %
Airport Bransby - Williams	13.0 min. 5.1 min.
	Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	10.1 min. 0.17 hr.

Composite Parameters	
Drainage Area	0.75 ha
Runoff Coefficient	0.36
SCS Curve No.	65.2 59.0
Modified Curve No. ⁴ , CN*	68.1 61.7
Initial Abstraction.	7.4 8.4

Notes:

1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for PR-201

Sheet 1 of 1



Project No: 19-10874
Project Name: Life at the Woodland
Designed/Checked By: RC/CPB
Date: 22-Feb-22

Land Use						Rainfall Data			
	Controlled Lots	Controlled Roadway	External		Gauging Station = Peterborough				
	Agriculture	0.00	0.00		ha				12 hr, 100 Yr Rainfall = 90.4 mm
	Range	0.00	0.00		ha				
	Grass	0.41	0.30		ha				
	Woods	0.00	0.00		ha				
	Wetland	0.00	0.00		ha				
	Gravel	0.00	0.00		ha				
	Impervious	0.05	0.25		ha				
SUM	0.46	0.55	0.26						
Hydrologic Soil Group¹	B	B	B						
Soil Type	0	0	0						
CN (Nashyd)	0.26	0.51	0.34						
CN (Nashyd)	64.7	77.7	67.3						
Pervious						Length	100	m	
						US Elev	213.2	m	
						DS Elev	206.6	m	
						Slope	6.6	%	
						Hilly			

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.26	n.a.
	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.51	
	B	0.40	0.30	0.19	0.14	0.05	0.76	0.90	0.34	
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	64.7	61.0
	B	74	65	61	58	50	85	98	77.7	61.0
	B	74	65	61	58	50	85	98	67.3	65.0
Initial Abstraction⁵, mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.8	5.8

Time of Concentration ⁶	
Total Length	100 m
Average Slope	6.6 %
Airport Bransby - Williams	12.5 min. 3.8 min.
	Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	10.1 min. 0.17 hr.

Composite Parameters	
Drainage Area	1.28 ha
Runoff Coefficient	0.39
SCS Curve No.	70.9 62.0
Modified Curve No. ⁴ , CN*	72.2 62.5
Initial Abstraction.	4.8 5.8

Notes:

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for $C \leq 0.4$, and Bransby-Williams for $C > 0.4$.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for PR-300				Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22			

Land Use			Rainfall Data		
Internal			Gauging Station = Peterborough		
Agriculture 0.00 ha Range 3.90 ha Grass 0.99 ha Woods 3.47 ha Wetland 0.00 ha Gravel 0.00 ha Impervious 0.14 ha SUM 8.50			12 hr, 100 Yr Rainfall = 90.4 mm		
			Drainage Area 8.50 ha	Impervious Area 0.14 ha	Percent Impervious 1.6%
			Connected Impervious 1.6%		
Pervious			Length 330 m		
Hydrologic Soil Group ¹ B			US Elev 213.5 m		
Soil Type 0			DS Elev 200.9 m		
C 0.18			Slope 3.8 %		
CN (Nashyd) 62.2			Rolling		

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.18	n.a.
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	62.2	61.6
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	8.4	8.5

Time of Concentration ⁶	
Total Length	330 m
Average Slope	3.8 %
Airport Bransby - Williams	35.2 min. 11.6 min. Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	23.6 min. 0.39 hr.

Composite Parameters	
Drainage Area	8.50 ha
Runoff Coefficient	0.18
SCS Curve No.	62.2 61.6
Modified Curve No. ⁴ , CN*	64.4 63.7
Initial Abstraction.	8.4 8.5

Notes:

- Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
- Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
- SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
- The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
- Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
- Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
- Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
- All impervious areas have been assumed to be directly connected.

Hydrologic Parameters for PR-400			Sheet 1 of 1
	Project No: 19-10874 Project Name: Life at the Woodland Designed/Checked By: RC/CPB Date: 22-Feb-22		

Land Use			Rainfall Data		
Internal			Gauging Station = Peterborough		
Agriculture 0.00 ha Range 0.00 ha Grass 0.51 ha Woods 0.00 ha Wetland 0.00 ha Gravel 0.00 ha Impervious 0.07 ha SUM 0.58			12 hr, 100 Yr Rainfall = 90.4 mm		
			Drainage Area 0.58 ha Impervious Area 0.07 ha Percent Impervious 12.1% Connected Impervious 12.1%		
Hydrologic Soil Group¹ B Soil Type 0 C 0.22 CN (Nashyd) 65.5			Pervious Length 165 m US Elev 211.6 m DS Elev 204.8 m Slope 4.1 % Rolling		

Parameter	Soil Group	Land Use							Weighted Value	
		Agriculture	Range	Grass	Woods	Wetland	Gravel	Imperv.	Incl. Imperv. NASHYD	Not Incl. Imperv. STANDHYD
Runoff Coefficient ² , C	B	0.32	0.22	0.13	0.11	0.05	0.76	0.90	0.22	n.a.
SCS Curve No. ³ , CN	B	74	65	61	58	50	85	98	65.5	61.0
Initial Abstraction ⁵ , mm		6.0	8.0	5.0	10.0	10.0	2.5	2.0	4.6	5.0

Time of Concentration ⁶	
Total Length	165 m
Average Slope	4.1 %
Airport Bransby - Williams	23.0 min. 7.5 min. Flat: 0-2% Slopes Rolling: 2-6% Slopes Hilly: >6% Slopes
Applicable Minimum ⁷	15.0 min.
Time to Peak	15.4 min. 0.26 hr.

Composite Parameters		
Drainage Area	0.58 ha	
Runoff Coefficient	0.22	
SCS Curve No.	65.5	61.0
Modified Curve No. ⁴ , CN*	66.1	60.5
Initial Abstraction.	4.6	5.0

Notes:

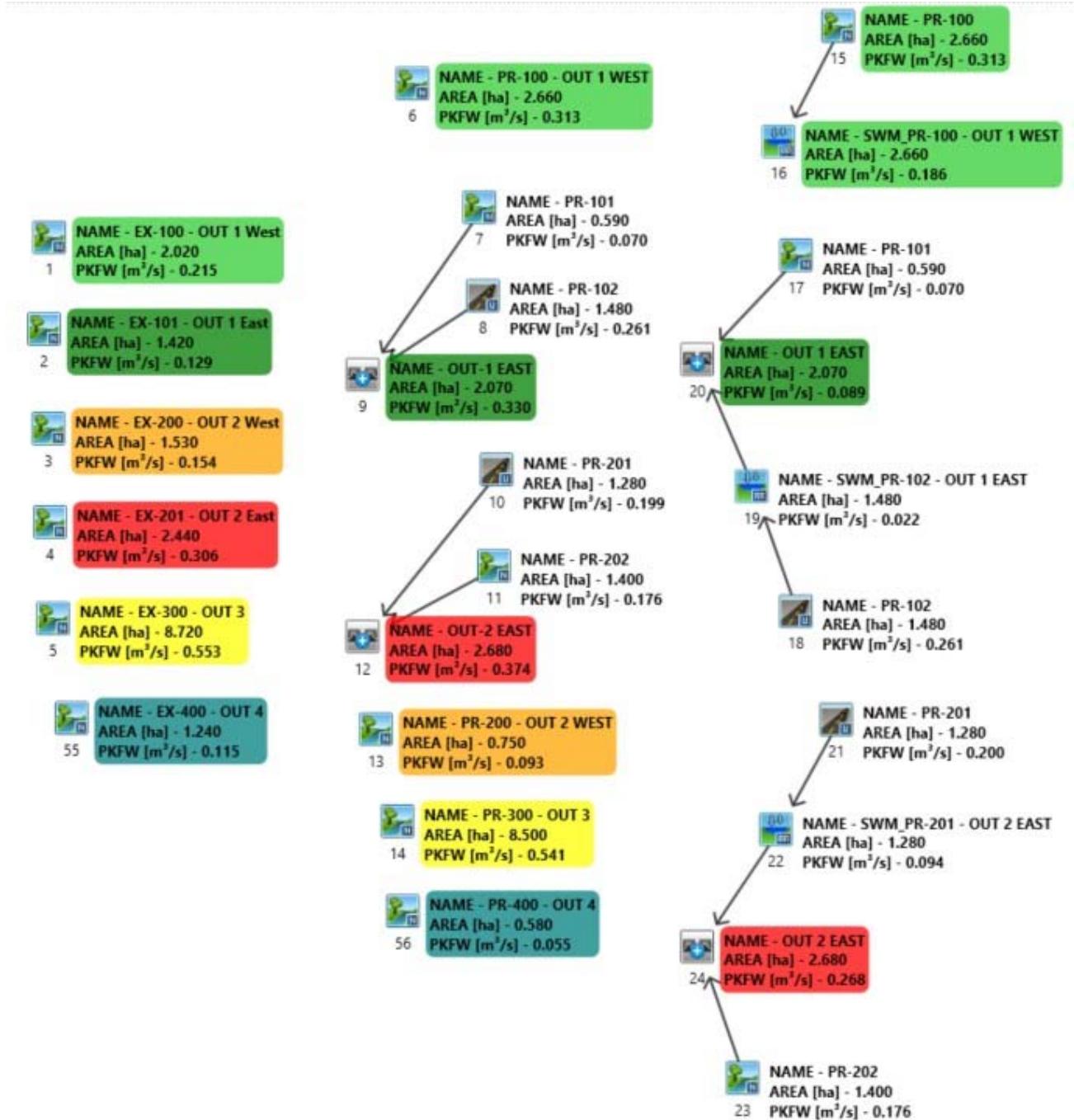
1. Hydrologic Soil Group obtained from Design Chart H2-6A, M.T.O. Drainage Manual, 1980.
2. Runoff coefficient obtained from M.T.O. Design Chart 1.07, M.T.O. Drainage Management Manual, 1997, Hydrologic Analysis and Design, McCuen 2004 and New Jersey Technical Manual for Stream Encroachment, 1984.
3. SCS Curve No. obtained from M.T.O. Design Chart 1.09, M.T.O. Drainage Management Manual, 1997, and Table 2-2a, TR-55, page 2-5.
4. The modified curve number is adjusted as per Paul Wisner & Associates (1982) and represents antecedent moisture conditions Type II
5. Initial Abstraction values taken from the Environmental and Engineering Services Department, The Corporation of the City of London, Dec 2005
6. Use Airport Equation to calculate time of concentration for C <= 0.4, and Bransby-Williams for C > 0.4.
7. Minimum Time of Concentration for use in the Rational Method and Hydrologic Model has been set to 15 minutes
8. All impervious areas have been assumed to be directly connected.

Appendix B

Hydrologic Modelling



VO3 Analysis



----- (cms) (ha.m.) | (cms)
 (ha.m.)
 **** WARNING : FIRST OUTFLOW IS NOT ZERO.
 0.0001 0.0072 | 0.1306
 0.0171
 0.0194 0.0065 0.0083 | 0.1492
 0.0220 0.0242 0.0096 | 0.1656
 0.0248 0.0501 0.0112 | 0.1806
 0.0278 0.0806 0.0129 | 0.1944
 0.0000 0.1098 0.0149 | 0.0000
 R.V. AREA QPEAK TPEAK
 (mm) (ha) (cms) (hrs)
 INFLOW : ID= 2 (0015) 2.660 0.063 3.08
 6.68 OUTFLOW: ID= 1 (0016) 2.660 0.020 3.58
 3.97
 PEAK FLOW REDUCTION [Qout/Qin](%)= 31.42
 TIME SHIFT OF PEAK FLOW (min)= 30.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0093

 | CALIB | NASHYD (0004) | Area (ha)= 2.44 Curve Number
 (CN)= 68.8 | ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear
 Res.(N)= 3.00 ----- U.H. Tp(hrs)= 0.17
 Unit Hyd Qpeak (cms)= 0.548
 PEAK FLOW (cms)= 0.056 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 6.456
 TOTAL RAINFALL (mm)= 38.750
 RUNOFF COEFFICIENT = 0.167

 | STANDHYD (0008) | Area (ha)= 1.48
 | ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00

 IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 0.34 1.14
 Dep. Storage (mm)= 1.00 5.30
 Average Slope (%)= 2.00 5.00
 Length (m)= 99.33 40.00
 Mannings n = 0.013 0.250
 Max.Eff.Inten.(mm/hr)= 60.40 9.81
 over (min) 5.00 20.00
 Storage Coeff. (min)= 2.53 (iii) 16.10 (ii)
 Unit Hyd. Tpeak (min)= 5.00 20.00
 Unit Hyd. peak (cms)= 0.29 0.06
 TOTALS
 PEAK FLOW (cms)= 0.06 0.02
 0.067 (iii)
 TIME TO PEAK (hrs)= 3.00 3.25
 3.00
 RUNOFF VOLUME (mm)= 37.75 5.65
 13.03
 TOTAL RAINFALL (mm)= 38.75 38.75
 38.75
 RUNOFF COEFFICIENT = 0.97 0.15
 0.34
 ***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | ADD HYD (0009) | AREA QPEAK TPEAK R.V.
 | 1 + 2 = 3 | (ha) (cms) (hrs) (mm)
 ID1= 1 (0007): 0.59 0.014 3.08 6.76
 + ID2= 2 (0008): 1.48 0.067 3.00 13.03
 ======
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB | NASHYD (0003) | Area (ha)= 1.53 Curve Number
 (CN)= 61.7 | ID= 1 DT= 5.0 min | Ia (mm)= 8.70 # of Linear
 Res.(N)= 3.00 ----- U.H. Tp(hrs)= 0.17
 Unit Hyd Qpeak (cms)= 0.344
 PEAK FLOW (cms)= 0.025 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 4.793
 TOTAL RAINFALL (mm)= 38.750
 RUNOFF COEFFICIENT = 0.124
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB | NASHYD (0007) | Area (ha)= 0.59 Curve Number
 (CN)= 65.0 | ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear
 Res.(N)= 3.00 ----- U.H. Tp(hrs)= 0.17
 Unit Hyd Qpeak (cms)= 0.133
 PEAK FLOW (cms)= 0.014 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 6.762
 TOTAL RAINFALL (mm)= 38.750
 RUNOFF COEFFICIENT = 0.175
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 ID = 3 (0009): 2.07 0.081 3.00 11.24
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 | STANDHYD (0011) | Area (ha)= 1.40 Curve Number
 (CN)= 67.1 | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
 Res.(N)= 3.00 ----- U.H. Tp(hrs)= 0.17
 Unit Hyd Qpeak (cms)= 0.315
 PEAK FLOW (cms)= 0.037 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 7.323
 TOTAL RAINFALL (mm)= 38.750
 RUNOFF COEFFICIENT = 0.189
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB | STANDHYD (0010) | Area (ha)= 1.28
 | ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.(%)= 24.60

 IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 0.31 0.97
 Dep. Storage (mm)= 1.00 5.80
 Average Slope (%)= 1.00 6.60
 Length (m)= 92.38 100.00
 Mannings n = 0.013 0.250
 Max.Eff.Inten.(mm/hr)= 60.40 6.94
 over (min) 5.00 30.00
 Storage Coeff. (min)= 2.98 (ii) 27.82 (ii)
 Unit Hyd. Tpeak (min)= 5.00 30.00
 Unit Hyd. peak (cms)= 0.28 0.04
 TOTALS

 | ADD HYD (0009) |
 | 1 + 2 = 3 |
 | AREA QPEAK TPEAK R.V.
 | (ha) (cms) (hrs) (mm)
 ID1= 1 (0007): 0.59 0.014 3.08 6.76
 + ID2= 2 (0008): 1.48 0.067 3.00 13.03
 ======

PEAK FLOW (cms) = 0.05 0.01
 0.056 (iii)
 TIME TO PEAK (hrs) = 3.00 3.42
 3.00
 RUNOFF VOLUME (mm) = 37.75 5.86
 13.69
 TOTAL RAINFALL (mm) = 38.75 38.75
 38.75
 RUNOFF COEFFICIENT = 0.97 0.15
 0.35

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 CN* = 62.5 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0012)
 1 + 2 = 3 | AREA QPEAK TPEAK R.V.
 --- (ha) (cms) (hrs) (mm)
 ID1= 1 (0010): 1.28 0.056 3.00 13.69
 + ID2= 2 (0011): 1.40 0.037 3.08 7.32
 ID = 3 (0012): 2.68 0.092 3.00 10.36

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
 NASHYD (0005) | Area (ha) = 8.72 Curve Number
 (CN)= 64.6
 | ID= 1 DT= 5.0 min | Ia (mm) = 8.80 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms) = 0.854
 PEAK FLOW (cms) = 0.089 (i)
 TIME TO PEAK (hrs) = 3.333

CALIB
 NASHYD (0013) | Area (ha) = 0.75 Curve Number
 (CN)= 68.1
 | ID= 1 DT= 5.0 min | Ia (mm) = 7.40 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms) = 0.169
 PEAK FLOW (cms) = 0.017 (i)
 TIME TO PEAK (hrs) = 3.083
 RUNOFF VOLUME (mm) = 6.514
 TOTAL RAINFALL (mm) = 38.750
 RUNOFF COEFFICIENT = 0.168

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 NASHYD (0017) | Area (ha) = 0.59 Curve Number
 (CN)= 65.0
 | ID= 1 DT= 5.0 min | Ia (mm) = 4.70 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms) = 0.133
 PEAK FLOW (cms) = 0.014 (i)
 TIME TO PEAK (hrs) = 3.083
 RUNOFF VOLUME (mm) = 6.762
 TOTAL RAINFALL (mm) = 38.750
 RUNOFF COEFFICIENT = 0.175

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0018) | Area (ha) = 1.48
 | ID= 1 DT= 5.0 min | Total Imp(%) = 23.00 Dir. Conn.(%) =
 23.00

RUNOFF VOLUME (mm) = 5.303
 TOTAL RAINFALL (mm) = 38.750
 RUNOFF COEFFICIENT = 0.137

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB
 | NASHYD (0014) | Area (ha) = 8.50 Curve Number
 (CN)= 64.4
 | ID= 1 DT= 5.0 min | Ia (mm) = 8.40 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms) = 0.832
 PEAK FLOW (cms) = 0.089 (i)
 TIME TO PEAK (hrs) = 3.333
 RUNOFF VOLUME (mm) = 5.393
 TOTAL RAINFALL (mm) = 38.750
 RUNOFF COEFFICIENT = 0.139

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB
 | NASHYD (0006) | Area (ha) = 2.66 Curve Number
 (CN)= 64.8
 | ID= 1 DT= 5.0 min | Ia (mm) = 4.80 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms) = 0.598
 PEAK FLOW (cms) = 0.063 (i)
 TIME TO PEAK (hrs) = 3.083
 RUNOFF VOLUME (mm) = 6.680
 TOTAL RAINFALL (mm) = 38.750
 RUNOFF COEFFICIENT = 0.172

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

IMPERVIOUS PERVERIOUS (i)

Surface Area (ha) =	0.34	1.14
Dep. Storage (mm) =	1.00	5.30
Average Slope (%) =	2.00	5.00
Length (m) =	99.33	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr) =		60.40 9.81
over (min) =		5.00 20.00
Storage Coeff. (min) =		2.53 (ii) 16.10 (ii)
Unit Hyd. Tpeak (min) =		5.00 20.00
Unit Hyd. peak (cms) =		0.29 0.06

TOTALS
 PEAK FLOW (cms) = 0.06 0.02
 0.067 (iii)
 TIME TO PEAK (hrs) = 3.00 3.25
 3.00
 RUNOFF VOLUME (mm) = 37.75 5.65
 13.03
 TOTAL RAINFALL (mm) = 38.75 38.75
 38.75
 RUNOFF COEFFICIENT = 0.97 0.15
 0.34

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR (0019) |
 | IN= 2--> OUT= 1 |
 | DT= 5.0 min |
 STORAGE
 ----- (cms) (ha.m.) (cms)
 (ha.m.)

**** WARNING : FIRST OUTFLOW IS NOT ZERO.
 0.0001 0.0074 | 0.0165
 0.0238

0.0280	0.0045	0.0089		0.0180	
0.0326	0.0084	0.0111		0.0193	
0.0376	0.0110	0.0137		0.0206	
0.0435	0.0131	0.0166		0.0218	
0.0000	0.0149	0.0200		0.0000	

R.V.	AREA	QPEAK	TPEAK		
(mm)	(ha)	(cms)	(hrs)		
13.03	INFLOW : ID= 2 (0018)	1.480	0.067	3.00	
8.00	OUTFLOW: ID= 1 (0019)	1.480	0.010	3.83	
PEAK FLOW REDUCTION [Qout/Qin](%) = 14.63 TIME SHIFT OF PEAK FLOW (min) = 50.00 MAXIMUM STORAGE USED (ha.m.) =					
0.0125	-----				
ADD HYD (0020) 1 + 2 = 3 AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) ID1= 1 (0017): 0.59 0.014 3.08 6.76 + ID2= 2 (0019): 1.48 0.010 3.83 8.00 ===== ID = 3 (0020): 2.07 0.020 3.08 7.65					
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.					

CALIB NASHYD (0023) Area (ha)= 1.40 Curve Number (CN)= 67.1 ID= 1 DT= 5.0 min Ia (mm)= 4.60 # of Linear Res.(N)= 3.00					
***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!					

(i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES: CN* = 62.5 Ia = Dep. Storage (Above)					
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.					
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.					

RESERVOIR (0022) IN= 2---> OUT= 1 OUTFLOW STORAGE OUTFLOW DT= 5.0 min (cms) (ha.m.) (cms) ===== **** WARNING : FIRST OUTFLOW IS NOT ZERO. 0.0001 0.0052 0.0843					
0.0172	0.0056	0.0066		0.0945	
0.0200	0.0202	0.0082		0.1036	
0.0231	0.0402	0.0101		0.1121	
0.0265	0.0595	0.0122		0.1199	
0.0301	0.0728	0.0146		0.0000	
0.0000					
R.V.	AREA	QPEAK	TPEAK		
(mm)	(ha)	(cms)	(hrs)		
13.82	INFLOW : ID= 2 (0021)	1.280	0.057	3.00	
9.73	OUTFLOW: ID= 1 (0022)	1.280	0.019	3.08	
0.0081	PEAK FLOW REDUCTION [Qout/Qin](%) = 33.86 TIME SHIFT OF PEAK FLOW (min) = 5.00 MAXIMUM STORAGE USED (ha.m.) =				

CALIB NASHYD (0056) Area (ha)= 0.58 Curve Number (CN)= 66.1 ID= 1 DT= 5.0 min Ia (mm)= 4.60 # of Linear Res.(N)= 3.00					
U.H. Tp(hrs)= 0.26					
Unit Hyd Qpeak (cms)= 0.085 PEAK FLOW (cms)= 0.011 (i) TIME TO PEAK (hrs)= 3.167 RUNOFF VOLUME (mm)= 7.087 TOTAL RAINFALL (mm)= 38.750 RUNOFF COEFFICIENT = 0.183					

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME
STEP.

** SIMULATION NUMBER: 2 **

| READ STORM | Filename: C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-f4b8f2008cel\fcd4f25c |
| Pttotal= 52.45 mm | Comments: 5-Year, 6 hour SCS Type II - Peterboroug

TIME RAIN TIME RAIN |' TIME RAIN |
hrs mm/hr hrs mm/hr |' hrs mm/hr |
4.75 3.20 0.25 2.10 | 1.75 5.20 | 3.25 11.50 |
5.00 3.20 0.50 2.10 | 2.00 5.20 | 3.50 11.50 |
5.25 2.10 0.75 3.20 | 2.25 6.30 | 3.75 5.20 |
5.50 2.10 1.00 3.20 | 2.50 6.30 | 4.00 5.20 |
5.75 2.10 1.25 3.20 | 2.75 31.40 | 4.25 4.20 |
6.00 2.10 1.50 3.20 | 3.00 81.80 | 4.50 4.20 |

| CALIB |
| NASHYD (0002) | Area (ha)= 1.42 Curve Number
(CN)= 63.1
| ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hr)= 0.22

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN TIME RAIN |' TIME RAIN |
hrs mm/hr hrs mm/hr |' hrs mm/hr |
4.58 3.20 0.083 2.10 | 1.583 5.20 | 3.083 11.50 |
4.67 3.20 0.167 2.10 | 1.667 5.20 | 3.167 11.50 |
4.75 3.20 0.250 2.10 | 1.750 5.20 | 3.250 11.50 |
4.83 3.20 0.333 2.10 | 1.833 5.20 | 3.333 11.50 |
4.92 3.20 0.417 2.10 | 1.917 5.20 | 3.417 11.50 |
5.00 3.20 0.500 2.10 | 2.000 5.20 | 3.500 11.50 |
5.08 2.10 0.583 3.20 | 2.083 6.30 | 3.583 5.20 |
5.17 2.10 0.667 3.20 | 2.167 6.30 | 3.667 5.20 |
5.25 2.10 0.750 3.20 | 2.250 6.30 | 3.750 5.20 |
5.33 2.10 0.833 3.20 | 2.333 6.30 | 3.833 5.20 |
5.42 2.10 0.917 3.20 | 2.417 6.30 | 3.917 5.20 |
5.50 2.10 1.000 3.20 | 2.500 6.30 | 4.000 5.20 |
5.58 2.10 1.083 3.20 | 2.583 31.40 | 4.083 4.20 |
5.67 2.10 1.167 3.20 | 2.667 31.40 | 4.167 4.20 |
5.75 2.10 1.250 3.20 | 2.750 31.40 | 4.250 4.20 |
5.83 2.10 1.333 3.20 | 2.833 81.80 | 4.333 4.20 |
5.92 2.10 1.417 3.20 | 2.917 81.80 | 4.417 4.20 |
6.00 2.10 1.500 3.20 | 3.000 81.80 | 4.500 4.20 |

Unit Hyd Qpeak (cms)= 0.247

PEAK FLOW (cms)= 0.042 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 9.780
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.186

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |
| NASHYD (0001) | Area (ha)= 2.02 Curve Number
(CN)= 61.5
| ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hr)= 0.17

Unit Hyd Qpeak (cms)= 0.454

PEAK FLOW (cms)= 0.078 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 10.745
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.205

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |
| NASHYD (0015) | Area (ha)= 2.66 Curve Number
(CN)= 64.8
| ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hr)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.117 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 12.188
TOTAL RAINFALL (mm)= 52.450
RUNOFF COEFFICIENT = 0.232

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR (0016) |
| IN= 2--> OUT= 1 |
| DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW
STORAGE

(ha.m.) **** WARNING : FIRST OUTFLOW IS NOT ZERO.
0.0171 0.0001 0.0072 | 0.1306
0.0194 0.0065 0.0083 | 0.1492
0.0220 0.0242 0.0096 | 0.1656
0.0248 0.0501 0.0112 | 0.1806
0.0278 0.0806 0.0129 | 0.1944
0.0000 0.1098 0.0149 | 0.0000
----- AREA QPEAK TPEAK
R.V.
(mm) INFLOW : ID= 2 (0015) 2.660 0.117 3.08
12.19 OUTFLOW: ID= 1 (0016) 2.660 0.068 3.25
9.47

PEAK FLOW REDUCTION [Qout/Qin](%)= 58.45
TIME SHIFT OF PEAK FLOW (min)= 10.00
MAXIMUM STORAGE USED (ha.m.)= 0.0123

| CALIB |
| NASHYD (0004) | Area (ha)= 2.44 Curve Number
(CN)= 68.8
| ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear
Res.(N)= 3.00

----- U.H. Tp(hr)= 0.17
 Unit Hyd Qpeak (cms)= 0.548
 PEAK FLOW (cms)= 0.110 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 12.333
 TOTAL RAINFALL (mm)= 52.450
 RUNOFF COEFFICIENT = 0.235
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | STANDHYD (0008) | Area (ha)= 1.48
 | NASHYD (0003) | ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.(%)= 23.00

IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 0.34 1.14
 Dep. Storage (mm)= 1.00 5.30
 Average Slope (%)= 2.00 5.00
 Length (m)= 99.33 40.00
 Mannings n = 0.013 0.250
 Max.Eff.Inten.(mm/hr)= 81.80 18.50
 over (min) 5.00 15.00
 Storage Coeff. (min)= 2.24 (ii) 12.77 (ii)
 Unit Hyd. Tpeak (min)= 5.00 15.00
 Unit Hyd. peak (cms)= 0.30 0.08
 TOTALS
 PEAK FLOW (cms)= 0.08 0.04
 0.107 (iii)
 TIME TO PEAK (hrs)= 3.00 3.08
 3.00
 RUNOFF VOLUME (mm)= 51.45 10.51
 19.92
 TOTAL RAINFALL (mm)= 52.45 52.45
 52.45
 RUNOFF COEFFICIENT = 0.98 0.20
 0.38
 ***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | STANDHYD (0007) | Area (ha)= 0.59 Curve Number
 | NASHYD (0003) | ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear
 Res.(N)= 3.00

U.H. Tp(hr)= 0.17
 Unit Hyd Qpeak (cms)= 0.133
 PEAK FLOW (cms)= 0.026 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 12.312

ADD HYD (0009)
 1 + 2 = 3 AREA QPEAK TPEAK R.V.
 (ha) (cms) (hrs) (mm)
 ID1= 1 (0007): 0.59 0.026 3.08 12.31
 + ID2= 2 (0008): 1.48 0.107 3.00 19.92
 ======
 ID = 3 (0009): 2.07 0.133 3.00 17.75
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB | STANDHYD (0011) | Area (ha)= 1.40 Curve Number
 | NASHYD (0011) | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
 Res.(N)= 3.00

U.H. Tp(hr)= 0.17
 Unit Hyd Qpeak (cms)= 0.315
 PEAK FLOW (cms)= 0.067 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 13.234
 TOTAL RAINFALL (mm)= 52.450
 RUNOFF COEFFICIENT = 0.252
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0012)
 1 + 2 = 3 AREA QPEAK TPEAK R.V.
 (ha) (cms) (hrs) (mm)
 ID1= 1 (0010): 1.28 0.083 3.00 20.89
 + ID2= 2 (0011): 1.40 0.067 3.08 13.23
 ======
 ID = 3 (0012): 2.68 0.149 3.00 16.89
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB | STANDHYD (0010) | Area (ha)= 1.28
 | ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.(%)= 24.60

IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 0.31 0.97
 Dep. Storage (mm)= 1.00 5.80
 Average Slope (%)= 1.00 6.60
 Length (m)= 92.38 100.00
 | CALIB |

| NASHYD (0005) | Area (ha)= 8.72 Curve Number
 (CN)= 64.6 | Ia (mm)= 8.80 # of Linear
 ID= 1 DT= 5.0 min | Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.854

PEAK FLOW (cms)= 0.184 (i)
 TIME TO PEAK (hrs)= 3.333
 RUNOFF VOLUME (mm)= 10.419
 TOTAL RAINFALL (mm)= 52.450
 RUNOFF COEFFICIENT = 0.199

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0014) | Area (ha)= 8.50 Curve Number
 (CN)= 64.4 | Ia (mm)= 8.40 # of Linear
 ID= 1 DT= 5.0 min | Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.832

PEAK FLOW (cms)= 0.182 (i)
 TIME TO PEAK (hrs)= 3.333
 RUNOFF VOLUME (mm)= 10.518
 TOTAL RAINFALL (mm)= 52.450
 RUNOFF COEFFICIENT = 0.201

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0006) | Area (ha)= 2.66 Curve Number
 (CN)= 64.8 | Ia (mm)= 4.80 # of Linear
 ID= 1 DT= 5.0 min | Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.117 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 12.188
 TOTAL RAINFALL (mm)= 52.450
 RUNOFF COEFFICIENT = 0.232

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0013) | Area (ha)= 0.75 Curve Number
 (CN)= 68.1 | Ia (mm)= 7.40 # of Linear
 ID= 1 DT= 5.0 min | Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.169

PEAK FLOW (cms)= 0.034 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 12.328
 TOTAL RAINFALL (mm)= 52.450
 RUNOFF COEFFICIENT = 0.235

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0017) | Area (ha)= 0.59 Curve Number
 (CN)= 65.0 | Ia (mm)= 4.70 # of Linear
 ID= 1 DT= 5.0 min | Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.026 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 12.312
 TOTAL RAINFALL (mm)= 52.450
 RUNOFF COEFFICIENT = 0.235

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | STANDHYD (0018) | Area (ha)= 1.48
 | ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn. (%)= 23.00

 IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 0.34 1.14
 Dep. Storage (mm)= 1.00 5.30
 Average Slope (%)= 2.00 5.00
 Length (m)= 99.33 40.00
 Mannings n = 0.013 0.250
 Max.Eff.Inten.(mm/hr)= 81.80 18.50
 over (min) 5.00 15.00
 Storage Coeff. (min)= 2.24 (ii) 12.77 (ii)
 Unit Hyd. Tpeak (min)= 5.00 15.00
 Unit Hyd. peak (cms)= 0.30 0.08
 TOTALS
 PEAK FLOW (cms)= 0.08 0.04
 0.107 (iii)
 TIME TO PEAK (hrs)= 3.00 3.08
 3.00
 RUNOFF VOLUME (mm)= 51.45 10.51
 19.92
 TOTAL RAINFALL (mm)= 52.45 52.45
 52.45
 RUNOFF COEFFICIENT = 0.98 0.20
 0.38

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | IN= 2 ---> OUT= 1 | OUTFLOW STORAGE | OUTFLOW
 DT= 5.0 min | (cms) (ha.m.) | (cms)
 ----- (ha.m.)
 ***** WARNING : FIRST OUTFLOW IS NOT ZERO.
 0.0238 0.0001 0.0074 | 0.0165
 0.0280 0.0045 0.0089 | 0.0180
 0.0326 0.0084 0.0111 | 0.0193
 0.0376 0.0110 0.0137 | 0.0206
 0.0435 0.0131 0.0166 | 0.0218
 0.0000 0.0149 0.0200 | 0.0000

 R.V. AREA QPEAK TPEAK
 (mm) (ha) (cms) (hrs)
 INFLOW : ID= 2 (0018) 1.480 0.107 3.00
 19.92 OUTFLOW: ID= 1 (0019) 1.480 0.014 3.83
 14.89

 PEAK FLOW REDUCTION [Qout/Qin](%)= 13.40
 TIME SHIFT OF PEAK FLOW (min)= 50.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0190

 | ADD HYD (0020) | AREA QPEAK TPEAK R.V.
 | 1 + 2 = 3 | (ha) (cms) (hrs) (mm)
 | ID1= 1 (0017): 0.59 0.026 3.08 12.31
+ ID2= 2 (0019): 1.48 0.014 3.83 14.89
ID = 3 (0020): 2.07 0.038 3.08 14.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| RESERVOIR (0019) |

CALIB
 NASHYD (0023) | Area (ha) = 1.40 Curve Number
 (CN) = 67.1
 | ID= 1 DT= 5.0 min | Ia (mm) = 4.60 # of Linear
 Res.(N) = 3.00
 ----- U.H. Tp(hr)= 0.17

Unit Hyd Qpeak (cms) = 0.315

PEAK FLOW (cms) = 0.067 (i)

TIME TO PEAK (hrs) = 3.083

RUNOFF VOLUME (mm) = 13.234

TOTAL RAINFALL (mm) = 52.450

RUNOFF COEFFICIENT = 0.252

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0021) | Area (ha) = 1.28
 | ID= 1 DT= 5.0 min | Total Imp(%) = 25.00 Dir. Conn. (%) =
 25.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha) =	0.32	0.96
Dep. Storage (mm) =	1.00	5.80
Average Slope (%) =	1.00	6.60
Length (m) =	92.38	100.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr) =	81.80	15.49
over (min)	5.00	25.00
Storage Coeff. (min) =	2.64 (ii)	20.66 (ii)
Unit Hyd. Tpeak (min) =	5.00	25.00
Unit Hyd. peak (cms) =	0.29	0.05

TOTALS

PEAK FLOW (cms) = 0.07 0.02

0.084 (iii)

TIME TO PEAK (hrs) = 3.00 3.33

3.00

RUNOFF VOLUME (mm) = 51.45 10.93
 21.05
 TOTAL RAINFALL (mm) = 52.45 52.45
 52.45
 RUNOFF COEFFICIENT = 0.98 0.21
 0.40

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:

CN* = 62.5 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0022)
 IN= 2--> OUT= 1
 DT= 5.0 min

 STORAGE (ha.m.) OUTFLOW (cms) STORAGE (ha.m.) OUTFLOW (cms)
 0.0172 0.0056 0.0066 0.0945
 0.0200 0.0202 0.0082 0.1036
 0.0231 0.0402 0.0101 0.1121
 0.0265 0.0595 0.0122 0.1199
 0.0301 0.0728 0.0146 0.0000
 0.0000
 R.V. AREA QPEAK TPPEAK
 (ha) (cms) (hrs)
 1.280 0.084 3.00
 21.05 INFLOW : ID= 2 (0021) 1.280 0.084 3.00
 OUTFLOW: ID= 1 (0022) 1.280 0.043 3.08
 16.96

PEAK FLOW REDUCTION [Qout/Qin](%) = 50.74
 TIME SHIFT OF PEAK FLOW (min) = 5.00
 MAXIMUM STORAGE USED (ha.m) =

0.0105

----- U.H. Tp(hr)= 0.26

Unit Hyd Qpeak (cms) = 0.085

PEAK FLOW (cms) = 0.021 (i)

TIME TO PEAK (hrs) = 3.167

RUNOFF VOLUME (mm) = 12.845

TOTAL RAINFALL (mm) = 52.450

RUNOFF COEFFICIENT = 0.245

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 ** SIMULATION NUMBER: 3 **

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
 NASHYD (0055) | Area (ha) = 1.24 Curve Number
 (CN) = 67.5
 | ID= 1 DT= 5.0 min | Ia (mm) = 8.20 # of Linear
 Res.(N) = 3.00
 ----- U.H. Tp(hr)= 0.26

Unit Hyd Qpeak (cms) = 0.182

PEAK FLOW (cms) = 0.040 (i)

TIME TO PEAK (hrs) = 3.167

RUNOFF VOLUME (mm) = 11.748

TOTAL RAINFALL (mm) = 52.450

RUNOFF COEFFICIENT = 0.224

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 NASHYD (0056) | Area (ha) = 0.58 Curve Number
 (CN) = 66.1
 | ID= 1 DT= 5.0 min | Ia (mm) = 4.60 # of Linear
 Res.(N) = 3.00

READ STORM | Filename: C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-f4b8f2008cel\b881660d
 | Ptotal= 61.60 mm | Comments: 10-Year, 6 hour SCS Type II - Peterborou

TIME hrs	RAIN mm/hr	TIME hrs		TIME hrs		TIME hrs	
		RAIN mm/hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs
4.75	3.70	0.25	2.50 1.75	6.20 3.25	13.50		
5.00	3.70	0.50	2.50 2.00	6.20 3.50	13.50		
5.25	2.50	0.75	3.70 2.25	7.40 3.75	6.20		
5.50	2.50	1.00	3.70 2.50	7.40 4.00	6.20		
5.75	2.50	1.25	3.70 2.75	36.90 4.25	4.90		
6.00	2.50	1.50	3.70 3.00	95.90 4.50	4.90		

| CALIB |
| NASHYD (0002) | Area (ha)= 1.42 Curve Number
| (CN)= 63.1 |
| ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear
| Res.(N)= 3.00 |
----- U.H. Tp(hr)= 0.22

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME
STEP.

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN TIME RAIN |' TIME RAIN |
hrs mm/hr hrs mm/hr |' hrs mm/hr |
4.58 3.70 0.083 2.50 | 1.583 6.20 | 3.083 13.50 |
4.67 3.70 0.167 2.50 | 1.667 6.20 | 3.167 13.50 |
4.75 3.70 0.250 2.50 | 1.750 6.20 | 3.250 13.50 |
4.83 3.70 0.333 2.50 | 1.833 6.20 | 3.333 13.50 |
4.92 3.70 0.417 2.50 | 1.917 6.20 | 3.417 13.50 |
5.00 3.70 0.500 2.50 | 2.000 6.20 | 3.500 13.50 |
5.08 2.50 0.583 3.70 | 2.083 7.40 | 3.583 6.20 |
5.17 2.50 0.667 3.70 | 2.167 7.40 | 3.667 6.20 |
5.25 2.50 0.750 3.70 | 2.250 7.40 | 3.750 6.20 |
5.33 2.50 0.833 3.70 | 2.333 7.40 | 3.833 6.20 |
5.42 2.50 0.917 3.70 | 2.417 7.40 | 3.917 6.20 |
5.50 2.50 1.000 3.70 | 2.500 7.40 | 4.000 6.20 |
5.58 2.50 1.083 3.70 | 2.583 36.90 | 4.083 4.90 |
5.67 2.50 1.167 3.70 | 2.667 36.90 | 4.167 4.90 |
5.75 2.50 1.250 3.70 | 2.750 36.90 | 4.250 4.90 |

| CALIB |
| NASHYD (0001) | Area (ha)= 2.02 Curve Number
| (CN)= 61.5 |
| ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear
| Res.(N)= 3.00 |
----- U.H. Tp(hr)= 0.17

Unit Hyd Qpeak (cms)= 0.454

PEAK FLOW (cms)= 0.107 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 14.669
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.238

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |
| NASHYD (0015) | Area (ha)= 2.66 Curve Number
| (CN)= 64.8 |
| ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear
| Res.(N)= 3.00 |
----- U.H. Tp(hr)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.159 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 16.505
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.268

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR (0016) |
| IN= 2--> OUT= 1 |
| DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW
STORAGE
(ha.m.) (cms) (ha.m.) | (cms)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
0.0001 0.0072 | 0.1306
0.0171 0.0065 0.0083 | 0.1492
0.0194 0.0242 0.0096 | 0.1656
0.0220 0.0501 0.0112 | 0.1806
0.0248 0.0806 0.0129 | 0.1944
0.0278 0.1098 0.0149 | 0.0000
0.0000
R.V.
(mm)
INFLOW : ID= 2 (0015) 2.660 0.159 3.08
16.50 OUTFLOW: ID= 1 (0016) 2.660 0.104 3.25
13.79

PEAK FLOW REDUCTION [Qout/Qin](%)= 65.62
TIME SHIFT OF PEAK FLOW (min)= 10.00
MAXIMUM STORAGE USED (ha.m.)= 0.0146

| CALIB |
| NASHYD (0003) | Area (ha)= 1.53 Curve Number
| (CN)= 61.7 |
| ID= 1 DT= 5.0 min | Ia (mm)= 8.70 # of Linear
| Res.(N)= 3.00 |
----- U.H. Tp(hr)= 0.17

Unit Hyd Qpeak (cms)= 0.344

PEAK FLOW (cms)= 0.073 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 13.242
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.215

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |
| NASHYD (0007) | Area (ha)= 0.59 Curve Number
| (CN)= 65.0 |

| ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear
Res.(N) = 3.00

----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.035 (i)

TIME TO PEAK (hrs)= 3.083

RUNOFF VOLUME (mm)= 16.657

TOTAL RAINFALL (mm)= 61.600

RUNOFF COEFFICIENT = 0.270

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | STANDHYD (0008) | Area (ha)= 1.48
| ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn. (%)= 23.00

----- IMPERVIOUS PERVIOUS (i)

Surface Area (ha)= 0.34 1.14

Dep. Storage (mm)= 1.00 5.30

Average Slope (%)= 2.00 5.00

Length (m)= 99.33 40.00

Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 95.90 28.35

over (min) 5.00 15.00

Storage Coeff. (min)= 2.10 (ii) 10.98 (ii)

Unit Hyd. Tpeak (min)= 5.00 15.00

Unit Hyd. peak (cms)= 0.31 0.09

TOTALS

PEAK FLOW (cms)= 0.09 0.05

0.136 (iii)

TIME TO PEAK (hrs)= 3.00 3.08

3.00

RUNOFF VOLUME (mm)= 60.60 14.36

24.99

TOTAL RAINFALL (mm)= 61.60 61.60

61.60

RUNOFF COEFFICIENT = 0.98 0.23

0.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

CN* = 60.7 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0009) | AREA QPEAK TPEAK R.V.
| 1 + 2 = 3 | (ha) (cms) (hrs) (mm)

| ID1= 1 (0007): 0.59 0.035 3.08 16.66
+ ID2= 2 (0008): 1.48 0.136 3.00 24.99
=====
| ID = 3 (0009): 2.07 0.171 3.00 22.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB | NASHYD (0011) | Area (ha)= 1.40 Curve Number
(CN)= 67.1
| ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
Res.(N) = 3.00
----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms)= 0.090 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 17.833
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.289

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | STANDHYD (0010) | Area (ha)= 1.28

| ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn. (%)= 24.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

----- IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 0.31 0.97
Dep. Storage (mm)= 1.00 5.80
Average Slope (%)= 1.00 6.60
Length (m)= 92.38 100.00
Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 95.90 26.51
over (min) 5.00 20.00
Storage Coeff. (min)= 2.48 (ii) 17.02 (ii)
Unit Hyd. Tpeak (min)= 5.00 20.00
Unit Hyd. peak (cms)= 0.29 0.06

TOTALS

PEAK FLOW (cms)= 0.08 0.04

0.108 (iii)

TIME TO PEAK (hrs)= 3.00 3.17

3.00

RUNOFF VOLUME (mm)= 60.60 14.96

26.18

TOTAL RAINFALL (mm)= 61.60 61.60

61.60

RUNOFF COEFFICIENT = 0.98 0.24

0.42

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

CN* = 62.5 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | NASHYD (0005) | Area (ha)= 8.72 Curve Number
(CN)= 64.6
| ID= 1 DT= 5.0 min | Ia (mm)= 8.80 # of Linear
Res.(N) = 3.00
----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.854

PEAK FLOW (cms)= 0.261 (i)
TIME TO PEAK (hrs)= 3.333
RUNOFF VOLUME (mm)= 14.519
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.236

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | NASHYD (0014) | Area (ha)= 8.50 Curve Number
(CN)= 64.4
| ID= 1 DT= 5.0 min | Ia (mm)= 8.40 # of Linear
Res.(N) = 3.00
----- U.H. Tp(hrs)= 0.39

Unit Hyd Qpeak (cms)= 0.832

PEAK FLOW (cms)= 0.256 (i)
TIME TO PEAK (hrs)= 3.333
RUNOFF VOLUME (mm)= 14.616
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.237

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0012) | AREA QPEAK TPEAK R.V.
| 1 + 2 = 3 | (ha) (cms) (hrs) (mm)

| ID1= 1 (0010): 1.28 0.108 3.00 26.18
+ ID2= 2 (0011): 1.40 0.090 3.08 17.83
=====
| ID = 3 (0012): 2.68 0.196 3.00 21.82

| CALIB |

NASHYD (0006)	Area (ha)=	2.66	Curve Number
(CN)= 64.8	Ia (mm)=	4.80	# of Linear
ID= 1 DT= 5.0 min	Res.(N)=	3.00	

	U.H. Tp(hr)=	0.17	
Unit Hyd Qpeak (cms)=	0.598		
PEAK FLOW (cms)=	0.159 (i)		
TIME TO PEAK (hrs)=	3.083		
RUNOFF VOLUME (mm)=	16.505		
TOTAL RAINFALL (mm)=	61.600		
RUNOFF COEFFICIENT =	0.268		
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.			

CALIB			
NASHYD (0013)	Area (ha)=	0.75	Curve Number
(CN)= 68.1	Ia (mm)=	7.40	# of Linear
ID= 1 DT= 5.0 min	Res.(N)=	3.00	

	U.H. Tp(hr)=	0.17	
Unit Hyd Qpeak (cms)=	0.169		
PEAK FLOW (cms)=	0.046 (i)		
TIME TO PEAK (hrs)=	3.083		
RUNOFF VOLUME (mm)=	16.902		
TOTAL RAINFALL (mm)=	61.600		
RUNOFF COEFFICIENT =	0.274		
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.			

CALIB			
NASHYD (0017)	Area (ha)=	0.59	Curve Number
(CN)= 65.0	Ia (mm)=	4.70	# of Linear
ID= 1 DT= 5.0 min	Res.(N)=	3.00	

	U.H. Tp(hr)=	0.17	
Unit Hyd Qpeak (cms)=	0.133		
***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!			
(i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:			
CN* = 60.7 Ia = Dep. Storage (Above)			
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL			

THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0019)			
IN= 2----> OUT= 1			
DT= 5.0 min	OUTFLOW	STORAGE	OUTFLOW
STORAGE	(cms)	(ha.m.)	(cms)
(ha.m.)	**** WARNING : FIRST OUTFLOW IS NOT ZERO.		
0.0238	0.0001	0.0074	0.0165
	0.0045	0.0089	0.0180
0.0280	0.0084	0.0111	0.0193
0.0326	0.0110	0.0137	0.0206
0.0376	0.0131	0.0166	0.0218
0.0435	0.0149	0.0200	0.0000
0.0000			

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
INFLOW : ID= 2 (0018)	1.480	0.136	3.00
24.99	OUTFLOW: ID= 1 (0019)	1.480	0.017
19.96			3.83

0.0241	PEAK FLOW REDUCTION [Qout/Qin](%)=	12.25	
	TIME SHIFT OF PEAK FLOW (min)=	50.00	
	MAXIMUM STORAGE USED (ha.m.)=		

ADD HYD (0020)	AREA	QPEAK	TPEAK
1 + 2 = 3	(ha)	(cms)	(hrs)
	R.V.	(mm)	

CALIB			
STANDHYD (0018)	Area (ha)=	1.48	Curve Number
(CN)= 67.1	Ia (mm)=	4.60	# of Linear
ID= 1 DT= 5.0 min	Res.(N)=	3.00	

	U.H. Tp(hr)=	0.17	
Unit Hyd Qpeak (cms)=	0.315		
PEAK FLOW (cms)=	0.090 (i)		
TIME TO PEAK (hrs)=	3.083		
RUNOFF VOLUME (mm)=	17.833		
TOTAL RAINFALL (mm)=	61.600		
RUNOFF COEFFICIENT =	0.289		
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.			

CALIB			
STANDHYD (0021)	Area (ha)=	1.28	Curve Number
(CN)= 67.1	Ia (mm)=	4.60	# of Linear
ID= 1 DT= 5.0 min	Total Imp(%)=	25.00	Dir. Conn. (%)=
25.00	-----		
IMPERVIOUS	PVIOUS (i)		
Surface Area (ha)=	0.32	0.96	
Dep. Storage (mm)=	1.00	5.80	
Average Slope (%)=	1.00	6.60	
Length (m)=	92.38	100.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	95.90	26.51	
over (min)	5.00	20.00	
Storage Coeff. (min)=	2.48 (ii)	17.02 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.29	0.06	

TOTALS

PEAK FLOW	(cms)=	0.09	0.04
0.109 (iii)			
TIME TO PEAK	(hrs)=	3.00	3.17
3.00			
RUNOFF VOLUME	(mm)=	60.60	14.96
26.36			
TOTAL RAINFALL	(mm)=	61.60	61.60
61.60			
RUNOFF COEFFICIENT	=	0.98	0.24
0.43			

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
CN* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0022)		OUTFLOW	STORAGE	OUTFLOW
IN=	DT=			
2 ----> OUT= 1	5.0 min			
STORAGE				
(ha.m.)				
**** WARNING : FIRST OUTFLOW IS NOT ZERO.				
0.0001	0.0052		0.0843	
0.0172				
0.0200	0.0056	0.0066		0.0945
0.0231				
0.0265	0.0202	0.0082		0.1036
0.0301	0.0402	0.0101		0.1121
0.0000	0.0595	0.0122		0.1199
	0.0728	0.0146		0.0000

AREA QPEAK TPEAK

R.V.

(mm)	(ha)	(cms)	(hrs)
INFLOW : ID= 2 (0021)	1.280	0.109	3.00
26.36 OUTFLOW: ID= 1 (0022)	1.280	0.059	3.08
22.27			
PEAK FLOW REDUCTION [Qout/Qin](%)= 54.24			
TIME SHIFT OF PEAK FLOW (min)= 5.00			
MAXIMUM STORAGE USED (ha.m.)=			
0.0122			

ADD HYD (0024)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0022):		1.28	0.059	3.08	22.27
+ ID2= 2 (0023):		1.40	0.090	3.08	17.83
ID = 3 (0024):		2.68	0.149	3.08	19.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0055)	Area	(ha)=	1.24	Curve Number
(CN)=	67.5	Ia	(mm)=	8.20	# of Linear
ID= 1 DT= 5.0 min	Res.(N)= 3.00				
		U.H. Tp(hrs)=	0.26		

Unit Hyd Qpeak (cms)= 0.182

PEAK FLOW (cms)= 0.056 (i)
TIME TO PEAK (hrs)= 3.167
RUNOFF VOLUME (mm)= 16.219
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.263

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				1.25	4.40		2.75	43.70		4.25	5.80	
5.75	2.90			1.50	4.40		3.00	113.70		4.50	5.80	
CALIB	NASHYD (0056)	Area	(ha)=	0.58	Curve Number							
(CN)=	66.1	Ia	(mm)=	4.60	# of Linear							
ID= 1 DT= 5.0 min	Res.(N)= 3.00											
		U.H. Tp(hrs)=	0.26									

Unit Hyd Qpeak (cms)= 0.085
PEAK FLOW (cms)= 0.028 (i)
TIME TO PEAK (hrs)= 3.167
RUNOFF VOLUME (mm)= 17.337
TOTAL RAINFALL (mm)= 61.600
RUNOFF COEFFICIENT = 0.281

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

----- TRANSFORMED HYETOGRAPH -----			
TIME	RAIN	TIME	RAIN
TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr
4.58	4.40	0.083	2.90 1.583
4.67	4.40	0.167	2.90 1.667
4.75	4.40	0.250	2.90 1.750
4.83	4.40	0.333	2.90 1.833
4.92	4.40	0.417	2.90 1.917
5.00	4.40	0.500	2.90 2.000
5.08	2.90	0.583	4.40 2.083
5.17	2.90	0.667	4.40 2.167
5.25	2.90	0.750	4.40 2.250
5.33	2.90	0.833	4.40 2.333
5.42	2.90	0.917	4.40 2.417

READ STORM		Filename: C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-			
		f4bf8f2008cel\c775860c			
Ptotal= 72.90 mm		Comments: 25-Year, 6 hour SCS Type II - Peterborou			
TIME	RAIN	TIME	RAIN	' TIME	RAIN
hrs	mm/hr	hrs	mm/hr	' hrs	mm/hr
4.75	4.40	0.25	2.90 1.75	7.30 3.25	16.00
5.00	4.40	0.50	2.90 2.00	7.30 3.50	16.00
5.25	2.90	0.75	4.40 2.25	8.80 3.75	7.30
5.50	2.90	1.00	4.40 2.50	8.80 4.00	7.30

CALIB	NASHYD (0002)	Area	(ha)=	1.42	Curve Number
(CN)=	63.1	Ia	(mm)=	9.10	# of Linear
ID= 1 DT= 5.0 min	Res.(N)= 3.00				

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

5.50	2.90	1.000	4.40 2.500	8.80 4.000	7.30
5.58	2.90	1.083	4.40 2.583	43.70 4.083	5.80
5.67	2.90	1.167	4.40 2.667	43.70 4.167	5.80
5.75	2.90	1.250	4.40 2.750	43.70 4.250	5.80
5.83	2.90	1.333	4.40 2.833	113.70 4.333	5.80
5.92	2.90	1.417	4.40 2.917	113.70 4.417	5.80
6.00	2.90	1.500	4.40 3.000	113.70 4.500	5.80

Unit Hyd Qpeak (cms)= 0.247
PEAK FLOW (cms)= 0.086 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 19.144
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.263

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0015)	Area (ha)=	2.66	Curve Number
(CN)=	64.8	ID= 1 DT= 5.0 min	Ia (mm)=	4.80 # of Linear
Res.(N)=	3.00	U.H. Tp(hrs)= 0.17		

Unit Hyd Qpeak (cms)= 0.598
PEAK FLOW (cms)= 0.216 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 22.424
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.308

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0016)	IN= 2--> OUT= 1	DT= 5.0 min	OUTFLOW	STORAGE	OUTFLOW
STORAGE	(ha.m.)		(cms)	(ha.m.)	(cms)

**** WARNING : FIRST OUTFLOW IS NOT ZERO.
0.0001 0.0072 | 0.1306
0.0171 0.0065 0.0083 | 0.1492
0.0194 0.0242 0.0096 | 0.1656
0.0220 0.0501 0.0112 | 0.1806
0.0248 0.0806 0.0129 | 0.1944
0.0278 0.1098 0.0149 | 0.0000

AREA QPEAK TPEAK
R.V. (ha) (cms) (hrs)

INFLOW : ID= 2 (0015) 2.660 0.216 3.08
22.42

OUTFLOW: ID= 1 (0016) 2.660 0.140 3.25
19.71

PEAK FLOW REDUCTION [Qout/Qin](%)= 64.86
TIME SHIFT OF PEAK FLOW (min)= 10.00
MAXIMUM STORAGE USED (ha.m.)= 0.0185

CALIB	NASHYD (0001)	Area (ha)=	2.02	Curve Number
(CN)=	61.5	ID= 1 DT= 5.0 min	Ia (mm)=	5.30 # of Linear
Res.(N)=	3.00	U.H. Tp(hrs)= 0.17		

Unit Hyd Qpeak (cms)= 0.454
PEAK FLOW (cms)= 0.147 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 20.094
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.276

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0004)	Area (ha)=	2.44	Curve Number
(CN)=	68.8	ID= 1 DT= 5.0 min	Ia (mm)=	8.00 # of Linear
Res.(N)=	3.00	U.H. Tp(hrs)= 0.17		

Unit Hyd Qpeak (cms)= 0.548
PEAK FLOW (cms)= 0.210 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 23.305
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.320

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0003)	Area (ha)=	1.53	Curve Number
(CN)=	61.7	ID= 1 DT= 5.0 min	Ia (mm)=	8.70 # of Linear
Res.(N)=	3.00	U.H. Tp(hrs)= 0.17		

Unit Hyd Qpeak (cms)= 0.344
PEAK FLOW (cms)= 0.103 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 18.510
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.254

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0007)	Area (ha)=	0.59	Curve Number
(CN)=	65.0	ID= 1 DT= 5.0 min	Ia (mm)=	4.70 # of Linear
Res.(N)=	3.00	U.H. Tp(hrs)= 0.17		

Unit Hyd Qpeak (cms)= 0.133
PEAK FLOW (cms)= 0.048 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 22.611
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.310

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0008)	Area (ha)=	1.48	
ID= 1 DT= 5.0 min	Total Imp(%)=	23.00	Dir. Conn.(%)=	23.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 0.34 1.14
Dep. Storage (mm)= 1.00 5.30
Average Slope (%)= 2.00 5.00
Length (m)= 99.33 40.00
Mannings n = 0.013 0.250
Max.Eff.Inten.(mm/hr)= 113.70 38.86
over (min) 5.00 10.00
Storage Coeff. (min)= 1.96 (ii) 9.79 (ii)
Unit Hyd. Tpeak (min)= 5.00 10.00
Unit Hyd. peak (cms)= 0.31 0.11

TOTALS
PEAK FLOW (cms)= 0.11 0.08
0.190 (iii) TIME TO PEAK (hrs)= 3.00 3.08
3.00

RUNOFF VOLUME	(mm) =	71.90	19.69	
31.70	TOTAL RAINFALL	(mm) =	72.90	72.90
72.90	RUNOFF COEFFICIENT	=	0.99	0.27
0.43				

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0009)		AREA	QPEAK	TPEAK	R.V.	
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)	
		ID1= 1 (0007):	0.59	0.048	3.08	22.61
		+ ID2= 2 (0008):	1.48	0.190	3.00	31.70
		ID = 3 (0009):	2.07	0.238	3.00	29.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB		Area	(ha) =	1.40	Curve Number
NASHYD (0011)		Ia	(mm) =	4.60	# of Linear
(CN) = 67.1		Res.(N) = 3.00			
		U.H. Tp(hrs) =	0.17		
Unit Hyd Qpeak (cms) = 0.315					
PEAK FLOW (cms) = 0.123 (i)					
TIME TO PEAK (hrs) = 3.083					
RUNOFF VOLUME (mm) = 24.104					
TOTAL RAINFALL (mm) = 72.900					
RUNOFF COEFFICIENT = 0.331					

ADD HYD (0012)		AREA	QPEAK	TPEAK	R.V.	
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)	
		ID1= 1 (0010):	1.28	0.135	3.00	33.15
		+ ID2= 2 (0011):	1.40	0.123	3.08	24.10
		ID = 3 (0012):	2.68	0.257	3.00	28.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB		Area	(ha) =	8.72	Curve Number
NASHYD (0005)		Ia	(mm) =	8.80	# of Linear
(CN) = 64.6		Res.(N) = 3.00			
		U.H. Tp(hrs) =	0.39		
Unit Hyd Qpeak (cms) = 0.854					
PEAK FLOW (cms) = 0.369 (i)					
TIME TO PEAK (hrs) = 3.333					
RUNOFF VOLUME (mm) = 20.209					
TOTAL RAINFALL (mm) = 72.900					
RUNOFF COEFFICIENT = 0.277					

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area	(ha) =	8.50	Curve Number
NASHYD (0014)		Ia	(mm) =	8.40	# of Linear
(CN) = 64.4		Res.(N) = 3.00			
		U.H. Tp(hrs) =	0.39		
Unit Hyd Qpeak (cms) = 0.832					
PEAK FLOW (cms) = 0.361 (i)					
TIME TO PEAK (hrs) = 3.333					
RUNOFF VOLUME (mm) = 20.300					
TOTAL RAINFALL (mm) = 72.900					
RUNOFF COEFFICIENT = 0.278					

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		STANDHYD (0010)	Area	(ha) =	1.28
ID= 1 DT= 5.0 min		Total	Imp(%) =	24.60	Dir. Conn.(%) =
24.60					

IMPERVIOUS PERVIOUS (i)					
Surface Area	(ha) =	0.31	0.97		
Dep. Storage	(mm) =	1.00	5.80		
Average Slope	(%) =	1.00	6.60		
Length	(m) =	92.38	100.00		
Mannings n	=	0.013	0.250		
Max.Eff.Inten.(mm/hr) =	113.70	36.62			
over (min)	5.00	20.00			
Storage Coeff. (min) =	2.31 (ii)	15.09 (ii)			
Unit Hyd. Tpeak (min) =	5.00	20.00			
Unit Hyd. peak (cms) =	0.30	0.07			

TOTALS PEAK FLOW (cms) = 0.10 0.06

0.135 (iii) TIME TO PEAK (hrs) = 3.00 3.17

3.00 RUNOFF VOLUME (mm) = 71.90 20.51

33.15 TOTAL RAINFALL (mm) = 72.90 72.90

72.90 RUNOFF COEFFICIENT = 0.99 0.28

0.45 ***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

CN* = 62.5 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area	(ha) =	2.66	Curve Number
NASHYD (0006)		Ia	(mm) =	4.80	# of Linear
(CN) = 64.8		Res.(N) = 3.00			
		U.H. Tp(hrs) =	0.17		

Unit Hyd Qpeak (cms) = 0.598

PEAK FLOW (cms) = 0.216 (i)

TIME TO PEAK (hrs) = 3.083

RUNOFF VOLUME (mm) = 22.424

TOTAL RAINFALL (mm) = 72.900

RUNOFF COEFFICIENT = 0.308

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area	(ha) =	0.75	Curve Number
NASHYD (0013)		Ia	(mm) =	7.40	# of Linear
(CN) = 68.1		Res.(N) = 3.00			
		U.H. Tp(hrs) =	0.17		

Unit Hyd Qpeak (cms) = 0.169

PEAK FLOW (cms) = 0.064 (i)

TIME TO PEAK (hrs) = 3.083

RUNOFF VOLUME (mm) = 23.172

TOTAL RAINFALL (mm) = 72.900

RUNOFF COEFFICIENT = 0.318

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |

| NASHYD (0017) | Area (ha)= 0.59 Curve Number
 (CN)= 65.0
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hr)= 0.17
 Unit Hyd Qpeak (cms)= 0.133
 PEAK FLOW (cms)= 0.048 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 22.611
 TOTAL RAINFALL (mm)= 72.900
 RUNOFF COEFFICIENT = 0.310

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB
 | STANDHYD (0018) | Area (ha)= 1.48
 | ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn. (%)=
 23.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.34	1.14	
Dep. Storage (mm)=	1.00	5.30	
Average Slope (%)=	2.00	5.00	
Length (m)=	99.33	40.00	
Mannings n =	0.013	0.250	
Max.Eff. Inten. (mm/hr)=	113.70	38.86	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.96 (ii)	9.79 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.31	0.11	

TOTALS

PEAK FLOW (cms)=	0.11	0.08	
0.190 (iii)			
TIME TO PEAK (hrs)=	3.00	3.08	
3.00			
RUNOFF VOLUME (mm)=	71.90	19.69	
31.70			
TOTAL RAINFALL (mm)=	72.90	72.90	
72.90			

RUNOFF COEFFICIENT = 0.99
 TIME SHIFT OF PEAK FLOW (min)= 55.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0313

RUNOFF COEFFICIENT = 0.99
 0.43
 ***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 (i) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR (0019) |
 | IN= 2--> OUT= 1 |
 | DT= 5.0 min |
 STORAGE (ha.m.) OUTFLOW (cms) STORAGE (ha.m.) OUTFLOW (cms)

	***** WARNING : FIRST OUTFLOW IS NOT ZERO.		
0.0238	0.0001	0.0074	0.0165
0.0280	0.0045	0.0089	0.0180
0.0326	0.0084	0.0111	0.0193
0.0376	0.0110	0.0137	0.0206
0.0435	0.0131	0.0166	0.0218
0.0000	0.0149	0.0200	0.0000

AREA QPEAK TPEAK R.V.
 (ha) (cms) (hrs) (mm)

	INFLOW : ID= 2 (0018)	1.480	0.190	3.00
31.70	OUTFLOW: ID= 1 (0019)	1.480	0.019	3.92
26.67				

PEAK FLOW REDUCTION [Qout/Qin](%)= 9.99
 TIME SHIFT OF PEAK FLOW (min)= 55.00
 MAXIMUM STORAGE USED (ha.m.)=

 ADD HYD (0020)
 1 + 2 = 3
 AREA QPEAK TPEAK R.V.
 (ha) (cms) (hrs) (mm)

ID1= 1 (0017):	0.59	0.048	3.08	22.61
+ ID2= 2 (0019):	1.48	0.019	3.92	26.67
-----	2.07	0.065	3.08	25.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB
 | NASHYD (0023) | Area (ha)= 1.40 Curve Number
 (CN)= 67.1
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hr)= 0.17
 Unit Hyd Qpeak (cms)= 0.315
 PEAK FLOW (cms)= 0.123 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 24.104
 TOTAL RAINFALL (mm)= 72.900
 RUNOFF COEFFICIENT = 0.331

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB
 | STANDHYD (0021) | Area (ha)= 1.28
 | ID= 1 DT= 5.0 min | Total Imp(%)= 25.00 Dir. Conn. (%)=
 25.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.32	0.96	
Dep. Storage (mm)=	1.00	5.80	
Average Slope (%)=	1.00	6.60	

| RESERVOIR (0022) |
 | IN= 2--> OUT= 1 |
 | DT= 5.0 min |
 STORAGE (ha.m.) OUTFLOW (cms) STORAGE (ha.m.) OUTFLOW (cms)

	***** WARNING : FIRST OUTFLOW IS NOT ZERO.		
0.0172	0.0001	0.0052	0.0843
0.0200	0.0056	0.0066	0.0945
0.0231	0.0202	0.0082	0.1036
0.0265	0.0402	0.0101	0.1121

0.0301	0.0595	0.0122		0.1199
0.0000	0.0728	0.0146		0.0000
R.V.	AREA	QPEAK	TPEAK	
(mm)	(ha)	(cms)	(hrs)	
INFLOW : ID= 2 (0021)	1.280	0.137	3.00	
33.35 OUTFLOW: ID= 1 (0022)	1.280	0.071	3.17	
29.27				
PEAK FLOW REDUCTION [Qout/Qin](%) = 52.21				
TIME SHIFT OF PEAK FLOW (min) = 10.00				
MAXIMUM STORAGE USED (ha.m.) =				
0.0144				

ADD HYD (0024)	1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
(CN)= 67.5		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0022):	1.28	0.071	3.17	29.27	
+ ID2= 2 (0023):	1.40	0.123	3.08	24.10	
ID = 3 (0024):	2.68	0.194	3.08	26.57	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0055)	Area	(ha)=	1.24	Curve Number
(CN)= 67.5					
ID= 1 DT= 5.0 min	Ia	(mm)=	8.20	# of Linear	
Res.(N)= 3.00					

----- U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.182

PEAK FLOW (cms)= 0.078 (i)
TIME TO PEAK (hrs)= 3.167

RUNOFF VOLUME (mm)= 22.370
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.307

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0056)	Area	(ha)=	0.58	Curve Number
(CN)= 66.1					
ID= 1 DT= 5.0 min	Ia	(mm)=	4.60	# of Linear	
Res.(N)= 3.00					

----- U.H. Tp(hrs)= 0.26

Unit Hyd Qpeak (cms)= 0.085

PEAK FLOW (cms)= 0.038 (i)
TIME TO PEAK (hrs)= 3.167
RUNOFF VOLUME (mm)= 23.476
TOTAL RAINFALL (mm)= 72.900
RUNOFF COEFFICIENT = 0.322

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

** SIMULATION NUMBER: 5 **

READ STORM	Filename: C:\Users\mwilson\AppData\Local\Temp\f4b8f2008cel\4694a7c7	
		Comments: 50-Year, 6 hour SCS Type II - Peterborou
TIME RAIN		
hrs mm/hr		
4.75 4.90	0.25	3.30 1.75
		8.10 3.25
		17.90 17.90

5.00 4.90	0.50	3.30 2.00	8.10 3.50	17.90
5.25 3.30	0.75	4.90 2.25	9.80 3.75	8.10
5.50 3.30	1.00	4.90 2.50	9.80 4.00	8.10
5.75 3.30	1.25	4.90 2.75	48.90 4.25	6.50
6.00 3.30	1.50	4.90 3.00	127.00 4.50	6.50

5.25 3.30	0.750	4.90 2.250	9.80 3.750	8.10
5.33 3.30	0.833	4.90 2.333	9.80 3.833	8.10
5.42 3.30	0.917	4.90 2.417	9.80 3.917	8.10
5.50 3.30	1.000	4.90 2.500	9.80 4.000	8.10
5.58 3.30	1.083	4.90 2.583	48.90 4.083	6.50
5.67 3.30	1.167	4.90 2.667	48.90 4.167	6.50
5.75 3.30	1.250	4.90 2.750	48.90 4.250	6.50
5.83 3.30	1.333	4.90 2.833	127.00 4.333	6.50
5.92 3.30	1.417	4.90 2.917	127.00 4.417	6.50
6.00 3.30	1.500	4.90 3.000	127.00 4.500	6.50

CALIB	NASHYD (0002)	Area	(ha)=	1.42	Curve Number
(CN)= 63.1					
ID= 1 DT= 5.0 min	Ia	(mm)=	9.10	# of Linear	
Res.(N)= 3.00					

----- U.H. Tp(hrs)= 0.22

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME
STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	'	TIME	RAIN	'
hrs	mm/hr	hrs	mm/hr		hrs	mm/hr	
4.58 4.90	0.083	3.30 1.583	8.10 3.083		17.90		
4.67 4.90	0.167	3.30 1.667	8.10 3.167		17.90		
4.75 4.90	0.250	3.30 1.750	8.10 3.250		17.90		
4.83 4.90	0.333	3.30 1.833	8.10 3.333		17.90		
4.92 4.90	0.417	3.30 1.917	8.10 3.417		17.90		
5.00 4.90	0.500	3.30 2.000	8.10 3.500		17.90		
5.08 3.30	0.583	4.90 2.083	9.80 3.583		8.10		
5.17 3.30	0.667	4.90 2.167	9.80 3.667		8.10		

Unit Hyd Qpeak (cms)= 0.247
PEAK FLOW (cms)= 0.107 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 23.680
TOTAL RAINFALL (mm)= 81.475
RUNOFF COEFFICIENT = 0.291

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0001)	Area	(ha)=	2.02	Curve Number
(CN)= 61.5					
ID= 1 DT= 5.0 min	Ia	(mm)=	5.30	# of Linear	
Res.(N)= 3.00					

----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.454
PEAK FLOW (cms)= 0.180 (i)
TIME TO PEAK (hrs)= 3.083
RUNOFF VOLUME (mm)= 24.585
TOTAL RAINFALL (mm)= 81.475

RUNOFF COEFFICIENT = 0.302

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
NASHYD	(0015)
(CN)=	64.8
ID=	1 DT= 5.0 min
Res.(N)=	3.00
U.H. Tp(hr)=	0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.264 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 27.291
 TOTAL RAINFALL (mm)= 81.475
 RUNOFF COEFFICIENT = 0.335

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR	(0016)
IN=	2--> OUT= 1
DT=	5.0 min
STORAGE	
(ha.m.)	

OUTFLOW STORAGE | OUTFLOW
 (cms) (ha.m.) | (cms)

**** WARNING : FIRST OUTFLOW IS NOT ZERO.
 0.0001 0.0072 | 0.1306

0.0171	0.0065	0.0083	0.1492
0.0194	0.0242	0.0096	0.1656
0.0220	0.0501	0.0112	0.1806
0.0248	0.0806	0.0129	0.1944
0.0278	0.1098	0.0149	0.0000
0.0000			

TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 22.900
 TOTAL RAINFALL (mm)= 81.475
 RUNOFF COEFFICIENT = 0.281

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
NASHYD	(0007)
(CN)=	65.0
ID=	1 DT= 5.0 min
Res.(N)=	3.00
U.H. Tp(hr)=	0.17

Unit Hyd Qpeak (cms)= 0.133

PEAK FLOW (cms)= 0.059 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 27.504
 TOTAL RAINFALL (mm)= 81.475
 RUNOFF COEFFICIENT = 0.338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD	(0008)
ID=	1 DT= 5.0 min
23.00	Total Imp(%)= 23.00 Dir. Conn.(%)=

IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 0.34 1.14
 Dep. Storage (mm)= 1.00 5.30
 Average Slope (%)= 2.00 5.00
 Length (m)= 99.33 40.00
 Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 127.00 47.44
 over (min) 5.00 10.00
 Storage Coeff. (min)= 1.88 (ii) 9.10 (ii)
 Unit Hyd. Tpeak (min)= 5.00 10.00
 Unit Hyd. peak (cms)= 0.32 0.12

R.V. AREA QPEAK TPEAK
 (mm) (ha) (cms) (hrs)
 INFLOW : ID= 2 (0015) 2.660 0.264 3.08
 27.29 OUTFLOW: ID= 1 (0016) 2.660 0.165 3.25
 24.58
 PEAK FLOW REDUCTION [Qout/Qin](%)= 62.53
 TIME SHIFT OF PEAK FLOW (min)= 10.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0220

CALIB	
NASHYD	(0004)
(CN)=	68.8
ID=	1 DT= 5.0 min
Res.(N)=	3.00
U.H. Tp(hr)=	0.17

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.257 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 28.513
 TOTAL RAINFALL (mm)= 81.475
 RUNOFF COEFFICIENT = 0.350

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
NASHYD	(0003)
(CN)=	61.7
ID=	1 DT= 5.0 min
Res.(N)=	3.00
U.H. Tp(hr)=	0.17

Unit Hyd Qpeak (cms)= 0.344

PEAK FLOW (cms)= 0.128 (i)

TOTALS
 PEAK FLOW (cms)= 0.12 0.11
 0.225 (iii)
 TIME TO PEAK (hrs)= 3.00 3.08
 3.00
 RUNOFF VOLUME (mm)= 80.48 24.11
 37.07
 TOTAL RAINFALL (mm)= 81.48 81.48
 81.48
 RUNOFF COEFFICIENT = 0.99 0.30
 0.46
 ***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD	(0009)
1 + 2 = 3	AREA QPEAK TPEAK R.V.
	(ha) (cms) (hrs) (mm)
ID1= 1 (0007):	0.59 0.059 3.08 27.50
+ ID2= 2 (0008):	1.48 0.225 3.00 37.07
=	=
ID = 3 (0009):	2.07 0.283 3.00 34.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	
NASHYD	(0011)
(CN)=	67.1
ID=	1 DT= 5.0 min
Res.(N)=	3.00
U.H. Tp(hr)=	0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms) = 0.149 (i)
 TIME TO PEAK (hrs) = 3.083
 RUNOFF VOLUME (mm) = 29.236
 TOTAL RAINFALL (mm) = 81.475
 RUNOFF COEFFICIENT = 0.359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0010)	Area (ha) = 1.28
ID= 1 DT= 5.0 min	Total Imp(%) = 24.60 Dir. Conn.(%) = 24.60

ADD HYD (0012)	
1 + 2 = 3	AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)
ID1= 1 (0010):	1.28 0.172 3.00 38.72
+ ID2= 2 (0011):	1.40 0.149 3.08 29.24
ID = 3 (0012):	2.68 0.320 3.00 33.77

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Surface Area (ha) = 0.31	IMPERVIOUS 0.97
Dep. Storage (mm) = 1.00	5.80
Average Slope (%) = 1.00	6.60
Length (m) = 92.38	100.00
Mannings n = 0.013	0.250
Max.Eff.Inten.(mm/hr) = 127.00	44.89
over (min) 5.00	15.00
Storage Coeff. (min) = 2.21 (ii)	13.99 (ii)
Unit Hyd. Tpeak (min) = 5.00	15.00
Unit Hyd. peak (cms) = 0.30	0.08

CALIB	
NASHYD (0005)	Area (ha) = 8.72 Curve Number (CN) = 64.6
ID= 1 DT= 5.0 min Res.(N)= 3.00	Ia (mm) = 8.80 # of Linear U.H. Tp(hrs) = 0.39

Unit Hyd Qpeak (cms) = 0.854

PEAK FLOW (cms) = 0.458 (i)
 TIME TO PEAK (hrs) = 3.250
 RUNOFF VOLUME (mm) = 24.926
 TOTAL RAINFALL (mm) = 81.475
 RUNOFF COEFFICIENT = 0.306

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TOTALS	
PEAK FLOW (cms) = 0.11	0.07
0.172 (iii)	
TIME TO PEAK (hrs) = 3.00	3.08
3.00	
RUNOFF VOLUME (mm) = 80.48	25.11
38.72	
TOTAL RAINFALL (mm) = 81.48	81.48
81.48	
RUNOFF COEFFICIENT = 0.48	0.99 0.31

CALIB	
NASHYD (0014)	Area (ha) = 8.50 Curve Number (CN) = 64.4
ID= 1 DT= 5.0 min Res.(N)= 3.00	Ia (mm) = 8.40 # of Linear U.H. Tp(hrs) = 0.39

Unit Hyd Qpeak (cms) = 0.832

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 CN* = 62.5 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

PEAK FLOW (cms) = 0.448 (i)
 TIME TO PEAK (hrs) = 3.250
 RUNOFF VOLUME (mm) = 25.010
 TOTAL RAINFALL (mm) = 81.475
 RUNOFF COEFFICIENT = 0.307

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
NASHYD (0006)	Area (ha) = 2.66 Curve Number (CN) = 64.8
ID= 1 DT= 5.0 min Res.(N)= 3.00	Ia (mm) = 4.80 # of Linear U.H. Tp(hrs) = 0.17

CALIB	
NASHYD (0017)	Area (ha) = 0.59 Curve Number (CN) = 65.0
ID= 1 DT= 5.0 min Res.(N)= 3.00	Ia (mm) = 4.70 # of Linear U.H. Tp(hrs) = 0.17

Unit Hyd Qpeak (cms) = 0.133

PEAK FLOW (cms) = 0.059 (i)
 TIME TO PEAK (hrs) = 3.083
 RUNOFF VOLUME (mm) = 27.504
 TOTAL RAINFALL (mm) = 81.475
 RUNOFF COEFFICIENT = 0.338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
NASHYD (0013)	Area (ha) = 0.75 Curve Number (CN) = 68.1
ID= 1 DT= 5.0 min Res.(N)= 3.00	Ia (mm) = 7.40 # of Linear U.H. Tp(hrs) = 0.17

CALIB	
STANDHYD (0018)	Area (ha) = 1.48
ID= 1 DT= 5.0 min Total Imp(%) = 23.00	Dir. Conn.(%) = 23.00

IMPERVIOUS	PERVERIOUS (i)
Surface Area (ha) = 0.34	1.14
Dep. Storage (mm) = 1.00	5.30
Average Slope (%) = 2.00	5.00
Length (m) = 99.33	40.00
Mannings n = 0.013	0.250
Max.Eff.Inten.(mm/hr) = 127.00	47.44
over (min) 5.00	10.00
Storage Coeff. (min) = 1.88 (ii)	9.10 (ii)
Unit Hyd. Tpeak (min) = 5.00	10.00
Unit Hyd. peak (cms) = 0.32	0.12

TOTALS
 PEAK FLOW (cms) = 0.12 0.11
 0.225 (ii)

CALIB	
NASHYD (0013)	Area (ha) = 0.75 Curve Number (CN) = 68.1
ID= 1 DT= 5.0 min Res.(N)= 3.00	Ia (mm) = 7.40 # of Linear U.H. Tp(hrs) = 0.17

TIME TO PEAK (hrs)=	3.00	3.08	OUTFLOW: ID= 1 (0019)	1.480	0.020	4.00
RUNOFF VOLUME (mm)=	80.48	24.11	32.04			
TOTAL RAINFALL (mm)=	81.48	81.48	PEAK FLOW REDUCTION [Qout/Qin](%)= 9.12			
RUNOFF COEFFICIENT =	0.99	0.30	TIME SHIFT OF PEAK FLOW (min)= 60.00			
0.46			MAXIMUM STORAGE USED (ha.m.)=			

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
CN* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0019)		OUTFLOW	STORAGE	OUTFLOW	
IN= 2	---	OUT= 1			
DT= 5.0 min					
STORAGE					
(ha.m.)					
**** WARNING : FIRST OUTFLOW IS NOT ZERO.					
0.0238		0.0001	0.0074	0.0165	
0.0280		0.0045	0.0089	0.0180	
0.0326		0.0084	0.0111	0.0193	
0.0376		0.0110	0.0137	0.0206	
0.0435		0.0131	0.0166	0.0218	
0.0000		0.0149	0.0200	0.0000	
R.V.		AREA	QPEAK	TPEAK	
(mm)		(ha)	(cms)	(hrs)	
INFLOW : ID= 2 (0018)		1.480	0.225	3.00	
37.07					

ADD HYD (0020)	1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0017):		0.59	0.059	3.08	27.50
+ ID2= 2 (0019):		1.48	0.020	4.00	32.04
ID = 3 (0020):		2.07	0.077	3.08	30.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0023)	Area	(ha)=	1.40	Curve Number
(CN)= 67.1				
ID= 1 DT= 5.0 min	Ia	(mm)=	4.60	# of Linear
Res.(N)= 3.00				
U.H. Tp(hrs)=	0.17			
Unit Hyd Ppeak (cms)=	0.315			
PEAK FLOW (cms)=	0.149 (i)			
TIME TO PEAK (hrs)=	3.083			
RUNOFF VOLUME (mm)=	29.236			
TOTAL RAINFALL (mm)=	81.475			
RUNOFF COEFFICIENT =	0.359			

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0021)	Area	(ha)=	1.28	
-----------------------	------	-------	------	--

ID= 1 DT= 5.0 min	Total Imp(%)=	25.00	Dir. Conn.(%)=		
25.00					
	IMPERVIOUS	PERVIOUS (i)			
Surface Area (ha)=	0.32	0.96			
Dep. Storage (mm)=	1.00	5.80			
Average Slope (%)=	1.00	6.60			
Length (m)=	92.38	100.00			
Mannings n =	0.013	0.250			
Max.Eff.Inten.(mm/hr)=	127.00	44.89			
over (min)	5.00	15.00			
Storage Coeff. (min)=	2.21 (ii)	13.99 (ii)			
Unit Hyd. Tpeak (min)=	5.00	15.00			
Unit Hyd. peak (cms)=	0.30	0.08			
TOTALS					
PEAK FLOW (cms)=	0.11	0.07			
0.173 (iii)					
TIME TO PEAK (hrs)=	3.00	3.08			
3.00					
RUNOFF VOLUME (mm)=	80.47	25.11			
38.94					
TOTAL RAINFALL (mm)=	81.48	81.48			
81.48					
RUNOFF COEFFICIENT =	0.99	0.31			
0.48					

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
CN* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0022)		OUTFLOW	STORAGE	OUTFLOW	
IN= 2	---	OUT= 1			
DT= 5.0 min					
STORAGE					
(ha.m.)					
**** WARNING : FIRST OUTFLOW IS NOT ZERO.					

ADD HYD (0024)	1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0022):		1.28	0.085	3.17	34.86
+ ID2= 2 (0023):		1.40	0.149	3.08	29.24
ID = 3 (0024):		2.68	0.232	3.08	31.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0055)	Area	(ha)=	1.24	Curve Number
(CN)= 67.5				

| ID= 1 DT= 5.0 min | Ia (mm)= 8.20 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hr)= 0.26
 Unit Hyd Qpeak (cms)= 0.182
 PEAK FLOW (cms)= 0.096 (i)
 TIME TO PEAK (hrs)= 3.167
 RUNOFF VOLUME (mm)= 27.435
 TOTAL RAINFALL (mm)= 81.475
 RUNOFF COEFFICIENT = 0.337
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB | NASHYD (0056) | Area (ha)= 0.58 Curve Number
 (CN)= 66.1
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hr)= 0.26
 Unit Hyd Qpeak (cms)= 0.085
 PEAK FLOW (cms)= 0.047 (i)
 TIME TO PEAK (hrs)= 3.167
 RUNOFF VOLUME (mm)= 28.510
 TOTAL RAINFALL (mm)= 81.475
 RUNOFF COEFFICIENT = 0.350
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 **** SIMULATION NUMBER: 6 ***

 | READ STORM | Filename: C:\Users\mwilson\AppData\Local\Temp\ad98c7d6-b765-49b3-b3b5-f4b8f2008ce1\3ec6332a

| Ptotal= 89.93 mm | Comments: 100-Year, 6 hour SCS Type II - Peterboro

 TIME RAIN TIME RAIN | ' TIME RAIN |
 hrs mm/hr hrs mm/hr | hrs mm/hr | hrs mm/hr |
 4.75 5.40 0.25 3.60 | 1.75 9.00 | 3.25 19.80 |
 5.00 5.40 0.50 3.60 | 2.00 9.00 | 3.50 19.80 |
 5.25 3.60 0.75 5.40 | 2.25 10.80 | 3.75 9.00 |
 5.50 3.60 1.00 5.40 | 2.50 10.80 | 4.00 9.00 |
 5.75 3.60 1.25 5.40 | 2.75 53.90 | 4.25 7.20 |
 6.00 3.60 1.50 5.40 | 3.00 140.20 | 4.50 7.20 |

 | CALIB | NASHYD (0002) | Area (ha)= 1.42 Curve Number
 (CN)= 63.1
 | ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hr)= 0.22
 NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

 TIME RAIN ----- TRANSFORMED HYETOGRAPH -----
 hrs mm/hr hrs mm/hr | hrs mm/hr | hrs mm/hr |
 4.58 5.40 0.083 3.60 | 1.583 9.00 | 3.083 19.80 |
 4.67 5.40 0.167 3.60 | 1.667 9.00 | 3.167 19.80 |
 4.75 5.40 0.250 3.60 | 1.750 9.00 | 3.250 19.80 |

 | ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hr)= 0.17
 Unit Hyd Qpeak (cms)= 0.454
 PEAK FLOW (cms)= 0.215 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 29.289
 TOTAL RAINFALL (mm)= 89.925
 RUNOFF COEFFICIENT = 0.326
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB | NASHYD (0015) | Area (ha)= 2.66 Curve Number
 (CN)= 64.8
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear
 Res.(N)= 3.00
 ----- U.H. Tp(hr)= 0.17
 Unit Hyd Qpeak (cms)= 0.598
 PEAK FLOW (cms)= 0.313 (i)
 TIME TO PEAK (hrs)= 3.083
 RUNOFF VOLUME (mm)= 32.364
 TOTAL RAINFALL (mm)= 89.925
 RUNOFF COEFFICIENT = 0.360
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | RESERVOIR (0016) | IN= 2--> OUT= 1 | DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW
 STORAGE
 (hrs.) (cms) (ha.m.) | (cms)
 (hrs.)
 **** WARNING : FIRST OUTFLOW IS NOT ZERO.
 0.0001 0.0072 | 0.1306
 0.0171

0.0194	0.0065	0.0083		0.1492
0.0220	0.0242	0.0096		0.1656
0.0248	0.0501	0.0112		0.1806
0.0278	0.0806	0.0129		0.1944
0.0000	0.1098	0.0149		0.0000
R.V.	AREA	QPEAK	TPEAK	
(mm)	(ha)	(cms)	(hrs)	
INFLOW : ID= 2 (0015)	2.660	0.313	3.08	
32.36	OUTFLOW: ID= 1 (0016)	2.660	0.186	3.25
29.65				
PEAK FLOW REDUCTION [Qout/Qin](%)= 59.59				
TIME SHIFT OF PEAK FLOW (min)= 10.00				
MAXIMUM STORAGE USED (ha.m.)=				
0.0261				
CALIB NASHYD (0004)	Area (ha)=	2.44	Curve Number	
(CN)= 68.8	Ia (mm)=	8.00	# of Linear	
ID= 1 DT= 5.0 min	Res.(N)= 3.00			
-----	U.H. Tp(hrs)=	0.17		
Unit Hyd Qpeak (cms)=	0.548			
PEAK FLOW (cms)=	0.306 (i)			
TIME TO PEAK (hrs)=	3.083			
RUNOFF VOLUME (mm)=	33.929			
TOTAL RAINFALL (mm)=	89.925			
RUNOFF COEFFICIENT =	0.377			
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.				
CALIB STANDHYD (0007)	Area (ha)=	0.59	Curve Number	
(CN)= 65.0	Ia (mm)=	4.70	# of Linear	
ID= 1 DT= 5.0 min	Res.(N)= 3.00			
-----	U.H. Tp(hrs)=	0.17		
Unit Hyd Qpeak (cms)=	0.133			
PEAK FLOW (cms)=	0.070 (i)			
TIME TO PEAK (hrs)=	3.083			
RUNOFF VOLUME (mm)=	32.601			
TOTAL RAINFALL (mm)=	89.925			
RUNOFF COEFFICIENT =	0.363			
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.				
CALIB STANDHYD (0008)	Area (ha)=	1.48		
ID= 1 DT= 5.0 min	Total Imp(%)= 23.00	Dir. Conn.(%)=		
23.00				
				IMPERVIOUS PERVIOUS (i)

Surface Area (ha)=	0.34	1.14
Dep. Storage (mm)=	1.00	5.30
Average Slope (%)=	2.00	5.00
Length (m)=	99.33	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	140.20	56.45
over (min)	5.00	10.00
Storage Coeff. (min)=	1.81 (ii)	8.54 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00
Unit Hyd. peak (cms)=	0.32	0.12
TOTALS		
PEAK FLOW (cms)=	0.13	0.13
0.261 (iii)	TIME TO PEAK (hrs)=	3.00
3.00	RUNOFF VOLUME (mm)=	88.92
42.59	TOTAL RAINFALL (mm)=	89.93
89.93	RUNOFF COEFFICIENT =	0.99
0.47	0.32	

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
CN* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0009)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0007):	0.59	0.070	3.08	32.60	
+ ID2= 2 (0008):	1.48	0.261	3.00	42.59	
=====					
ID = 3 (0009):	2.07	0.330	3.00	39.74	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB STANDHYD (0011)	Area (ha)=	1.40	Curve Number	
(CN)= 67.1	Ia (mm)=	4.60	# of Linear	
ID= 1 DT= 5.0 min	Res.(N)= 3.00			
-----	U.H. Tp(hrs)=	0.17		
Unit Hyd Qpeak (cms)=	0.315			
PEAK FLOW (cms)=	0.176 (i)			
TIME TO PEAK (hrs)=	3.083			
RUNOFF VOLUME (mm)=	34.567			
TOTAL RAINFALL (mm)=	89.925			
RUNOFF COEFFICIENT =	0.384			
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.				
CALIB STANDHYD (0010)	Area (ha)=	1.28		
ID= 1 DT= 5.0 min	Total Imp(%)= 24.60	Dir. Conn.(%)=		
24.60				
				IMPERVIOUS PERVIOUS (i)
Surface Area (ha)=	0.31	0.97		
Dep. Storage (mm)=	1.00	5.80		
Average Slope (%)=	1.00	6.60		
Length (m)=	92.38	100.00		
Mannings n =	0.013	0.250		
Max.Eff.Inten.(mm/hr)=	140.20	53.60		
over (min)	5.00	15.00		
Storage Coeff. (min)=	2.13 (ii)	13.10 (ii)		
Unit Hyd. Tpeak (min)=	5.00	15.00		
Unit Hyd. peak (cms)=	0.31	0.08		
TOTALS				
PEAK FLOW (cms)=	0.12	0.09		
0.199 (iii)	TIME TO PEAK (hrs)=	3.00		
3.00				3.08

RUNOFF VOLUME	(mm) =	88.92	29.92	
44.43	TOTAL RAINFALL	(mm) =	89.93	89.93
89.93	RUNOFF COEFFICIENT	=	0.99	0.33
0.49				

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
CN* = 62.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0012)				
1 + 2 = 3				
AREA	QPEAK	TPEAK	R.V.	
(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (0010):	1.28	0.199	3.00	44.43
+ ID2= 2 (0011):	1.40	0.176	3.08	34.57
=====				
ID = 3 (0012):	2.68	0.374	3.00	39.28

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
NASHYD (0005)				
(CN)= 64.6	Area	(ha) =	8.72	Curve Number
ID= 1 DT= 5.0 min	Ia	(mm) =	8.80	# of Linear
Res.(N)= 3.00				
-----	U.H. Tp(hrs)=		0.39	

Unit Hyd Qpeak (cms) = 0.854

PEAK FLOW (cms) = 0.553 (i)
TIME TO PEAK (hrs) = 3.250
RUNOFF VOLUME (mm) = 29.868
TOTAL RAINFALL (mm) = 89.925
RUNOFF COEFFICIENT = 0.332

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0014)				
(CN)= 64.4	Area	(ha) =	8.50	Curve Number
ID= 1 DT= 5.0 min	Ia	(mm) =	8.40	# of Linear
Res.(N)= 3.00				
-----	U.H. Tp(hrs)=		0.39	

Unit Hyd Qpeak (cms) = 0.832

PEAK FLOW (cms) = 0.541 (i)
TIME TO PEAK (hrs) = 3.250
RUNOFF VOLUME (mm) = 29.943
TOTAL RAINFALL (mm) = 89.925
RUNOFF COEFFICIENT = 0.333

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0006)				
(CN)= 64.8	Area	(ha) =	2.66	Curve Number
ID= 1 DT= 5.0 min	Ia	(mm) =	4.80	# of Linear
Res.(N)= 3.00				
-----	U.H. Tp(hrs)=		0.17	

Unit Hyd Qpeak (cms) = 0.598
PEAK FLOW (cms) = 0.313 (i)
TIME TO PEAK (hrs) = 3.083
RUNOFF VOLUME (mm) = 32.364
TOTAL RAINFALL (mm) = 89.925
RUNOFF COEFFICIENT = 0.360

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |

NASHYD (0013)				
(CN)= 68.1	Area	(ha) =	0.75	Curve Number
ID= 1 DT= 5.0 min	Ia	(mm) =	7.40	# of Linear
Res.(N)= 3.00				
-----	U.H. Tp(hrs)=		0.17	

Unit Hyd Qpeak (cms) = 0.169

PEAK FLOW (cms) = 0.093 (i)
TIME TO PEAK (hrs) = 3.083
RUNOFF VOLUME (mm) = 33.676
TOTAL RAINFALL (mm) = 89.925
RUNOFF COEFFICIENT = 0.374

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0017)				
(CN)= 65.0	Area	(ha) =	0.59	Curve Number
ID= 1 DT= 5.0 min	Ia	(mm) =	4.70	# of Linear
Res.(N)= 3.00				
-----	U.H. Tp(hrs)=		0.17	

Unit Hyd Qpeak (cms) = 0.133

PEAK FLOW (cms) = 0.070 (i)
TIME TO PEAK (hrs) = 3.083
RUNOFF VOLUME (mm) = 32.601
TOTAL RAINFALL (mm) = 89.925
RUNOFF COEFFICIENT = 0.363

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0018)				
(ID= 1 DT= 5.0 min	Area	(ha) =	1.48	
Total Imp(%)= 23.00	Dir. Conn. (%)=			
23.00				

IMPERVIOUS PERVIOUS (i)
Surface Area (ha) = 0.34 1.14
Dep. Storage (mm) = 1.00 5.30

Average Slope (%) =	2.00	5.00
Length (m) =	99.33	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr) =	140.20	56.45
over (min)	5.00	10.00
Storage Coeff. (min) =	1.81 (ii)	8.54 (iii)
Unit Hyd. Tpeak (min) =	5.00	10.00
Unit Hyd. peak (cms) =	0.32	0.12

TOTALS

0.261 (iii)	PEAK FLOW (cms) =	0.13	0.13
	TIME TO PEAK (hrs) =	3.00	3.00

3.00	RUNOFF VOLUME (mm) =	88.92	28.75
------	----------------------	-------	-------

42.59	TOTAL RAINFALL (mm) =	89.93	89.93
-------	-----------------------	-------	-------

89.93	RUNOFF COEFFICIENT =	0.99	0.32
-------	----------------------	------	------

0.47

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
CN* = 60.7 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0019)			
IN= 2--> OUT= 1			
DT= 5.0 min			
STORAGE	OUTFLOW	STORAGE	OUTFLOW
(ha.m.)	(cms)	(ha.m.)	(cms)
	***** WARNING : FIRST OUTFLOW IS NOT ZERO.		
	0.0001	0.0074	0.0165
0.0238		0.0045	0.0089
0.0280		0.0084	0.0111
0.0326			0.0193

	0.0110	0.0137		0.0206	
0.0376		0.0131	0.0166		0.0218
0.0435		0.0149	0.0200		0.0000
0.0000					

PEAK FLOW	(cms)=	0.176 (i)
TIME TO PEAK	(hrs)=	3.083
RUNOFF VOLUME	(mm)=	34.567
TOTAL RAINFALL	(mm)=	89.925
RUNOFF COEFFICIENT	=	0.384

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

R.V.	AREA	QPEAK	TPEAK	
(mm)	(ha)	(cms)	(hrs)	
INFLOW : ID= 2 (0018)	1.480	0.261	3.00	
42.59 OUTFLOW: ID= 1 (0019)	1.480	0.022	4.08	
37.56				

CALIB STANDHYD (0021)	Area	(ha)=	1.28
ID= 1 DT= 5.0 min	Total Imp(%)=	25.00	Dir. Conn.(%)=
25.00			

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.34			
TIME SHIFT OF PEAK FLOW (min)= 65.00			
MAXIMUM STORAGE USED (ha.m.)=			

0.0433

Surface Area	(ha)=	0.32	IMPERVIOUS	0.96
Dep. Storage	(mm)=	1.00		5.80
Average Slope	(%)=	1.00		6.60
Length	(m)=	92.38		100.00
Mannings n	=	0.013		0.250

Max.Eff.Inten.(mm/hr)=	140.20	53.60
over (min)	5.00	15.00
Storage Coeff. (min)=	2.13 (ii)	13.10 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.31	0.08

TOTALS

PEAK FLOW	(cms)=	0.12	0.09
0.200 (iii)	TIME TO PEAK	(hrs)=	3.00
3.00	RUNOFF VOLUME	(mm)=	88.92

44.66 TOTAL RAINFALL	(mm)=	89.93	29.92
89.93 RUNOFF COEFFICIENT	=	0.99	0.33
0.50			

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN* = 62.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0023)	Area	(ha)=	1.40	Curve Number
(CN)= 67.1	Ia	(mm)=	4.60	# of Linear
ID= 1 DT= 5.0 min	Res.(N)=	3.00		
-----	U.H. Tp(hrs)=	0.17		

Unit Hyd Qpeak (cms)= 0.315

+ ID2= 2 (0023):	1.40	0.176	3.08	34.57
=====				
ID = 3 (0024):	2.68	0.268	3.08	37.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0022)	OUTFLOW	STORAGE	OUTFLOW	
IN= 2--> OUT= 1	(cms)	(ha.m.)	(cms)	
DT= 5.0 min	0.0001	0.0052	0.0843	
0.0172	0.0056	0.0066	0.0945	
0.0200	0.0202	0.0082	0.1036	
0.0231	0.0402	0.0101	0.1121	
0.0265	0.0595	0.0122	0.1199	
0.0301	0.0728	0.0146	0.0000	
0.0000				

CALIB NASHYD (0055)	Area	(ha)=	1.24	Curve Number
(CN)= 67.5	Ia	(mm)=	8.20	# of Linear
ID= 1 DT= 5.0 min	Res.(N)=	3.00		
-----	U.H. Tp(hrs)=	0.26		

Unit Hyd Qpeak (cms)= 0.182

PEAK FLOW	(cms)=	0.115 (i)
TIME TO PEAK	(hrs)=	3.167
RUNOFF VOLUME	(mm)=	32.714
TOTAL RAINFALL	(mm)=	89.925
RUNOFF COEFFICIENT	=	0.364

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

R.V.	AREA	QPEAK	TPEAK	
(mm)	(ha)	(cms)	(hrs)	
INFLOW : ID= 2 (0021)	1.280	0.200	3.00	
44.66 OUTFLOW: ID= 1 (0022)	1.280	0.094	3.25	
40.58				

CALIB NASHYD (0056)	Area	(ha)=	0.58	Curve Number
(CN)= 66.1	Ia	(mm)=	4.60	# of Linear
ID= 1 DT= 5.0 min	Res.(N)=	3.00		
-----	U.H. Tp(hrs)=	0.26		

Unit Hyd Qpeak (cms)= 0.085

PEAK FLOW	(cms)=	0.055 (i)
TIME TO PEAK	(hrs)=	3.167
RUNOFF VOLUME	(mm)=	33.746
TOTAL RAINFALL	(mm)=	89.925
RUNOFF COEFFICIENT	=	0.375

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0024)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0022):	1.28	0.094	3.25	40.58

```
*****
** SIMULATION NUMBER: 7 **
*****
```

| CHICAGO STORM | IDF curve parameters: A= 405.000
| Ptotal= 24.91 mm | B= 3.000
C= 0.760
used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 10.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
3.17	2.07	0.17	1.76	1.17	11.75
3.33	1.93	0.33	2.00	1.33	57.66
3.50	1.81	0.50	2.32	1.50	15.20
3.67	1.71	0.67	2.81	1.67	8.31
3.83	1.62	0.83	3.61	1.83	5.91
4.00	1.54	1.00	5.28	2.00	4.66

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
3.08	2.07	0.083	1.76	1.083	11.75
3.17	2.07	0.167	1.76	1.167	11.75
3.25	1.93	0.250	2.00	1.250	57.66
3.33	1.93	0.333	2.00	1.333	57.66
3.42	1.81	0.417	2.32	1.417	15.20
3.50	1.81	0.500	2.32	1.500	15.20
3.58	1.71	0.583	2.81	1.583	8.31
3.67	1.71	0.667	2.81	1.667	8.31
3.75	1.62	0.750	3.61	1.750	5.91
3.83	1.62	0.833	3.61	1.833	5.91
3.92	1.54	0.917	5.28	1.917	4.66
4.00	1.54	1.000	5.28	2.000	4.66

Unit Hyd Qpeak (cms)= 0.247

PEAK FLOW (cms)= 0.004 (i)
TIME TO PEAK (hrs)= 1.667
RUNOFF VOLUME (mm)= 1.518
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.061

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | NASHYD (0002) | Area (ha)= 1.42 Curve Number
(CN)= 63.1
| ID= 1 DT= 5.0 min | Ia (mm)= 9.10 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.22

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

| CALIB | NASHYD (0001) | Area (ha)= 2.02 Curve Number
(CN)= 61.5

| ID= 1 DT= 5.0 min | Ia (mm)= 5.30 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.454

PEAK FLOW (cms)= 0.012 (i)
TIME TO PEAK (hrs)= 1.500
RUNOFF VOLUME (mm)= 2.144
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.086

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB | NASHYD (0015) | Area (ha)= 2.66 Curve Number
(CN)= 64.8
| ID= 1 DT= 5.0 min | Ia (mm)= 4.80 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.598

PEAK FLOW (cms)= 0.019 (i)
TIME TO PEAK (hrs)= 1.500
RUNOFF VOLUME (mm)= 2.548
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.102

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR (0016) | IN= 2--> OUT= 1
| DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW
STORAGE
----- (cms) (ha.m.) | (cms)
(ha.m.)

**** WARNING : FIRST OUTFLOW IS NOT ZERO.
0.0001 0.0072 | 0.1306

0.0171

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
0.0194	0.0065	0.0083	0.1492
0.0220	0.0242	0.0096	0.1656
0.0248	0.0501	0.0112	0.1806
0.0278	0.0806	0.0129	0.1944
0.0000	0.1098	0.0149	0.0000

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
2.55	INFLOW : ID= 2 (0015)	2.660	0.019 1.50
0.03	OUTFLOW: ID= 1 (0016)	2.660	0.000 4.58
0.0067	PEAK FLOW REDUCTION [Qout/Qin](%)= 0.50 TIME SHIFT OF PEAK FLOW (min)= 185.00 MAXIMUM STORAGE USED (ha.m.)=		

| CALIB | NASHYD (0004) | Area (ha)= 2.44 Curve Number
(CN)= 68.8
| ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.17

Unit Hyd Qpeak (cms)= 0.548

PEAK FLOW (cms)= 0.012 (i)
TIME TO PEAK (hrs)= 1.583
RUNOFF VOLUME (mm)= 2.156
TOTAL RAINFALL (mm)= 24.906
RUNOFF COEFFICIENT = 0.087

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----  

| CALIB |  

| NASHYD (0003) | Area (ha)= 1.53 Curve Number  

| (CN)= 61.7 |  

| ID= 1 DT= 5.0 min | Ia (mm)= 8.70 # of Linear  

Res.(N)= 3.00  

----- U.H. Tp(hrs)= 0.17  

Unit Hyd Qpeak (cms)= 0.344  

PEAK FLOW (cms)= 0.005 (i)  

TIME TO PEAK (hrs)= 1.583  

RUNOFF VOLUME (mm)= 1.505  

TOTAL RAINFALL (mm)= 24.906  

RUNOFF COEFFICIENT = 0.060  

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.  

-----  

-----  

| CALIB |  

| NASHYD (0007) | Area (ha)= 0.59 Curve Number  

| (CN)= 65.0 |  

| ID= 1 DT= 5.0 min | Ia (mm)= 4.70 # of Linear  

Res.(N)= 3.00  

----- U.H. Tp(hrs)= 0.17  

Unit Hyd Qpeak (cms)= 0.133  

PEAK FLOW (cms)= 0.004 (i)  

TIME TO PEAK (hrs)= 1.500  

RUNOFF VOLUME (mm)= 2.591  

TOTAL RAINFALL (mm)= 24.906  

RUNOFF COEFFICIENT = 0.104  

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.  

-----  

-----  

| CALIB |  

| STANDHYD (0008) | Area (ha)= 1.48  

| ID= 1 DT= 5.0 min | Total Imp(%)= 23.00 Dir. Conn.()%=  

23.00  

----- IMPERVIOUS PERVIOUS (i)

```

	Surface Area (ha)=	0.34	1.14
Dep. Storage (mm)=	1.00	5.30	
Average Slope (%)=	2.00	5.00	
Length (m)=	99.33	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	57.66	1.95	
over (min)	5.00	30.00	
Storage Coeff. (min)=	2.58 (ii)	28.49 (ii)	
Unit Hyd. Tpeak (min)=	5.00	30.00	
Unit Hyd. peak (cms)=	0.29	0.04	

TOTALS

	PEAK FLOW (cms)=	0.05	0.00
0.054 (iii)	TIME TO PEAK (hrs)=	1.33	1.92
1.33	RUNOFF VOLUME (mm)=	23.91	2.09
7.09	TOTAL RAINFALL (mm)=	24.91	24.91
24.91	RUNOFF COEFFICIENT =	0.96	0.08
0.28			

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
- CN* = 60.7 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

	ADD HYD (0009)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
7.46	1 + 2 = 3				
	ID1= 1 (0007):	0.59	0.004	1.50	2.59
	+ ID2= 2 (0008):	1.48	0.054	1.33	7.09
	ID = 3 (0009):	2.07	0.057	1.33	5.81

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----  

-----  

| CALIB |  

| NASHYD (0011) | Area (ha)= 1.40 Curve Number  

| (CN)= 67.1 |  

| ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear  

Res.(N)= 3.00  

----- U.H. Tp(hrs)= 0.17  

Unit Hyd Qpeak (cms)= 0.315  

PEAK FLOW (cms)= 0.011 (i)  

TIME TO PEAK (hrs)= 1.500  

RUNOFF VOLUME (mm)= 2.836  

TOTAL RAINFALL (mm)= 24.906  

RUNOFF COEFFICIENT = 0.114  

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.  

-----  

-----  

| CALIB |  

| STANDHYD (0010) | Area (ha)= 1.28  

| ID= 1 DT= 5.0 min | Total Imp(%)= 24.60 Dir. Conn.()%=  

24.60  

----- IMPERVIOUS PERVIOUS (i)

```

	RUNOFF VOLUME (mm)=	23.91	2.13
7.46	TOTAL RAINFALL (mm)=	24.91	24.91
24.91	RUNOFF COEFFICIENT =	0.96	0.09
0.30			

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
- CN* = 62.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

	ADD HYD (0012)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
	1 + 2 = 3				
	ID1= 1 (0010):	1.28	0.049	1.33	7.46
	+ ID2= 2 (0011):	1.40	0.011	1.50	2.84
	ID = 3 (0012):	2.68	0.056	1.33	5.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----  

-----  

| CALIB |  

| NASHYD (0005) | Area (ha)= 8.72 Curve Number  

| (CN)= 64.6 |  

| ID= 1 DT= 5.0 min | Ia (mm)= 8.80 # of Linear  

Res.(N)= 3.00  

----- U.H. Tp(hrs)= 0.39  

Unit Hyd Qpeak (cms)= 0.854  

PEAK FLOW (cms)= 0.021 (i)  

TIME TO PEAK (hrs)= 1.917  

RUNOFF VOLUME (mm)= 1.670  

TOTAL RAINFALL (mm)= 24.906  

RUNOFF COEFFICIENT = 0.067

```

	Surface Area (ha)=	0.31	0.97
Dep. Storage (mm)=	1.00	5.80	
Average Slope (%)=	1.00	6.60	
Length (m)=	92.38	100.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	57.66	1.57	
over (min)	5.00	50.00	
Storage Coeff. (min)=	3.04 (ii)	48.01 (ii)	
Unit Hyd. Tpeak (min)=	5.00	50.00	
Unit Hyd. peak (cms)=	0.27	0.02	

TOTALS

PEAK FLOW (cms)=	0.05	0.00	
0.049 (iii)	TIME TO PEAK (hrs)=	1.33	2.33
1.33			

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0013)	Area (ha)=	0.75	Curve Number
	(CN)= 68.1	Ia (mm)=	7.40	# of Linear
	ID= 1 DT= 5.0 min	Res.(N)= 3.00		
			U.H. Tp(hr)=	0.17
		Unit Hyd Qpeak (cms)=	0.169	
		PEAK FLOW (cms)=	0.004 (i)	
		TIME TO PEAK (hrs)=	1.500	
		RUNOFF VOLUME (mm)=	2.237	
		TOTAL RAINFALL (mm)=	24.906	
		RUNOFF COEFFICIENT =	0.090	

Unit Hyd Qpeak (cms)= 0.832

PEAK FLOW (cms)= 0.022 (i)
 TIME TO PEAK (hrs)= 1.917
 RUNOFF VOLUME (mm)= 1.736
 TOTAL RAINFALL (mm)= 24.906
 RUNOFF COEFFICIENT = 0.070

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0014)	Area (ha)=	8.50	Curve Number
	(CN)= 64.4	Ia (mm)=	8.40	# of Linear
	ID= 1 DT= 5.0 min	Res.(N)= 3.00		
			U.H. Tp(hr)=	0.39

Unit Hyd Qpeak (cms)= 0.832

PEAK FLOW (cms)= 0.022 (i)
 TIME TO PEAK (hrs)= 1.917
 RUNOFF VOLUME (mm)= 1.736
 TOTAL RAINFALL (mm)= 24.906
 RUNOFF COEFFICIENT = 0.070

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0017)	Area (ha)=	0.59	Curve Number
	(CN)= 65.0	Ia (mm)=	4.70	# of Linear
	ID= 1 DT= 5.0 min	Res.(N)= 3.00		
			U.H. Tp(hr)=	0.17
		Unit Hyd Qpeak (cms)=	0.133	
		PEAK FLOW (cms)=	0.004 (i)	
		TIME TO PEAK (hrs)=	1.500	
		RUNOFF VOLUME (mm)=	2.591	
		TOTAL RAINFALL (mm)=	24.906	
		RUNOFF COEFFICIENT =	0.104	

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0018)	Area (ha)=	1.48	
	ID= 1 DT= 5.0 min	Total Imp(%)=	23.00	Dir. Conn.(%)=
		23.00		
		IMPERVIOUS Surface Area (ha)=	0.34	PERVIOUS (i)
		Dep. Storage (mm)=	1.00	5.30

Average Slope (%)= 2.00 5.00
 Length (m)= 99.33 40.00
 Mannings n = 0.013 0.250

Max.Eff. Inten. (mm/hr)= 57.66 1.95
 over (min) 5.00 30.00
 Storage Coeff. (min)= 2.58 (ii) 28.49 (ii)
 Unit Hyd. Tpeak (min)= 5.00 30.00
 Unit Hyd. peak (cms)= 0.29 0.04

TOTALS
 PEAK FLOW (cms)= 0.05 0.00
 0.054 (iii)
 TIME TO PEAK (hrs)= 1.33 1.92
 1.33
 RUNOFF VOLUME (mm)= 23.91 2.09
 7.09
 TOTAL RAINFALL (mm)= 24.91 24.91
 24.91
 RUNOFF COEFFICIENT = 0.96 0.08
 0.28

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 60.7 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0019)	OUTFLOW	STORAGE	OUTFLOW
IN= 2--> OUT= 1			
DT= 5.0 min			
STORAGE			
(ha.m.)	(cms)	(ha.m.)	(cms)
	0.0001	0.0074	0.0165
0.0238	0.0045	0.0089	0.0180
0.0280	0.0084	0.0111	0.0193
0.0326			

***** WARNING : FIRST OUTFLOW IS NOT ZERO.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0020)	AREA	QPEAK	TPEAK	R.V.	
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)	
	ID1= 1 (0017):	0.59	0.004	1.50	2.59
	+ ID2= 2 (0019):	1.48	0.003	3.50	2.06
	ID = 3 (0020):	2.07	0.004	1.50	2.21

| CALIB

| NASHYD (0023)

| Area (ha)= 1.40 Curve Number

| (CN)= 67.1

| ID= 1 DT= 5.0 min |

Res.(N)= 3.00

U.H. Tp(hr)= 0.17

Unit Hyd Qpeak (cms)= 0.315

PEAK FLOW (cms) = 0.011 (i)
 TIME TO PEAK (hrs) = 1.500
 RUNOFF VOLUME (mm) = 2.836
 TOTAL RAINFALL (mm) = 24.906
 RUNOFF COEFFICIENT = 0.114

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)	1.28
STANDHYD (0021)	Total Imp(%)	25.00
ID= 1 DT= 5.0 min	Dir. Conn. (%)	
25.00		

Surface Area (ha)	0.32	IMPERVIOUS	0.96	PERVIOUS (i)
Dep. Storage (mm)	1.00		5.80	
Average Slope (%)	1.00		6.60	
Length (m)	92.38		100.00	
Mannings n	= 0.013		0.250	
Max.Eff.Inten.(mm/hr)	57.66		1.57	
over (min)	5.00		50.00	
Storage Coeff. (min)	3.04 (ii)		48.01 (ii)	
Unit Hyd. Tpeak (min)	5.00		50.00	
Unit Hyd. peak (cms)	0.27		0.02	

TOTALS				
PEAK FLOW (cms)	= 0.05		0.00	
TIME TO PEAK (hrs)	= 1.33		2.33	
RUNOFF VOLUME (mm)	= 23.91		2.13	
TOTAL RAINFALL (mm)	= 24.91		24.91	
RUNOFF COEFFICIENT	= 0.96		0.09	
0.30				

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 62.5 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.

RESERVOIR (0022)	IN= 2--> OUT= 1	DT= 5.0 min	OUTFLOW	STORAGE	OUTFLOW
STORAGE			(cms)	(ha.m.)	(cms)
(ha.m.)					

***** WARNING : FIRST OUTFLOW IS NOT ZERO.
 0.0001 0.0052 | 0.0843
 0.0172 0.0056 0.0066 | 0.0945
 0.0200 0.0202 0.0082 | 0.1036
 0.0231 0.0402 0.0101 | 0.1121
 0.0265 0.0595 0.0122 | 0.1199
 0.0301 0.0728 0.0146 | 0.0000

R.V.	AREA	QPEAK	TPEAK
(mm)	(ha)	(cms)	(hrs)
INFLOW : ID= 2 (0021)	1.280	0.050	1.33
7.55 OUTFLOW: ID= 1 (0022)	1.280	0.004	2.75
3.46			

PEAK FLOW REDUCTION [Qout/Qin](%) = 8.63
 TIME SHIFT OF PEAK FLOW (min) = 85.00
 MAXIMUM STORAGE USED (ha.m.) =

0.0063

ADD HYD (0024)	1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0022):		1.28	0.004	2.75	3.46

+ ID2= 2 (0023): 1.40 0.011 1.50 2.84
 ======
 ID = 3 (0024): 2.68 0.011 1.50 3.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

CALIB	Area (ha)	1.24	Curve Number
NASHYD (0055)	(CN)	67.5	
ID= 1 DT= 5.0 min Ia (mm)	= 8.20	# of Linear	
Res.(N)= 3.00			
-----	U.H. Tp(hrs)	= 0.26	

Unit Hyd Qpeak (cms) = 0.182

PEAK FLOW (cms) = 0.005 (i)
 TIME TO PEAK (hrs) = 1.667
 RUNOFF VOLUME (mm) = 2.006
 TOTAL RAINFALL (mm) = 24.906
 RUNOFF COEFFICIENT = 0.081

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)	0.58	Curve Number
NASHYD (0056)	(CN)	66.1	
ID= 1 DT= 5.0 min Ia (mm)	= 4.60	# of Linear	
Res.(N)= 3.00			
-----	U.H. Tp(hrs)	= 0.26	

Unit Hyd Qpeak (cms) = 0.085

PEAK FLOW (cms) = 0.003 (i)
 TIME TO PEAK (hrs) = 1.667
 RUNOFF VOLUME (mm) = 2.735
 TOTAL RAINFALL (mm) = 24.906
 RUNOFF COEFFICIENT = 0.110

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Appendix C

Stormwater Facility Design



3.3.2 Water Quality Sizing Criteria

The volumetric water quality criteria are presented in Table 3.2. The values are based on a 24 hour drawdown time and a design which conforms to the guidance provided in this manual. Requirements differ with SWMP type to reflect differences in removal efficiencies. Of the specified storage volume for wet facilities, 40 m³/ha is extended detention, while the remainder represents the permanent pool.

Table 3.2 Water Quality Storage Requirements based on Receiving Waters^{1, 2}

Protection Level	SWMP Type	Storage Volume (m ³ /ha) for Impervious Level			
		35%	55%	70%	85%
<i>Enhanced</i> 80% long-term S.S. removal	Infiltration	25	30	35	40
	Wetlands	80	105	120	140
	Hybrid Wet Pond/Wetland	110	150	175	195
	Wet Pond	140	190	225	250
<i>Normal</i> 70% long-term S.S. removal	Infiltration	20	20	25	30
	Wetlands	60	70	80	90
	Hybrid Wet Pond/Wetland	75	90	105	120
	Wet Pond	90	110	130	150
<i>Basic</i> 60% long-term S.S. removal	Infiltration	20	20	20	20
	Wetlands	60	60	60	60
	Hybrid Wet Pond/Wetland	60	70	75	80
	Wet Pond	60	75	85	95
	Dry Pond (Continuous Flow)	90	150	200	240

¹Table 3.2 does not include every available SWMP type. Any SWMP type that can be demonstrated to the approval agencies to meet the required long-term suspended solids removal for the selected protection levels under the conditions of the site is acceptable for water quality objectives. The sizing for these SWMP types is to be determined based on performance results that have been peer-reviewed. The designer and those who review the design should be fully aware of the assumptions and sampling methodologies used in formulating performance predictions and their implications for the design.

²Hybrid Wet Pond/Wetland systems have 50-60% of their permanent pool volume in deeper portions of the facility (e.g., forebay, wet pond).

Stage-Storage-Discharge: PR-100 Roadside Ditch



Project No: 19-10874
Project Name: Life at the Woodland
Designed/Checked By: MW / CPB
Date: February 23, 2022

Storage Summary		
Top of Dead Storage:	1.00	m
Dead Storage Volume:	71.6	m ³
Active Storage Volume:	206.5	m ³

Discharge Summary			
Stage	Type	Invert Elev (m)	Diameter / Width (mm) (m)
1	Orifice Tube: Vertical	1.00	325

Outlet Capacity Summary			
Type	Diameter	Slope	Peak Flow % Full

Stage-Storage-Discharge Summary Table

Elevation m	Stage m	Stage 1 Orifice Tube	m³/s				Total Storage ha*m	Total Discharge m³/s	Notes
1.00	0.00	0.000					0.0072	0.000	
1.01	0.01	0.000					0.0073	0.000	
1.02	0.02	0.001					0.0075	0.001	
1.03	0.03	0.002					0.0077	0.002	
1.04	0.04	0.003					0.0079	0.003	
1.05	0.05	0.005					0.0081	0.005	
1.06	0.06	0.006					0.0083	0.006	
1.07	0.07	0.009					0.0085	0.009	
1.08	0.08	0.011					0.0087	0.011	
1.09	0.09	0.014					0.0089	0.014	
1.10	0.10	0.017					0.0091	0.017	
1.11	0.11	0.021					0.0094	0.021	<= 2 Yr: 93 m ³ (1.11m)
1.12	0.12	0.024					0.0096	0.024	
1.13	0.13	0.028					0.0099	0.028	
1.14	0.14	0.032					0.0101	0.032	
1.15	0.15	0.036					0.0104	0.036	
1.16	0.16	0.041					0.0106	0.041	
1.17	0.17	0.045					0.0109	0.045	
1.18	0.18	0.050					0.0112	0.050	
1.19	0.19	0.055					0.0115	0.055	
1.20	0.20	0.060					0.0117	0.060	
1.21	0.21	0.065					0.0120	0.065	
1.22	0.22	0.070					0.0123	0.070	<= 5 Yr: 123 m ³ (1.22m)
1.23	0.23	0.075					0.0126	0.075	
1.24	0.24	0.081					0.0129	0.081	
1.25	0.25	0.086					0.0133	0.086	
1.26	0.26	0.091					0.0136	0.091	
1.27	0.27	0.096					0.0139	0.096	
1.28	0.28	0.101					0.0142	0.101	
1.29	0.29	0.105					0.0146	0.105	
1.30	0.30	0.110					0.0149	0.110	<= 10 Yr: 146 m ³ (1.3m)
1.31	0.31	0.114					0.0153	0.114	
1.32	0.32	0.117					0.0156	0.117	
1.33	0.33	0.120					0.0160	0.120	
1.34	0.34	0.124					0.0163	0.124	
1.35	0.35	0.127					0.0167	0.127	
1.36	0.36	0.131					0.0171	0.131	
1.37	0.37	0.134					0.0175	0.134	
1.38	0.38	0.137					0.0178	0.137	
1.39	0.39	0.140					0.0182	0.140	
1.40	0.40	0.143					0.0186	0.143	<= 25 Yr: 185 m ³ (1.4m)
1.41	0.41	0.146					0.0190	0.146	
1.42	0.42	0.149					0.0194	0.149	
1.43	0.43	0.152					0.0199	0.152	
1.44	0.44	0.155					0.0203	0.155	
1.45	0.45	0.158					0.0207	0.158	
1.46	0.46	0.160					0.0211	0.160	
1.47	0.47	0.163					0.0216	0.163	
1.48	0.48	0.166					0.0220	0.166	<= 50 Yr: 220 m ³ (1.48m)

Stage-Storage-Discharge Summary Table									
Elevation	Stage	Stage 1 Orifice Tube					Total Storage	Total Discharge	
m	m	m³/s					ha*m	m³/s	Notes
1.49	0.49	0.168					0.0225	0.168	
1.50	0.50	0.171					0.0229	0.171	
1.51	0.51	0.173					0.0234	0.173	
1.52	0.52	0.176					0.0239	0.176	
1.53	0.53	0.178					0.0243	0.178	
1.54	0.54	0.181					0.0248	0.181	
1.55	0.55	0.183					0.0253	0.183	
1.56	0.56	0.185					0.0258	0.185	
1.57	0.57	0.188					0.0263	0.188	<= 100 Yr: 261 m³ (1.57m)
1.58	0.58	0.190					0.0268	0.190	
1.59	0.59	0.192					0.0273	0.192	
1.60	0.60	0.194					0.0278	0.194	

Stage-Storage-Discharge: PR-102 Roadside Ditch



Project No: 19-10874
Project Name: Life at the Woodland
Designed/Checked By: MW / CPB
Date: February 23, 2022

Storage Summary		
Top of Dead Storage:	1.00	m
Dead Storage Volume:	78.3	m³
Active Storage Volume:	356.7	m³

Discharge Summary			
Stage	Type	Invert Elev (m)	Diameter / Width (mm) (m)
1	Orifice Tube: Vertical	1.00	95

Outlet Capacity Summary			
Type	Diameter	Slope	Peak Flow % Full

Stage-Storage-Discharge Summary Table

Elevation m	Stage m	Stage 1 Orifice Tube					Total Storage	Total Discharge	Notes
							ha*m	m³/s	
1.00	0.00	0.000					0.0074	0.000	
1.01	0.01	0.000					0.0073	0.000	
1.02	0.02	0.000					0.0075	0.000	
1.03	0.03	0.001					0.0077	0.001	
1.04	0.04	0.001					0.0080	0.001	
1.05	0.05	0.002					0.0082	0.002	
1.06	0.06	0.003					0.0084	0.003	
1.07	0.07	0.004					0.0086	0.004	<= 25 mm: 85 m³ (1.07m)
1.08	0.08	0.005					0.0089	0.005	
1.09	0.09	0.005					0.0091	0.005	
1.10	0.10	0.006					0.0094	0.006	
1.11	0.11	0.006					0.0097	0.006	
1.12	0.12	0.007					0.0099	0.007	
1.13	0.13	0.007					0.0102	0.007	
1.14	0.14	0.008					0.0105	0.008	
1.15	0.15	0.008					0.0108	0.008	
1.16	0.16	0.008					0.0111	0.008	
1.17	0.17	0.009					0.0114	0.009	
1.18	0.18	0.009					0.0117	0.009	
1.19	0.19	0.009					0.0120	0.009	
1.20	0.20	0.010					0.0123	0.010	<= 2 Yr: 125 m³ (1.21m)
1.21	0.21	0.010					0.0126	0.010	
1.22	0.22	0.010					0.0130	0.010	
1.23	0.23	0.011					0.0133	0.011	
1.24	0.24	0.011					0.0137	0.011	
1.25	0.25	0.011					0.0140	0.011	
1.26	0.26	0.012					0.0144	0.012	
1.27	0.27	0.012					0.0147	0.012	
1.28	0.28	0.012					0.0151	0.012	
1.29	0.29	0.012					0.0155	0.012	
1.30	0.30	0.013					0.0158	0.013	
1.31	0.31	0.013					0.0162	0.013	
1.32	0.32	0.013					0.0166	0.013	
1.33	0.33	0.013					0.0170	0.013	
1.34	0.34	0.014					0.0174	0.014	
1.35	0.35	0.014					0.0178	0.014	
1.36	0.36	0.014					0.0183	0.014	
1.37	0.37	0.014					0.0187	0.014	
1.38	0.38	0.014					0.0191	0.014	<= 5 Yr: 190 m³ (1.38m)
1.39	0.39	0.015					0.0196	0.015	
1.40	0.40	0.015					0.0200	0.015	
1.41	0.41	0.015					0.0204	0.015	
1.42	0.42	0.015					0.0209	0.015	
1.43	0.43	0.016					0.0214	0.016	
1.44	0.44	0.016					0.0218	0.016	
1.45	0.45	0.016					0.0223	0.016	
1.46	0.46	0.016					0.0228	0.016	
1.47	0.47	0.016					0.0233	0.016	
1.48	0.48	0.017					0.0238	0.017	

Stage-Storage-Discharge Summary Table									
Elevation	Stage	Stage 1 Orifice Tube					Total Storage	Total Discharge	
m	m	m³/s					ha*m	m³/s	Notes
1.49	0.49	0.017					0.0243	0.017	<= 10 Yr: 241 m³ (1.49m)
1.50	0.50	0.017					0.0248	0.017	
1.51	0.51	0.017					0.0253	0.017	
1.52	0.52	0.017					0.0258	0.017	
1.53	0.53	0.017					0.0263	0.017	
1.54	0.54	0.018					0.0269	0.018	
1.55	0.55	0.018					0.0274	0.018	
1.56	0.56	0.018					0.0280	0.018	
1.57	0.57	0.018					0.0285	0.018	
1.58	0.58	0.018					0.0291	0.018	
1.59	0.59	0.019					0.0296	0.019	
1.60	0.60	0.019					0.0302	0.019	
1.61	0.61	0.019					0.0308	0.019	
1.62	0.62	0.019					0.0314	0.019	<= 25 Yr: 313 m³ (1.62m)
1.63	0.63	0.019					0.0320	0.019	
1.64	0.64	0.019					0.0326	0.019	
1.65	0.65	0.019					0.0332	0.019	
1.66	0.66	0.020					0.0338	0.020	
1.67	0.67	0.020					0.0344	0.020	
1.68	0.68	0.020					0.0350	0.020	
1.69	0.69	0.020					0.0356	0.020	
1.70	0.70	0.020					0.0363	0.020	
1.71	0.71	0.020					0.0369	0.020	
1.72	0.72	0.021					0.0376	0.021	<= 50 Yr: 372 m³ (1.72m)
1.73	0.73	0.021					0.0382	0.021	
1.74	0.74	0.021					0.0389	0.021	
1.75	0.75	0.021					0.0396	0.021	
1.76	0.76	0.021					0.0402	0.021	
1.77	0.77	0.021					0.0409	0.021	
1.78	0.78	0.021					0.0416	0.021	
1.79	0.79	0.022					0.0425	0.022	
1.80	0.80	0.022					0.0435	0.022	<= 100 Yr: 433 m³ (1.8m)

Stage-Storage-Discharge: PR-201 Roadside Ditch



Project No: 19-10874
Project Name: Life at the Woodland
Designed/Checked By: MW / CPB
Date: February 23, 2022

Storage Summary		
Top of Dead Storage:	1.00	m
Dead Storage Volume:	51.9	m ³
Active Storage Volume:	248.7	m ³

Discharge Summary			
Stage	Type	Invert Elev (m)	Diameter / Width (mm) (m)
1	Orifice Tube: Vertical	1.00	250

Outlet Capacity Summary			
Type	Diameter	Slope	Peak Flow % Full

Stage-Storage-Discharge Summary Table

Elevation m	Stage m	Stage 1 Orifice Tube					Total Storage ha*m	Total Discharge m ³ /s	Notes
1.00	0.00	0.000					0.0052	0.000	
1.01	0.01	0.000					0.0054	0.000	
1.02	0.02	0.001					0.0056	0.001	
1.03	0.03	0.001					0.0058	0.001	
1.04	0.04	0.003					0.0061	0.003	
1.05	0.05	0.004					0.0063	0.004	
1.06	0.06	0.006					0.0066	0.006	
1.07	0.07	0.007					0.0068	0.007	
1.08	0.08	0.010					0.0071	0.010	
1.09	0.09	0.012					0.0074	0.012	
1.10	0.10	0.015					0.0076	0.015	
1.11	0.11	0.017					0.0079	0.017	
1.12	0.12	0.020					0.0082	0.020	<= 25 mm: 63 m ³ (1.05m)
1.13	0.13	0.023					0.0085	0.023	
1.14	0.14	0.027					0.0088	0.027	
1.15	0.15	0.030					0.0091	0.030	
1.16	0.16	0.033					0.0094	0.033	
1.17	0.17	0.037					0.0097	0.037	
1.18	0.18	0.040					0.0101	0.040	
1.19	0.19	0.044					0.0104	0.044	
1.20	0.20	0.047					0.0108	0.047	<= 5 Yr: 105 m ³ (1.2m)
1.21	0.21	0.051					0.0111	0.051	
1.22	0.22	0.054					0.0115	0.054	
1.23	0.23	0.057					0.0118	0.057	
1.24	0.24	0.059					0.0122	0.059	
1.25	0.25	0.061					0.0126	0.061	<= 10 Yr: 122 m ³ (1.25m)
1.26	0.26	0.064					0.0130	0.064	
1.27	0.27	0.066					0.0133	0.066	
1.28	0.28	0.068					0.0137	0.068	
1.29	0.29	0.071					0.0141	0.071	
1.30	0.30	0.073					0.0146	0.073	<= 25 Yr: 144 m ³ (1.3m)
1.31	0.31	0.075					0.0150	0.075	
1.32	0.32	0.077					0.0154	0.077	
1.33	0.33	0.079					0.0158	0.079	
1.34	0.34	0.081					0.0163	0.081	
1.35	0.35	0.083					0.0167	0.083	
1.36	0.36	0.084					0.0172	0.084	
1.37	0.37	0.086					0.0176	0.086	<= 50 Yr: 174 m ³ (1.37m)
1.38	0.38	0.088					0.0181	0.088	
1.39	0.39	0.090					0.0186	0.090	
1.40	0.40	0.091					0.0190	0.091	
1.41	0.41	0.093					0.0195	0.093	
1.42	0.42	0.094					0.0200	0.094	<= 100 Yr: 200 m ³ (1.42m)
1.43	0.43	0.096					0.0205	0.096	
1.44	0.44	0.098					0.0210	0.098	
1.45	0.45	0.099					0.0215	0.099	
1.46	0.46	0.101					0.0221	0.101	
1.47	0.47	0.102					0.0226	0.102	
1.48	0.48	0.104					0.0231	0.104	

Stage-Storage-Discharge Summary Table									
Elevation	Stage	Stage 1 Orifice Tube					Total Storage	Total Discharge	
m	m	m³/s					ha*m	m³/s	Notes
1.49	0.49	0.105					0.0237	0.105	
1.50	0.50	0.107					0.0242	0.107	
1.51	0.51	0.108					0.0248	0.108	
1.52	0.52	0.109					0.0253	0.109	
1.53	0.53	0.111					0.0259	0.111	
1.54	0.54	0.112					0.0265	0.112	
1.55	0.55	0.113					0.0270	0.113	
1.56	0.56	0.115					0.0276	0.115	
1.57	0.57	0.116					0.0282	0.116	
1.58	0.58	0.117					0.0288	0.117	
1.59	0.59	0.119					0.0294	0.119	
1.60	0.60	0.120					0.0301	0.120	

Appendix D

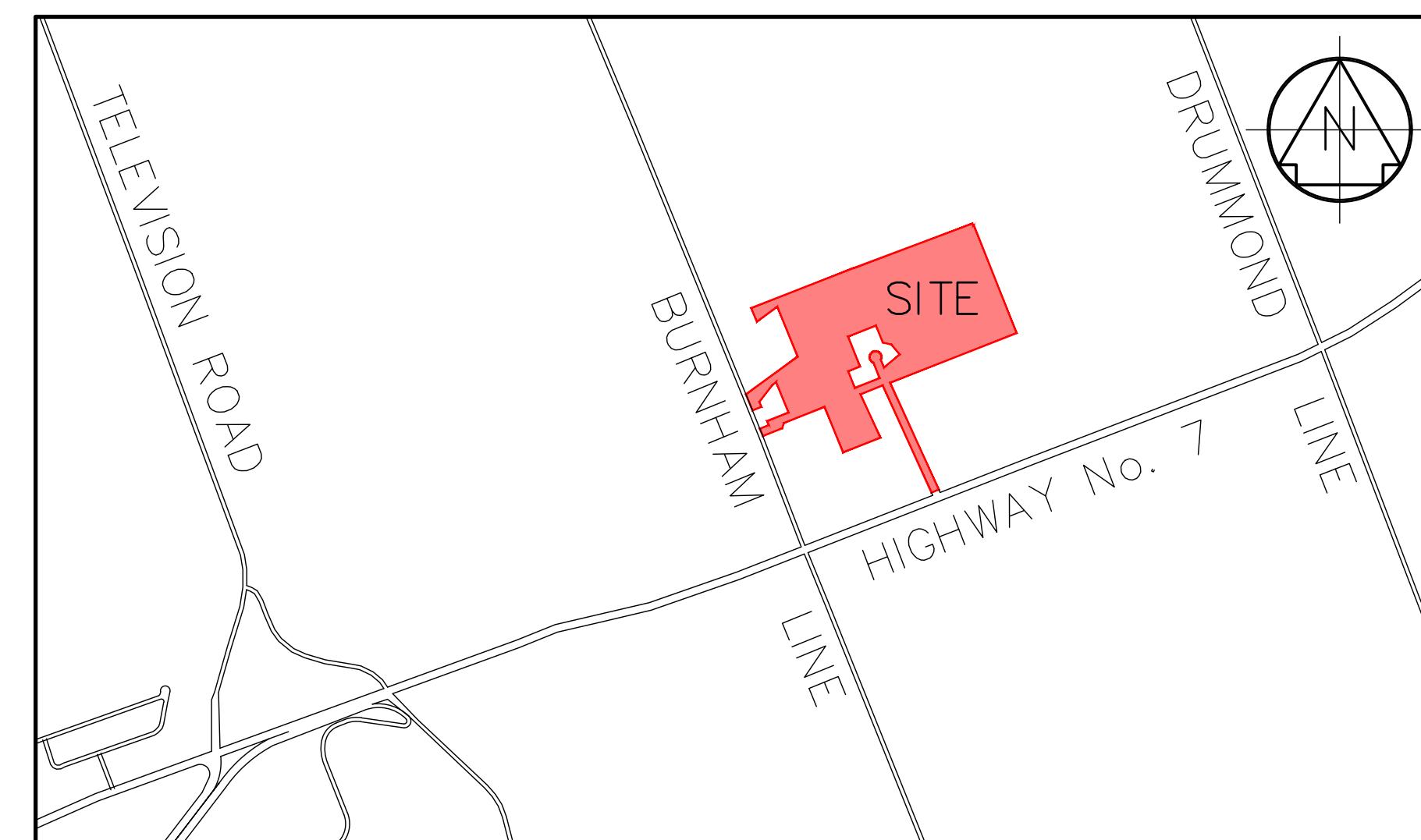
Drawings



LIFE AT THE WOODLAND SUBDIVISION

OTONabee-SOUTH MONAGHAN
TOWNSHIP OF OTONabee-SOUTH MONAGHAN, ONTARIO

WILLS PROJECT No. 19-10874

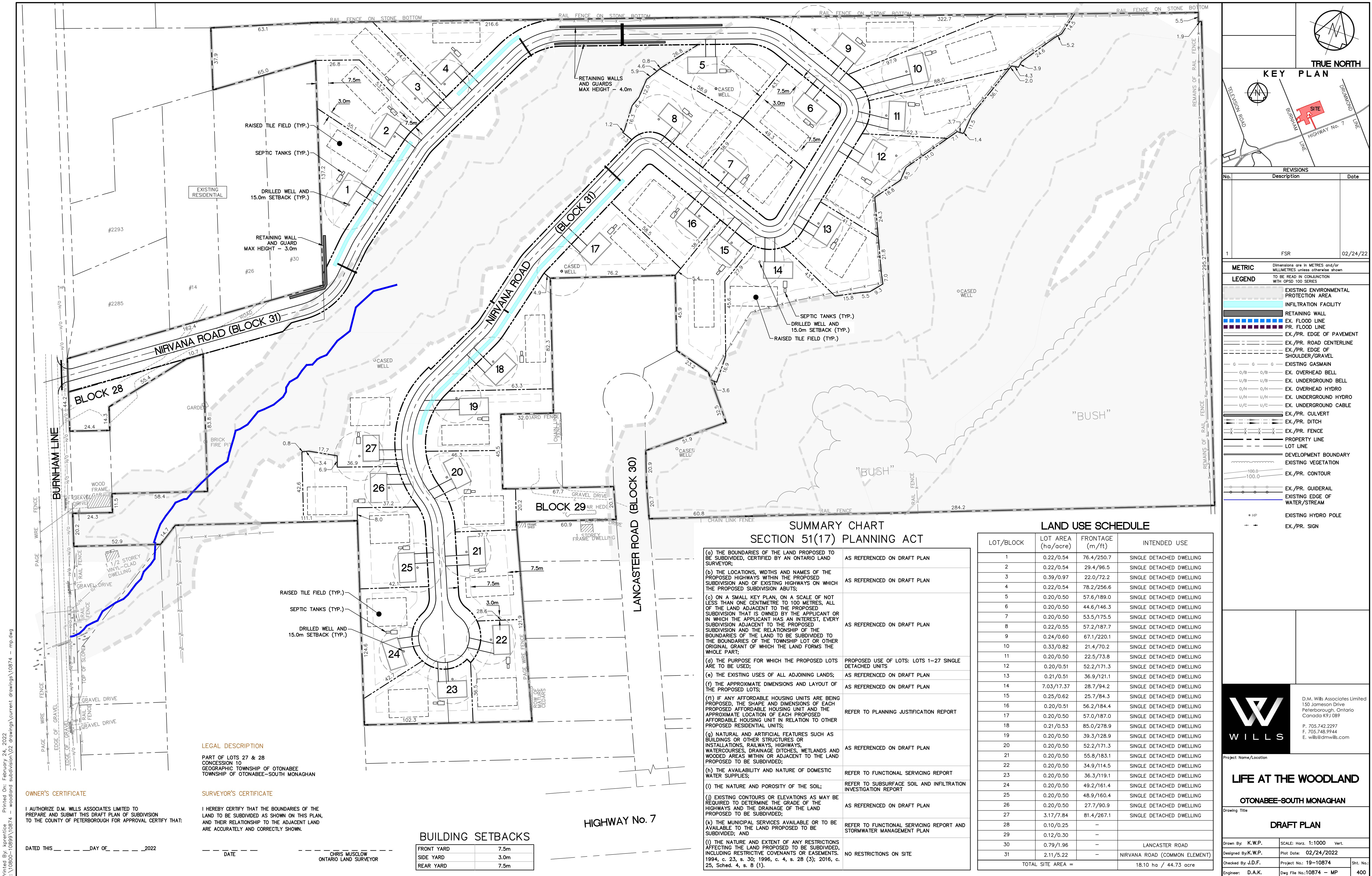


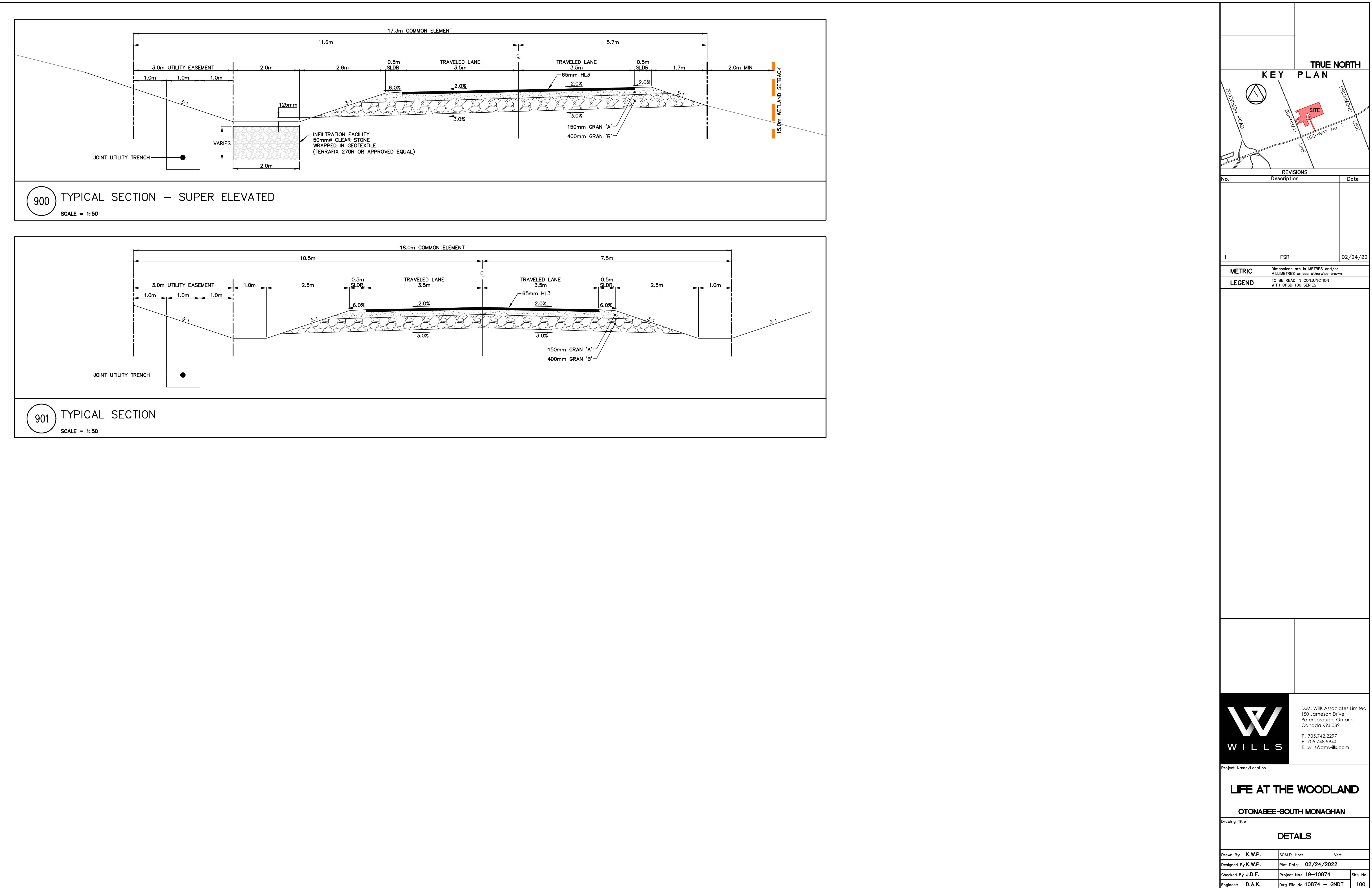
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101	DETAILS	0	02/24/2022
400	PLAN PROFILE STA: 0+000 – 0+060	0	02/24/2022
401	PLAN PROFILE STA: 0+060 – 0+140	0	02/24/2022
402	PLAN PROFILE STA: 0+140 – 0+300	0	02/24/2022
403	PLAN PROFILE STA: 0+300 – 0+460	0	02/24/2022
404	PLAN PROFILE STA: 0+460 – 0+560	0	02/24/2022
405	PLAN PROFILE STA: 0+560 – 0+680	0	02/24/2022
406	PLAN PROFILE STA: 0+680 – 0+760	0	02/24/2022
407	PLAN PROFILE STA: 0+760 – 0+920	0	02/24/2022
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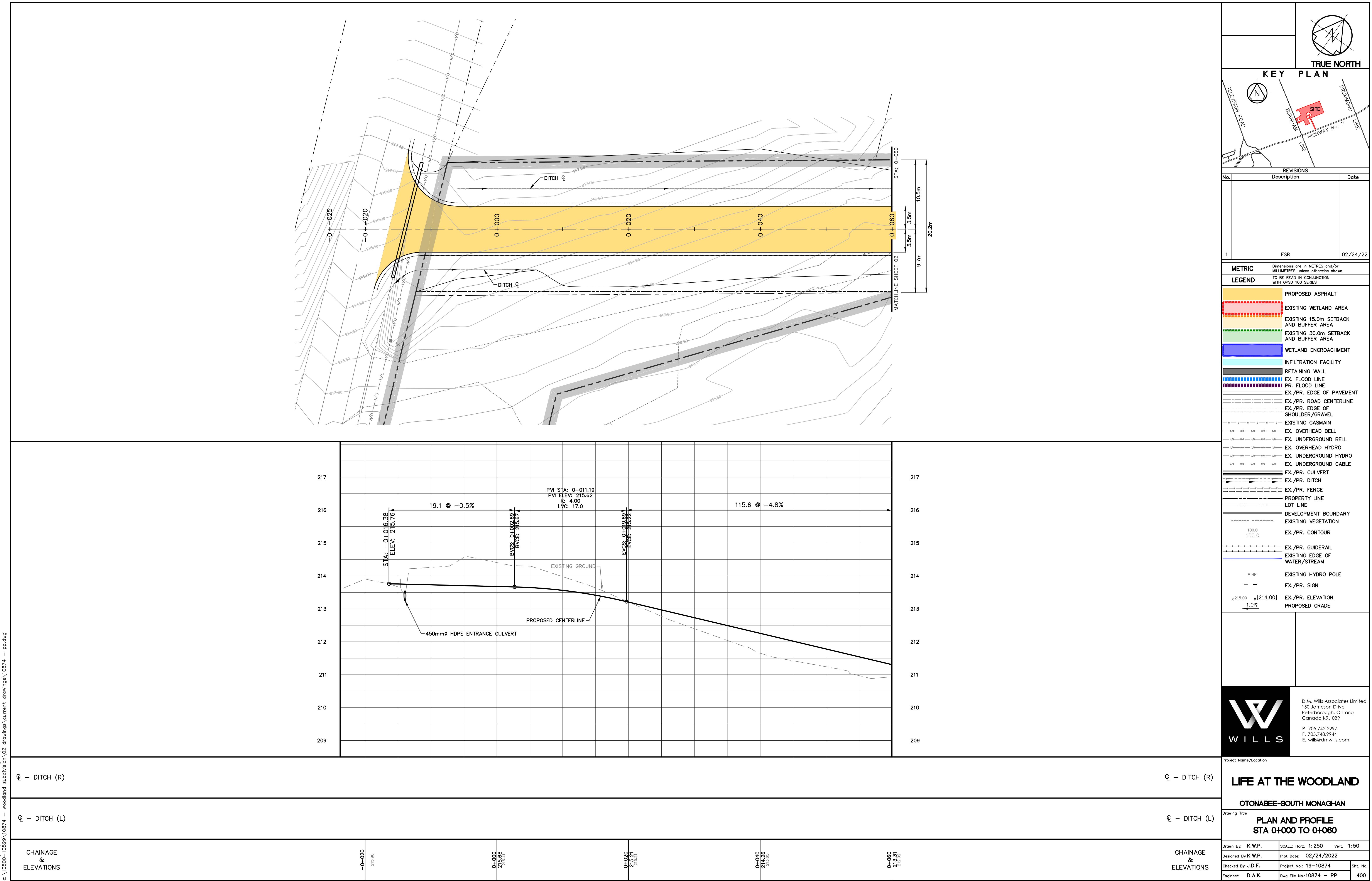
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150 Jameson Drive
Peterborough, Ontario
Canada K9J 0B9

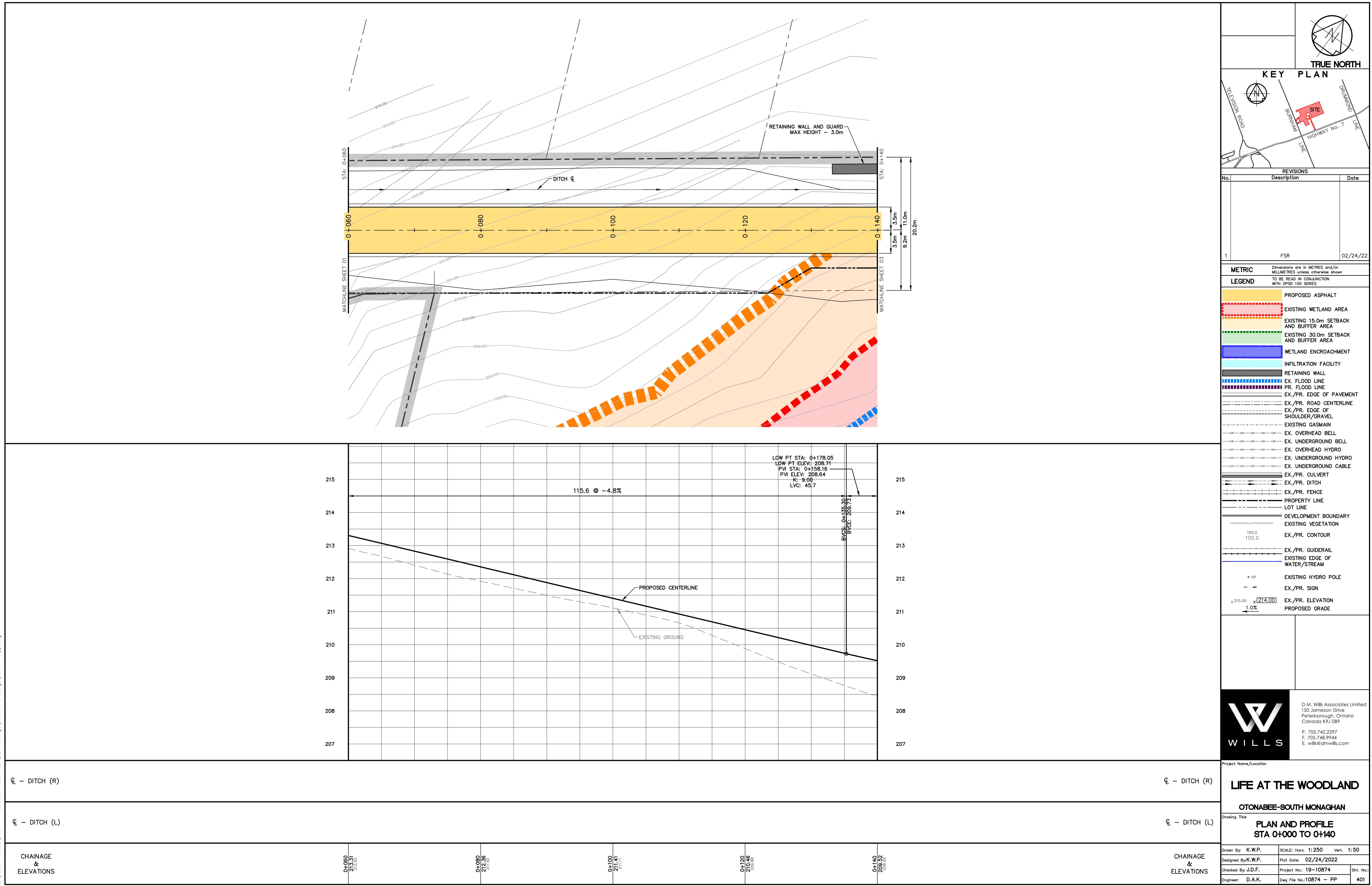
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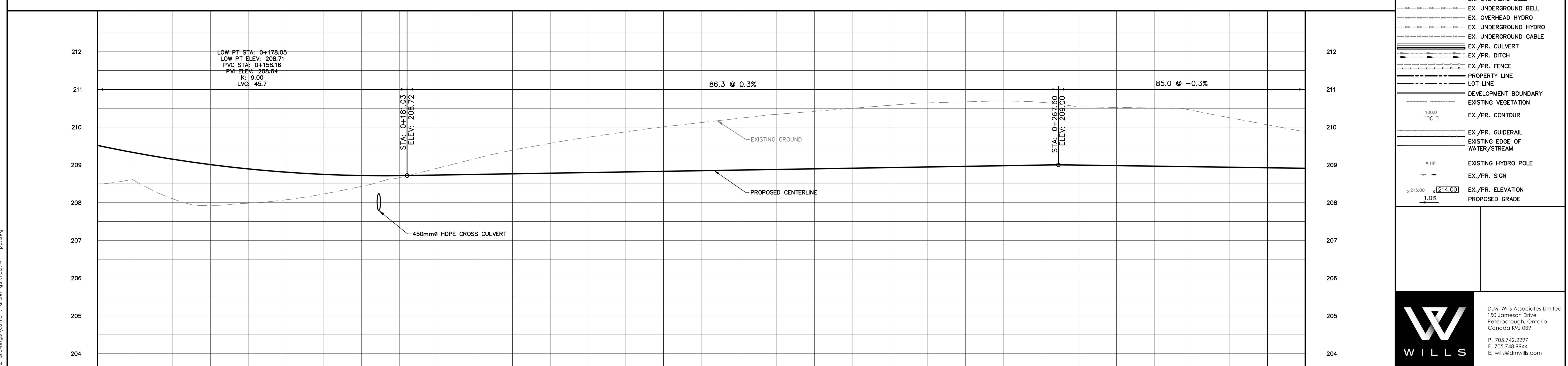
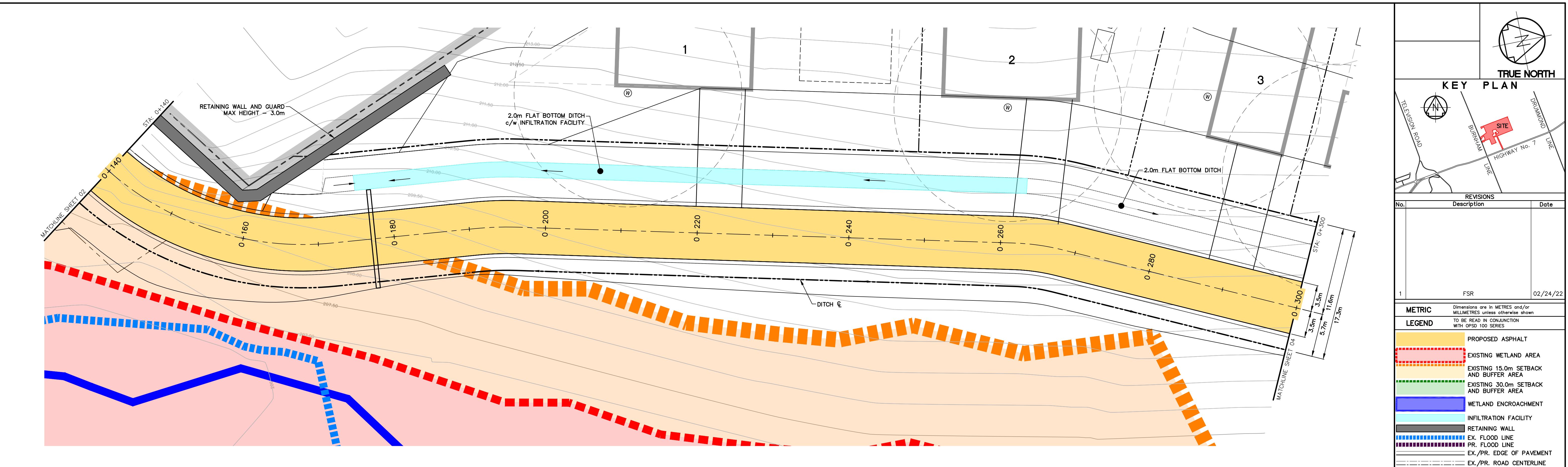












¢ - DITCH (R)

¢ - DITCH (R)

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¢ - DITCH (L)

CHAINAGE & ELEVATIONS

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208.98

0+160
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208.56

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208.56

0+200
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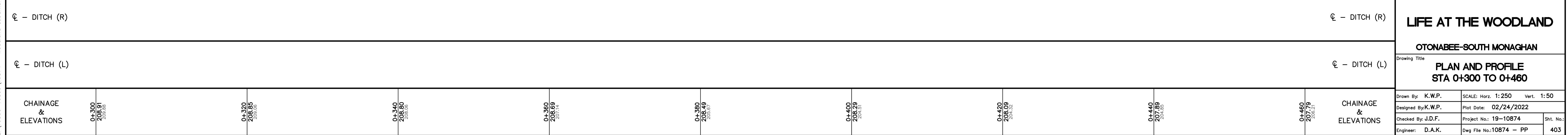
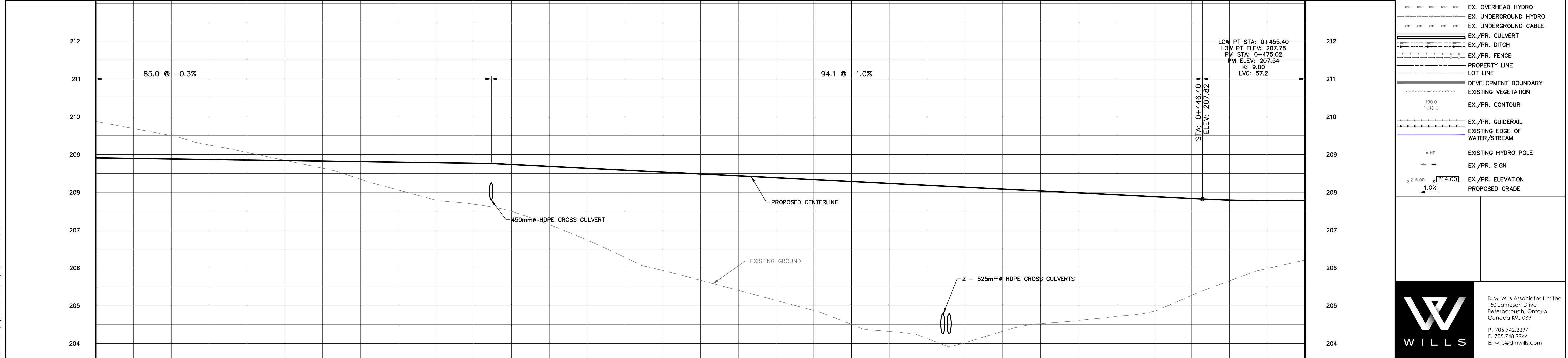
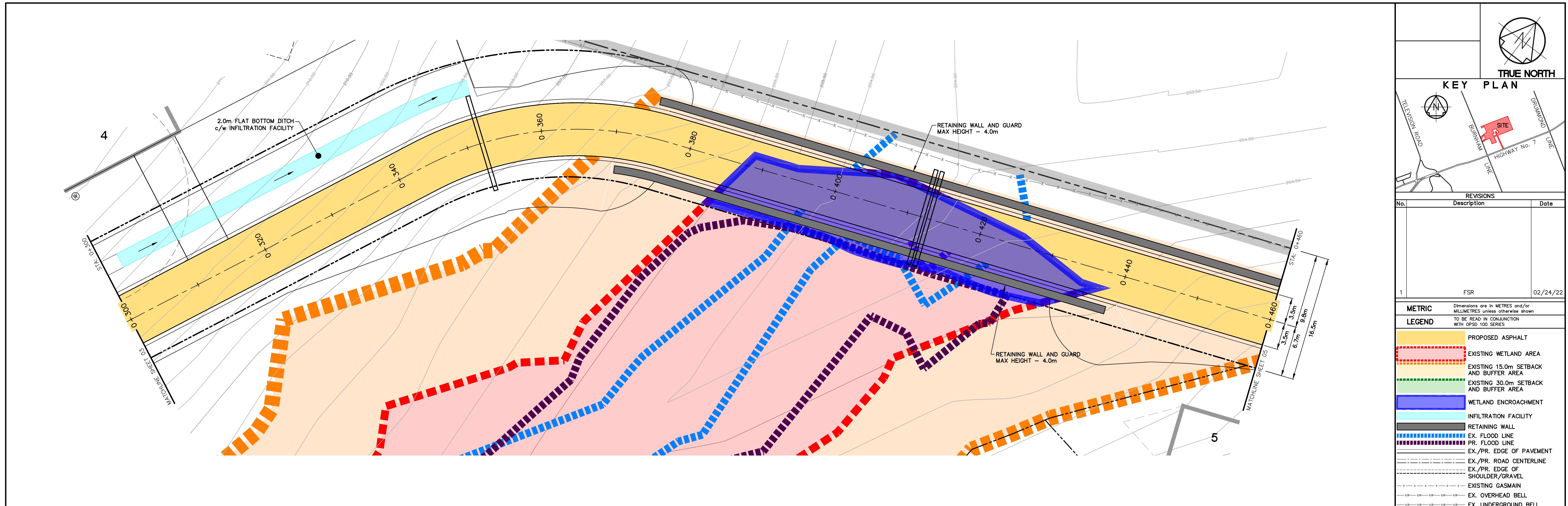
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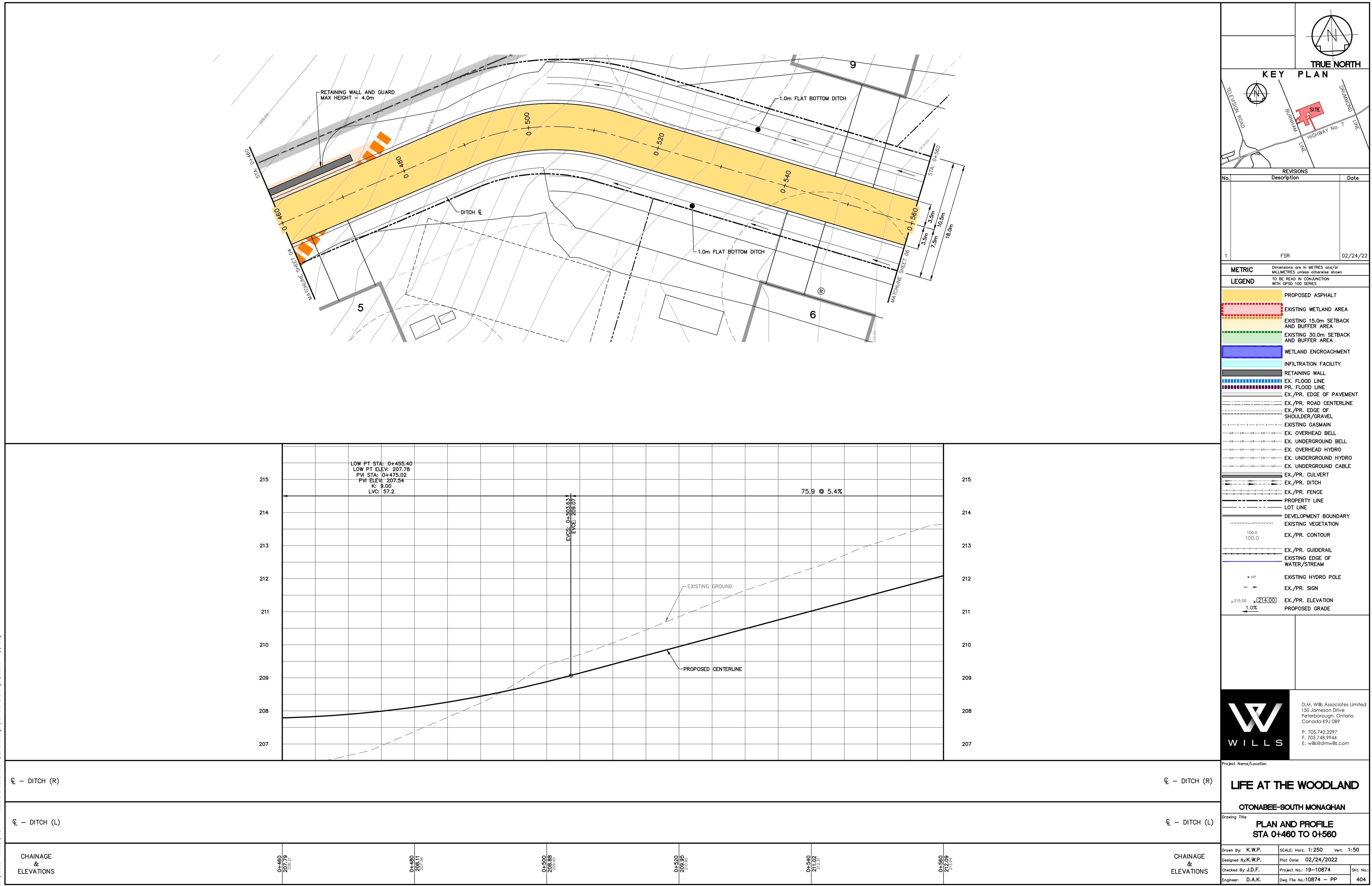
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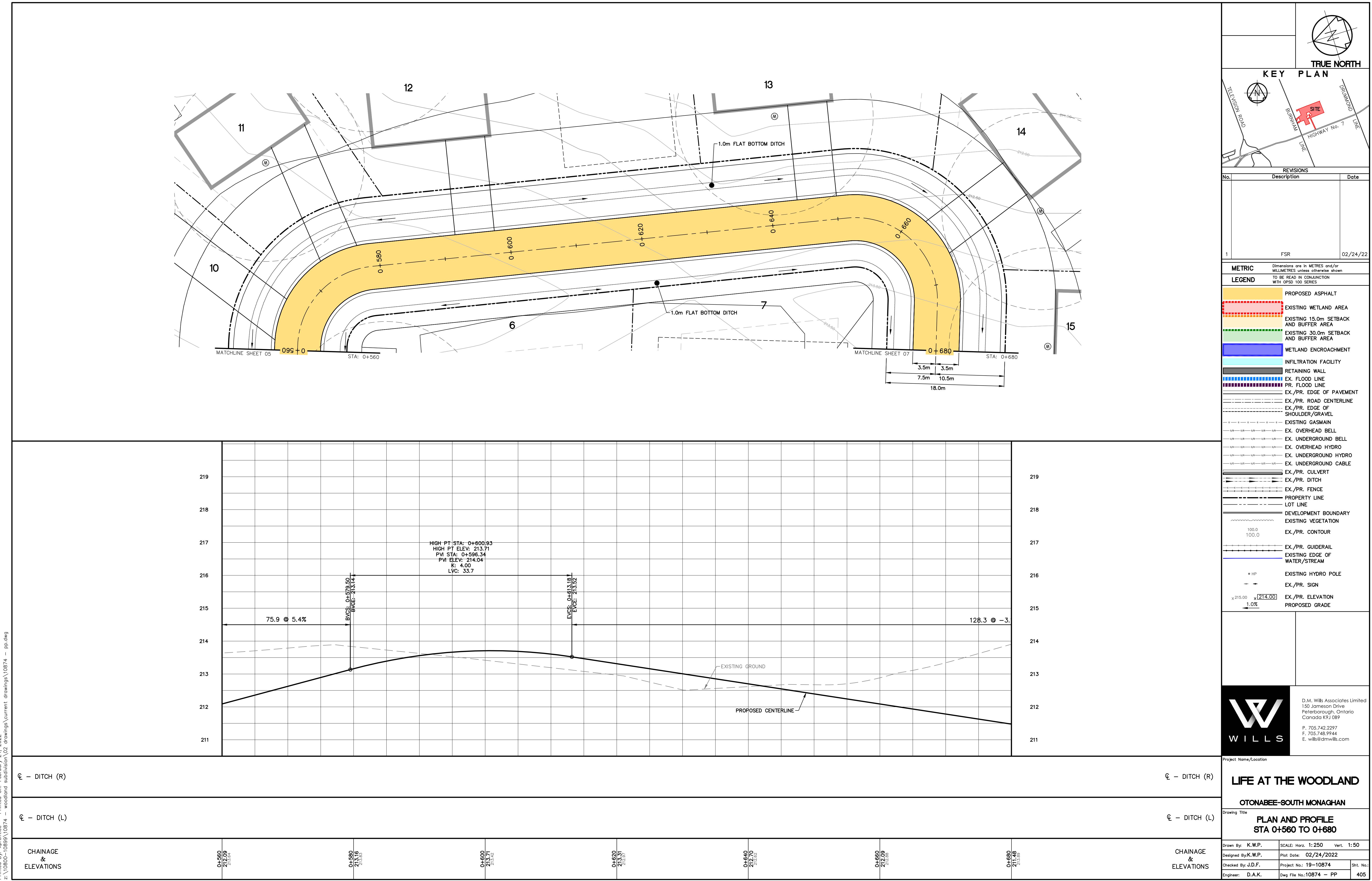
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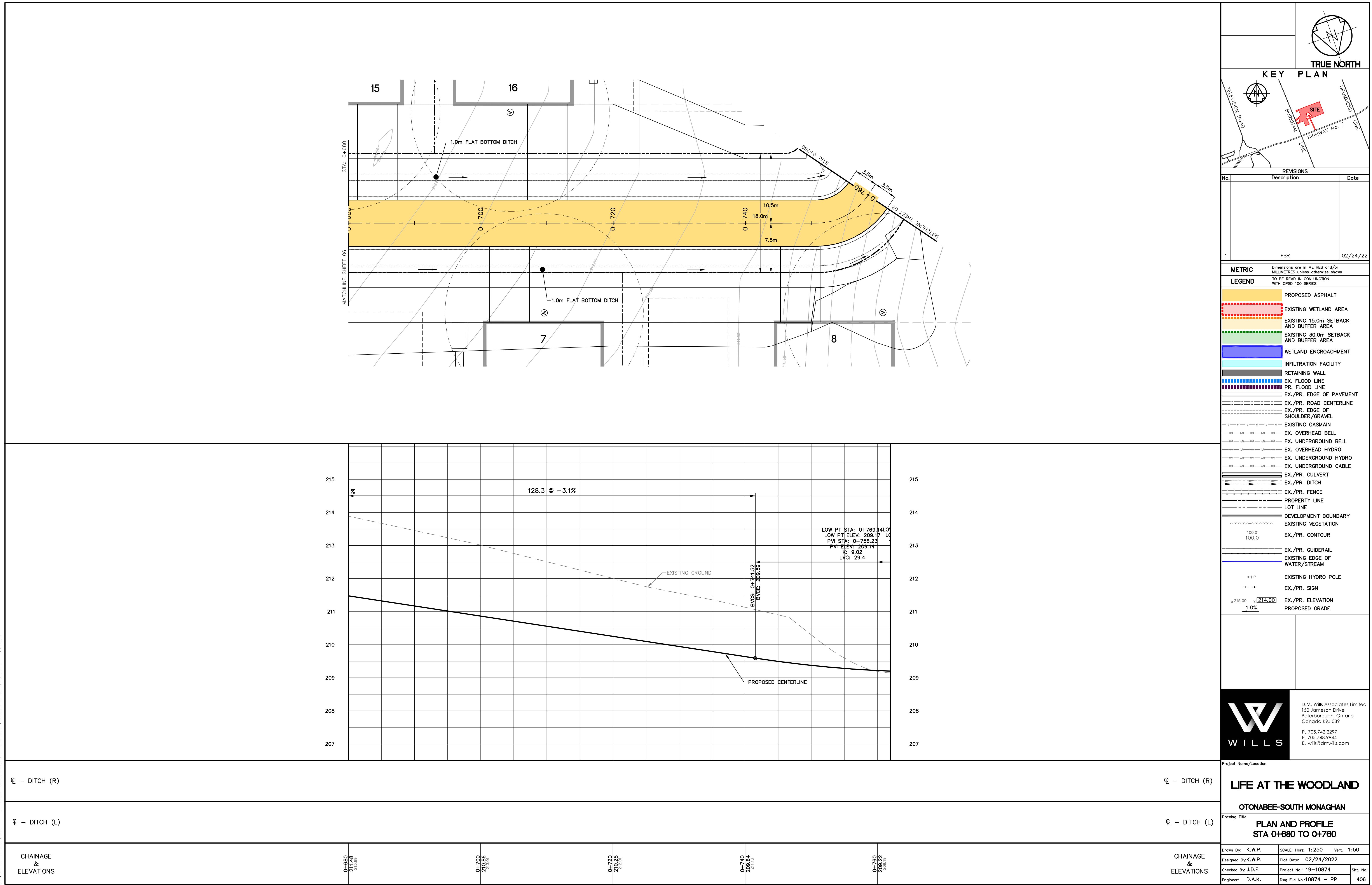
CHAINAGE & ELEVATIONS

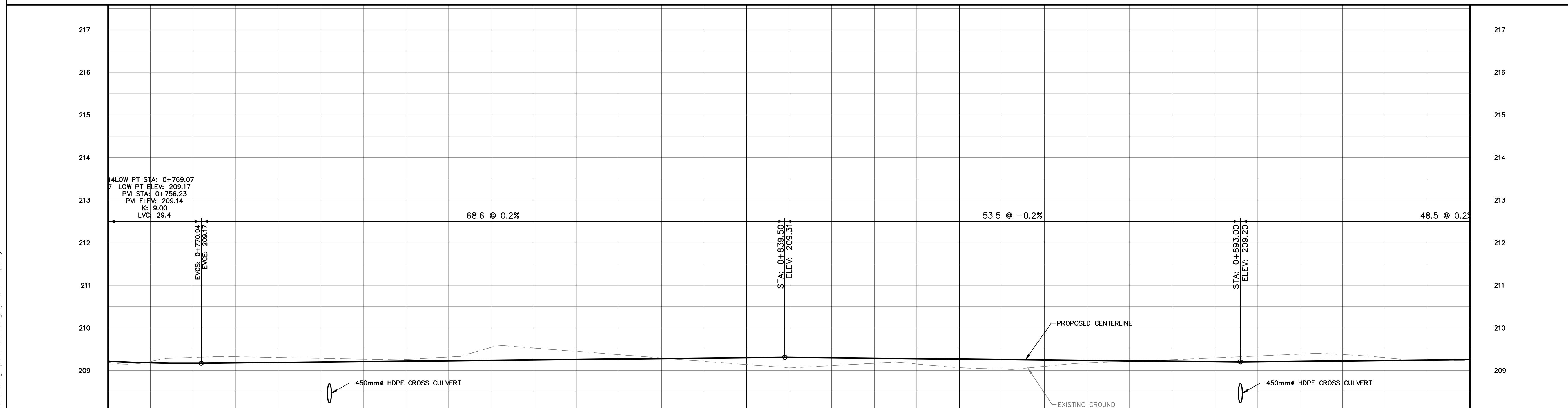
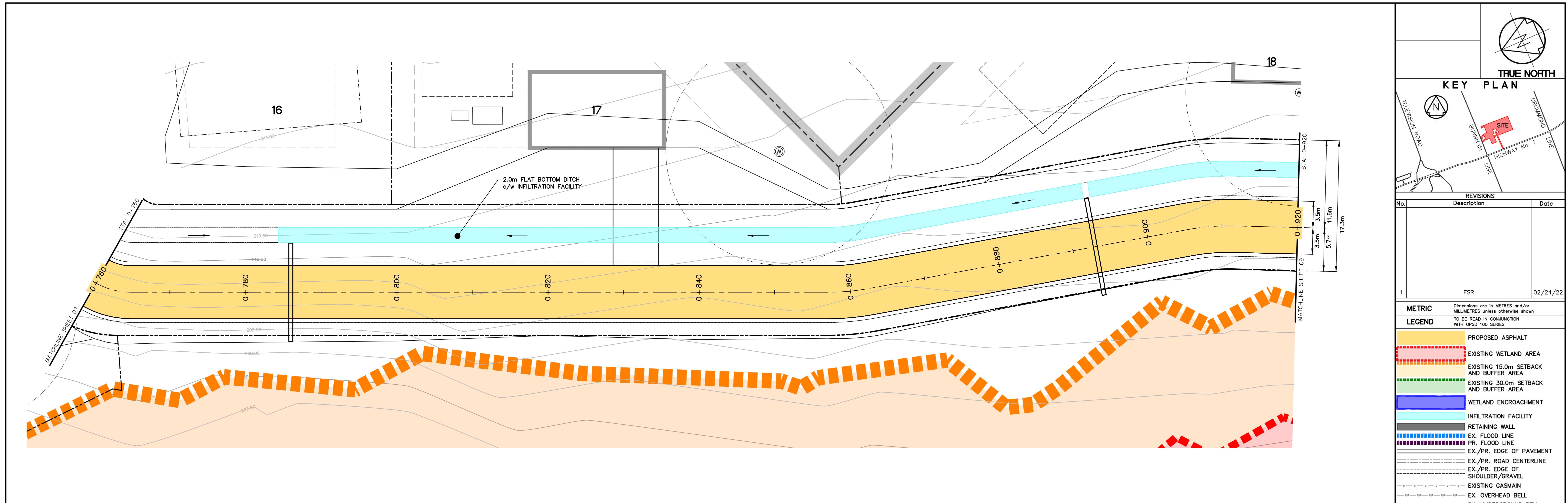
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Project Name/Location

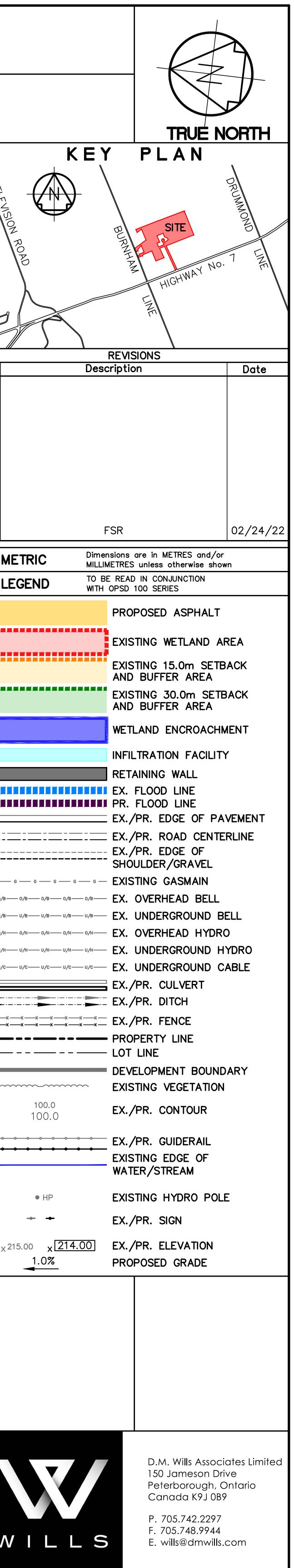
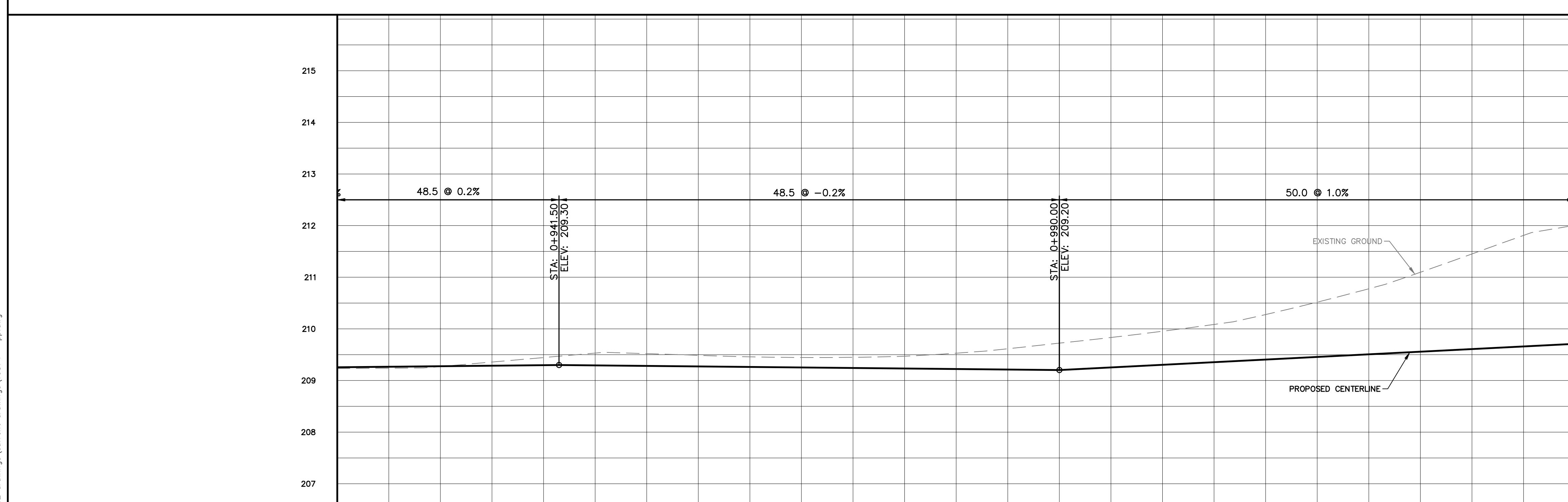
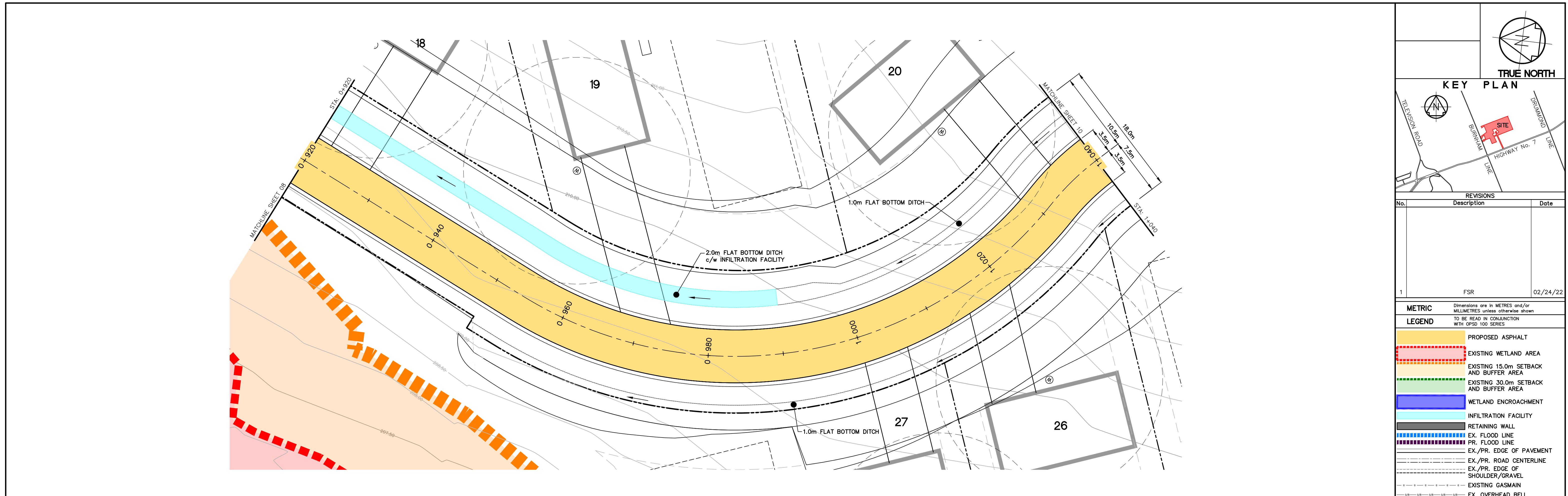
LIFE AT THE WOODLAND

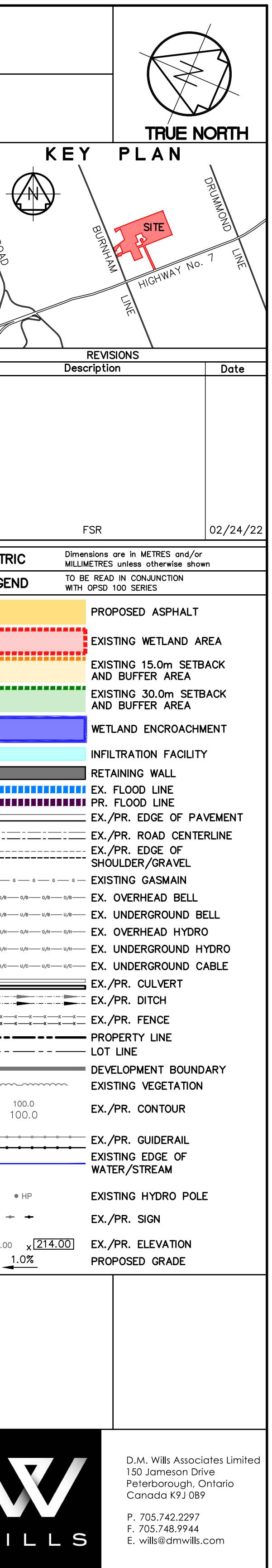
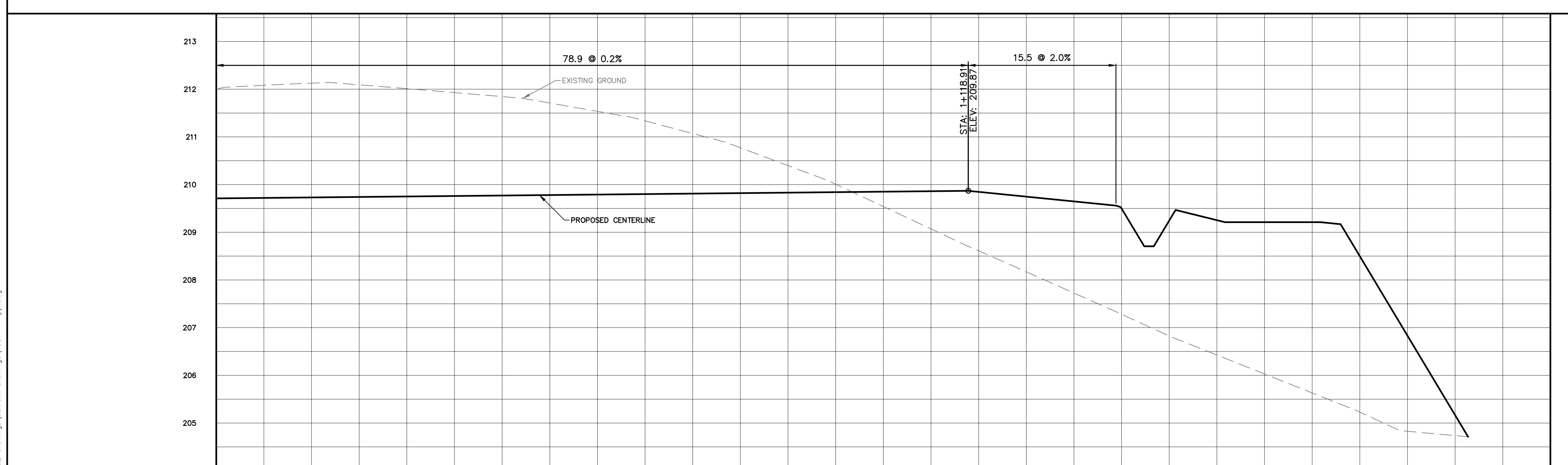
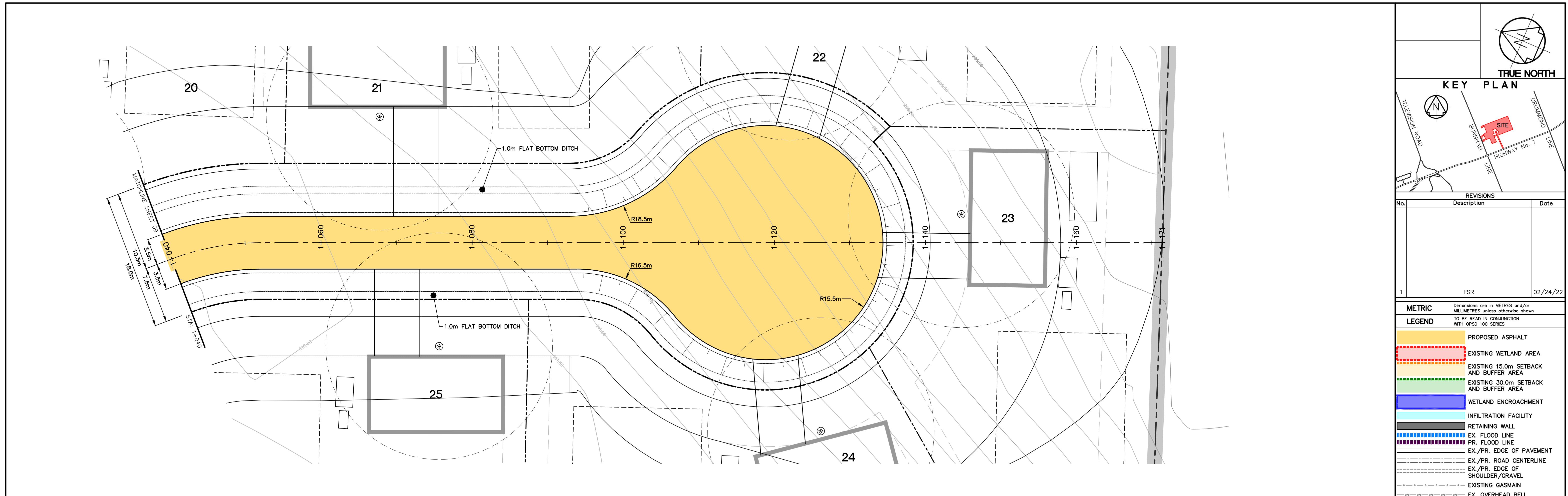
OTONABEE-SOUTH MONAGHAN

Drawing Title
**PLAN AND PROFILE
STA 0+760 TO 0+920**

Drawn By: K.W.P.	SCALE: Horz. 1:250 Vert. 1:50
Designed By: K.W.P.	Plot Date: 02/24/2022
Checked By: J.D.F.	Project No.: 19-10874
Engineer: D.A.K.	Sht. No.: 407

CHAINAGE & ELEVATIONS	CHAINAGE & ELEVATIONS
0+760 209.22	0+780 209.31
0+800 209.22	0+820 209.27
0+840 209.31	0+860 209.27
0+880 209.22	0+900 209.22
0+920 209.25	0+920 209.25





Project Name/Location	
LIFE AT THE WOODLAND	
OTONABEE-SOUTH MONAGHAN	
PLAN AND PROFILE	
CHAINAGE & ELEVATIONS	CHAINAGE & ELEVATIONS
Printed On: February 24, 2022 Printed On: February 24, 2022 - subdivision 02\drawings\current drawings\10874 - pp.dwg z:\10800-10899\10874	Drawn By: K.W.P. Scale: Horz. 1:250 Vert. 1:50 Designed By: K.W.P. Plot Date: 02/24/2022 Checked By: J.D.F. Project No: 19-10874 Sh. No.: Engineer: D.A.K. Dwg File No: 10874 - PP 409